The S904 and S905 Airfoils

May 1998—January 1999

D.M. Somers

Airfoils, Inc.

State College, Pennsylvania



Operated for the U.S. Department of Energy Office of Energy Efficiency and Renewable Energy by Midwest Research Institute • Battelle

Contract No. DE-AC36-99-GO10337

The S904 and S905 Airfoils

May 1998—January 1999

D.M. Somers
Airfoils, Inc.
State College, Pennsylvania

NREL Technical Monitor: Jim Tangler

Prepared under Subcontract No. AAM-8-18218-01



Operated for the U.S. Department of Energy Office of Energy Efficiency and Renewable Energy by Midwest Research Institute • Battelle

Contract No. DE-AC36-99-GO10337

This publication was reproduced from the best available copy submitted by the subcontractor and received no editorial review at NREL

NOTICE

This report was prepared as an account of work sponsored by an agency of the United States government. Neither the United States government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States government or any agency thereof.

Available electronically at http://www.osti.gov/bridge

Available for a processing fee to U.S. Department of Energy and its contractors, in paper, from:

U.S. Department of Energy Office of Scientific and Technical Information P.O. Box 62 Oak Ridge, TN 37831-0062

phone: 865.576.8401 fax: 865.576.5728

email: mailto:reports@adonis.osti.gov

Available for sale to the public, in paper, from:

U.S. Department of Commerce National Technical Information Service 5285 Port Royal Road Springfield, VA 22161

phone: 800.553.6847 fax: 703.605.6900

email: orders@ntis.fedworld.gov

online ordering: http://www.ntis.gov/ordering.htm



Table of Contents

Abstract		1
	on	
Symbols		1
Airfoil De	sign	2
Ob	jectives and Constraints	2
Phi	llosophy	3
Ex	ecution	5
Theoretica	l Procedure	6
Discussion	of Results	6
	04 Airfoil	
S90	05 Airfoil	7
Concludin	g Remarks	8
References	5	9
Appendix	A	46
Appendix	B	60
	List of Tables	
Table I.	Airfoil Design Specifications	10
Table II.	S904 Airfoil Coordinates	11
Table III.	S905 Airfoil Coordinates	12
	List of Figures	
Figure 1:	Airfoil shapes	13
Figure 2:	Inviscid pressure distributions for S904 airfoil	
Figure 3:	Section characteristics of S904 airfoil with transition free, transition	
_	fixed, and rough	20 – 30
Figure 4:	Inviscid pressure distributions for S905 airfoil	31 - 34
Figure 5:	Section characteristics of S905 airfoil with transition free,	
	transition fixed, and rough	35 - 45

ABSTRACT

A family of natural-laminar-flow airfoils, the S904 and S905, for cooling-tower fans has been designed and analyzed theoretically. The two primary objectives of high maximum lift, relatively insensitive to roughness, and low profile drag have been achieved. The constraint on the lift at zero angle of attack has not been satisfied. The constraints on the pitching moment and the airfoil thicknesses have essentially been satisfied. The airfoils should exhibit docile stalls.

INTRODUCTION

Large ducted fans are used in industrial and electrical-utility cooling towers to remove heat from circulating-water systems. The fans usually employ 4 to 12 blades having lengths of 1 1/2 to 6 m (5 to 20 ft). The blades are frequently operated in a moist environment, which contributes to leading-edge contamination and erosion. The blades typically incorporate National Advisory Committee for Aeronautics (NACA) airfoils (ref. 1).

The two airfoils designed under the present study are intended for the root and tip regions of a cooling-tower fan. The specific tasks performed under this study are described in National Renewable Energy Laboratory (NREL) Subcontract Number AAM-8-18218-01. The specifications for the airfoils are outlined in the Statement of Work. These specifications were later refined during discussions with James L. Tangler of NREL.

Because of the limitations of the theoretical methods (refs. 2 and 3) employed in this study, the results presented are in no way guaranteed to be accurate—either in an absolute or in a relative sense. This statement applies to the entire study.

SYMBOLS

C_p	pressure coefficient
c	airfoil chord, m
c_d	section profile-drag coefficient
c_l	section lift coefficient
$c_{\rm m}$	section pitching-moment coefficient about quarter-chord point
R	Reynolds number based on free-stream conditions and airfoil chord
t	airfoil thickness, m
x	airfoil abscissa, m

y airfoil ordinate, m

α angle of attack relative to x-axis, deg

Subscripts:

ll lower limit of low-drag range

max maximum

S turbulent boundary-layer separation

T boundary-layer transition

ul upper limit of low-drag range

0 zero lift

Abbreviations:

L. lower surface

S. turbulent boundary-layer separation location, x_9/c

T. boundary-layer transition location, x_T/c

U. upper surface

AIRFOIL DESIGN

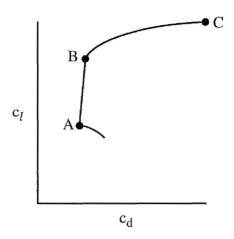
OBJECTIVES AND CONSTRAINTS

The design specifications for the family of airfoils are contained in table I. The family consists of two airfoils, root and tip. Two primary objectives are evident. The first objective is to achieve a high maximum lift coefficient. A requirement related to this objective is that the maximum lift coefficient not decrease significantly with transition fixed near the leading edge on both surfaces. In addition, the airfoils should exhibit docile stall characteristics. The second objective is to obtain low profile-drag coefficients over the range of lift coefficients from 0.20 to at least 1.10 for the root airfoil and from 0.65 to 1.20 for the tip airfoil.

Three major constraints were placed on the designs of these airfoils. First, the lift coefficient at zero angle of attack must equal 0.75. Second, the zero-lift pitching-moment coefficient must be no more negative than -0.15. Third, the airfoil thickness must equal 14-percent chord for the root airfoil and 10-percent chord for the tip airfoil.

PHILOSOPHY

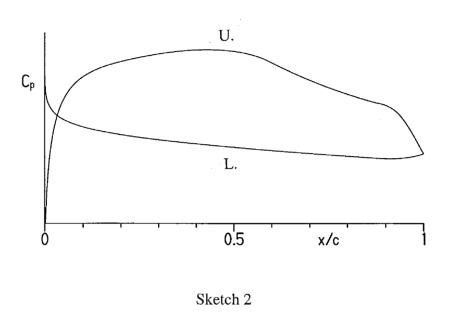
Given the above objectives and constraints, certain characteristics of the designs are apparent. The following sketch illustrates a drag polar that meets the goals for these designs. (The tip airfoil design specifications are used for the example.)



Sketch 1

The desired airfoil shape can be traced to the pressure distributions that occur at the various points in sketch 1. Point A is the lower limit of the low-drag, lift-coefficient range and point B, the upper limit. The drag increases rapidly outside the low-drag range because boundary-layer transition moves quickly toward the leading edge with increasing (or decreasing) lift coefficient. This feature results in a leading edge that produces a suction peak at higher lift coefficients, which ensures that transition on the upper surface will occur near the leading edge. Thus, the maximum lift coefficient, point C, occurs with turbulent flow along the entire upper surface and, therefore, should be relatively insensitive to roughness at the leading edge.

From the preceding discussion, the pressure distributions along the polar can be deduced. The pressure distribution at point A should look something like sketch 2, again using the tip airfoil as the example.



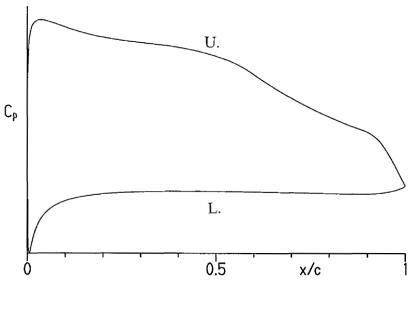
To achieve low drag, a favorable pressure gradient is desirable along the upper surface to about 45-percent chord. Aft of this point, a region having a shallow, adverse pressure gradient ("transition ramp") promotes the efficient transition from laminar to turbulent flow (ref. 4). The curved transition ramp (ref. 5) is followed by a concave pressure recovery, which results in a boundary-layer development that exhibits lower drag and less tendency toward separation than the corresponding linear or convex pressure recovery (ref. 4). The specific pressure recovery employed represents a compromise between maximum lift, drag, pitching moment, and stall characteristics. The steep, adverse pressure gradient aft of about 90-percent chord is a "separation ramp," originally proposed by F. X. Wortmann, which confines turbulent separation to a small region near the trailing edge. By constraining the movement of the separation point at high angles of attack, high lift coefficients can be achieved with little drag penalty. This feature also contributes to the docility of the stall characteristics. (See ref. 6.)

Along the lower surface, the pressure gradient is initially very adverse and then decreasingly so. Thus, transition is imminent over the entire forward portion of the lower surface. (See ref. 7.) This concept allows a wider low-drag range to be achieved and increases the amount of camber in the leading-edge region. The forward camber serves to balance, with respect to the pitching-moment constraint, the aft camber, both of which contribute to the achievement of a high maximum lift coefficient and low profile-drag coefficients. This region is followed by a nearly linear pressure recovery, which is an indistinguishable continuation of the forward pressure gradients.

¹Director, Institute for Aerodynamics and Gas Dynamics, University of Stuttgart, Germany.

The amounts of pressure recovery on the upper and lower surfaces are determined by the airfoil-thickness and pitching-moment constraints.

At point B, the pressure distribution should look like sketch 3.



Sketch 3

No suction spike exists at the leading edge. Instead, a gently rounded peak occurs aft of the leading edge. This feature allows higher lift coefficients to be reached without significant separation. At higher angles of attack, the peak becomes sharper and moves rapidly forward to the leading edge. This feature causes transition to move quickly toward the leading edge with increasing lift coefficient, which leads to the roughness insensitivity of the maximum lift coefficient.

EXECUTION

Given the pressure distributions previously discussed, the design of the airfoils is reduced to the inverse problem of transforming the pressure distributions into airfoil shapes. The Eppler Airfoil Design and Analysis Code (refs. 2 and 3) was used because of its unique capability for multipoint design and because of confidence gained during the design, analysis, and experimental verification of many other airfoils. (See ref. 8, for example.)

The root airfoil is designated the S904. The tip airfoil, the S905, was derived from the S904 airfoil to increase the aerodynamic and geometric compatibilities of the two airfoils. The S904 and S905 airfoil shapes are shown in figure 1 and the coordinates are contained in

tables II and III, respectively. The S904 airfoil thickness is 14-percent chord and the S905, 10-percent chord, which satisfy the design constraints.

THEORETICAL PROCEDURE

The section characteristics are predicted for Reynolds numbers of 0.5×10^6 through 1.5×10^6 , in increments of 0.1×10^6 . The computations were performed with transition free using transition mode 3, with transition fixed at 2-percent chord on the upper surface and 5-percent chord on the lower surface using transition mode 1, and "rough" using transition mode 9, which simulates distributed roughness due to, for example, leading-edge contamination by water drops or insects. (See ref. 3.) Because the free-stream Mach number for all relevant operating conditions remains below 0.2, all results are incompressible.

DISCUSSION OF RESULTS

S904 AIRFOIL

Pressure Distributions

The inviscid pressure distributions for the S904 airfoil at various angles of attack are shown in figure 2 and tabulated in appendix A.

Transition and Separation Locations

The variation of boundary-layer transition location with lift coefficient for the S904 airfoil is shown in figure 3 and tabulated in appendix A. It should be remembered that the method of references 2 and 3 "defines" the transition location as the end of the laminar boundary layer whether due to natural transition or laminar separation. Thus, for conditions that result in relatively long laminar separation bubbles (low lift coefficients for the upper surface, high lift coefficients for the lower surface, and low Reynolds numbers), poor agreement between the predicted "transition" locations and the locations measured experimentally can be expected. This poor agreement is worsened by the fact that transition is normally confirmed in experiments only by the detection of attached turbulent flow. For conditions that result in shorter laminar separation bubbles (high lift coefficients for the upper surface, low lift coefficients for the lower surface, and high Reynolds numbers), the agreement between theory and experiment is generally good. (See refs. 8 and 9.)

The variation of turbulent boundary-layer separation location with lift coefficient for the S904 airfoil is shown in figure 3 and tabulated in appendix A. A small, trailing-edge separation is predicted on the upper surface at all lift coefficients. This separation, which is caused by the separation ramp (fig. 2), generally increases in length with transition fixed and rough. Separation is predicted on the lower surface at low lift coefficients. Such separation usually has little effect on the section characteristics. (See ref. 9.)

Section Characteristics

Reynolds number effects.- The section characteristics of the S904 airfoil are shown in figure 3 and tabulated in appendix A. It should be noted that the maximum lift coefficient computed by the method of references 2 and 3 is not always realistic. Accordingly, an empirical criterion has been applied to the computed results. This criterion assumes that the maximum lift coefficient has been reached if the drag coefficient of the upper surface is greater than $0.0160 (2 \times 10^6/R)^{1/7}$ or if the length of turbulent separation on the upper surface is greater than 0.1000c. Thus, the maximum lift coefficient for the design Reynolds number of 0.5×10^6 is estimated to be 1.50, which meets the design objective. Based on the variation of the upper-surface separation location with lift coefficient, the stall characteristics are expected to be docile, which meets the design goal. The lift coefficient at zero angle of attack is predicted to be 0.73. Because of boundary-layer displacement effects not accounted for in the present analysis, however, the actual lift coefficient at zero angle of attack will probably be about 0.6, which is below the design constraint of 0.75. Low profile-drag coefficients are predicted over the range of lift coefficients from 0.16 to 1.21, which exceeds the range specified (0.20 to 1.10). The drag coefficient at the specified lower limit of the low-drag, lift-coefficient range ($c_I = 0.20$) is predicted to be 0.0080, which meets the design objective. The zero-lift pitching-moment coefficient is predicted to be -0.19, which exceeds the design constraint $(c_{m,0} \ge -0.15)$. Again because of boundary-layer displacement effects not accounted for in the present analysis, the pitching-moment coefficient is generally overpredicted by about 20 percent. Therefore, the actual zero-lift pitching-moment coefficient should be about -0.16, which still exceeds the design constraint. During the design process, it was determined that violating the constraints on the lift coefficient at zero angle of attack and the zero-lift pitchingmoment coefficient was necessary to meet other, more important goals.

Effect of roughness. The effect of roughness on the section characteristics of the S904 airfoil is shown in figure 3. The maximum lift coefficient for the design Reynolds number of 0.5×10^6 with transition fixed is estimated to be 1.41, a reduction of 6 percent from that with transition free. For the rough condition, the maximum lift coefficient is estimated to be 1.43, a reduction of 5 percent from that with transition free. Thus, the design requirement has been satisfied. The drag coefficients are, of course, adversely affected by the roughness.

S905 AIRFOIL

Pressure Distributions

The inviscid pressure distributions for the S905 airfoil at various angles of attack are shown in figure 4 and tabulated in appendix B.

Transition and Separation Locations

The variations of transition and separation locations with lift coefficient for the S905 airfoil are shown in figure 5 and tabulated in appendix B. A small, trailing-edge separation is

predicted on the upper surface at almost all lift coefficients. This separation, which is caused by the separation ramp (fig. 4), increases in length with transition fixed and rough.

Section Characteristics

Reynolds number effects.- The section characteristics of the S905 airfoil are shown in figure 5 and tabulated in appendix B. Using the previously described criterion, the maximum lift coefficient for the design Reynolds number of 1.0×10^6 is estimated to be 1.50, which meets the design objective. The stall characteristics are expected to be docile, which meets the design goal. The lift coefficient at zero angle of attack is predicted to be 0.75. Because of the previously mentioned effects, the actual lift coefficient at zero angle of attack will probably be about 0.6, which is below the design constraint of 0.75. During the design process, it was determined that violating the constraint was necessary to meet other, more important goals. Low drag coefficients are predicted over the range of lift coefficients from 0.59 to 1.16. Thus, the lower limit of the low-drag range is below the design objective ($c_{III} = 0.65$) although the upper limit is also below the design objective ($c_{l,ul} = 1.20$), primarily to meet other, more important goals. The drag coefficient at the specified lower limit of the low-drag range ($c_1 = 0.65$) is predicted to be 0.0070, which meets the design objective. The zero-lift pitching-moment coefficient is predicted to be -0.17, which exceeds the design constraint $(c_{m,0} \ge -0.15)$, although the actual zero-lift pitching-moment coefficient is expected to be about -0.15, which satisfies the constraint.

Effect of roughness. The effect of roughness on the section characteristics of the S905 airfoil is shown in figure 5. The maximum lift coefficient for the design Reynolds number of 1.0×10^6 with transition fixed is estimated to be 1.49, a reduction of 1 percent from that with transition free. For the rough condition, the maximum lift coefficient is estimated to be 1.48, a reduction of about 1 percent from that with transition free. Thus, the design requirement has been satisfied. The drag coefficients are, of course, adversely affected by the roughness.

CONCLUDING REMARKS

A family of natural-laminar-flow airfoils, the S904 and S905, for cooling-tower fans has been designed and analyzed theoretically. The two primary objectives of high maximum lift coefficient, relatively insensitive to leading-edge roughness, and low profile-drag coefficients have been achieved. The constraint on the lift coefficient at zero angle of attack has not been satisfied. The constraints on the pitching-moment coefficient and the airfoil thicknesses have essentially been satisfied. The airfoils should exhibit docile stall characteristics.

REFERENCES

- 1. Abbott, Ira H.; Von Doenhoff, Albert E.; and Stivers, Louis S., Jr.: Summary of Airfoil Data. NACA Rep. 824, 1945. (Supersedes NACA WR L-560.)
- 2. Eppler, Richard: Airfoil Design and Data. Springer-Verlag (Berlin), 1990.
- 3. Eppler, Richard: Airfoil Program System "PROFIL98." User's Guide. Richard Eppler, c.1998.
- 4. Wortmann, F. X.: Experimental Investigations on New Laminar Profiles for Gliders and Helicopters. TIL/T.4906, British Minist. Aviat., Mar. 1960. (Translated from Z. Flugwissenschaften, Bd. 5, Heft 8, Aug. 1957, S. 228–243.)
- 5. Eppler, Richard; and Somers, Dan M.: Airfoil Design for Reynolds Numbers Between 50,000 and 500,000. Proceedings of the Conference on Low Reynolds Number Airfoil Aerodynamics, UNDAS-CP-77B123, Univ. of Notre Dame, June 1985, pp. 1–14.
- 6. Maughmer, Mark D.; and Somers, Dan M.: Design and Experimental Results for a High-Altitude, Long-Endurance Airfoil. J. Aircr., vol. 26, no. 2, Feb. 1989, pp. 148–153.
- 7. Eppler, R.: Laminar Airfoils for Reynolds Numbers Greater Than 4×10^6 . B-819-35, Apr. 1969. (Available from NTIS as N69-28178; translated from Ingenieur-Archiv, Bd. 38, Heft 4/5, 1969, S. 232–240.)
- 8. Somers, Dan M.: Subsonic Natural-Laminar-Flow Airfoils. Natural Laminar Flow and Laminar Flow Control, R. W. Barnwell and M. Y. Hussaini, eds., Springer-Verlag New York, Inc., 1992, pp. 143–176.
- 9. Somers, Dan M.: Design and Experimental Results for the S814 Airfoil. NREL/SR-440-6919, Jan. 1997.

TABLE I.- AIRFOIL DESIGN SPECIFICATIONS

Airfoil	Root	Tip
Parameter	Objective/Constraint	
Reynolds number R	0.5×10^{6}	1.0×10^{6}
Maximum lift coefficient c _{l,max}	1.50	
Lift coefficient at zero angle of attack	0.75	
Lower limit of low-drag, lift-coefficient range $c_{l,1l}$	0.20	0.65
Profile-drag coefficient at lower limit of low-drag range	≤ 0.0080	≤ 0.0070
Upper limit of low-drag, lift-coefficient range $c_{l,ul}$	≥ 1.10	1.20
Zero-lift pitching-moment coefficient c _{m,0}	≥-0.15	
Airfoil thickness t/c	14%	10%

TABLE II.- S904 AIRFOIL COORDINATES

Upper Surface		Lower	Lower Surface	
x/c	y/c	x/c	y/c	
0.00019	0.00179	0.00000	-0.00004	
.00256	.00808	.00021	00165	
.00968	.01758	.00093	00316	
.02116	.02780	.00215	00470	
.03685	.03828	.00374	00627	
.05665	.04869	.01354	01266	
.08040	.05875	.02846	01889	
.10792	.06822	.04821	02465	
.13897	.07691	.07252	02979	
.17330	.08462	.10113	03414	
.21061	.09119	.13371	03759	
.25059	.09648	.16991	04003	
.29293	.10039	.20931	04131	
.33728	.10284	.25153	04120	
.38330	.10381	.29632	03951	
.43059	.10333	.34354	03619	
.47876	.10147	.39294	03140	
.52735	.09831	.44418	02524	
.57590	.09397	.49710	01784	
.62395	.08859	.55160	00978	
.67101	.08232	.60714	00186	
.71657	.07535	.66285	.00525	
.76012	.06785	.71775	.01102	
.80116	.05998	.77079	.01508	
.83919	.05188	.82084	.01719	
.87375	.04370	.86679	.01718	
.90436	.03546	.90735	.01506	
.93085	.02701	.94113	.01136	
.95346	.01852	.96729	.00713	
.97233	.01078	.98565	.00340	
.98703	.00476	.99645	.00088	
.99662	.00114	1.00000	.00000	
1.00000	.00000			

TABLE III.- S905 AIRFOIL COORDINATES

Upper Surface		Lower	Lower Surface	
x/c	y/c	x/c	y/c	
0.00003	0.00066	0.00004	-0.00070	
.00047	.00297	.00037	00179	
.00455	.01054	.00120	00266	
.01280	.01937	.00254	00346	
.02516	.02886	.00771	00536	
.04163	.03863	.02065	00762	
.06211	.04839	.03926	00898	
.08648	.05789	.06332	00945	
.11457	.06695	.09261	00909	
.14614	.07541	.12682	00800	
.18089	.08313	.16562	00627	
.21849	.08997	.20860	00402	
.25854	.09581	.25530	00138	
.30064	.10051	.30519	.00152	
.34435	.10391	.35772	.00455	
.38928	.10586	.41227	.00755	
.43504	.10625	.46821	.01041	
.48128	.10496	.52486	.01296	
.52766	.10192	.58152	.01510	
.57397	.09708	.63745	.01667	
.62009	.09058	.69190	.01759	
.66582	.08287	.74412	.01779	
.71067	.07440	.79336	.01725	
.75405	.06552	.83888	.01593	
.79539	.05651	.87997	.01390	
.83410	.04761	.91590	.01120	
.86962	.03901	.94594	.00809	
.90137	.03076	.96955	.00501	
.92905	.02278	.98647	.00240	
.95269	.01521	.99662	.00063	
.97222	.00863	1.00000	.00000	
.98716	.00373			
.99670	.00088			
1.00000	.00000			

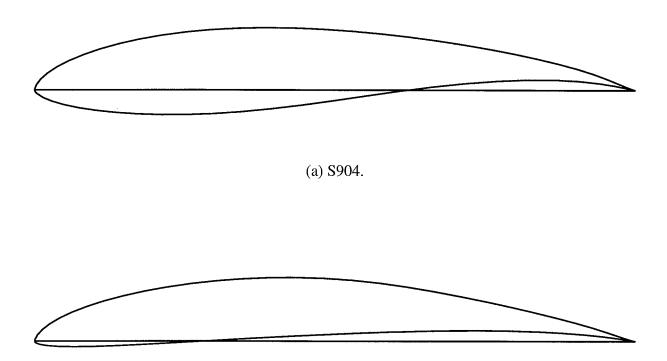


Figure 1.- Airfoil shapes.

(b) S905.

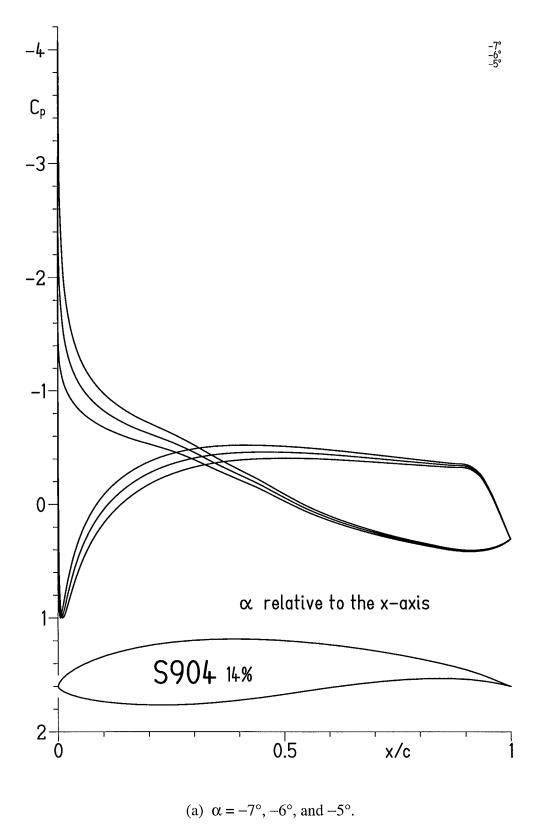
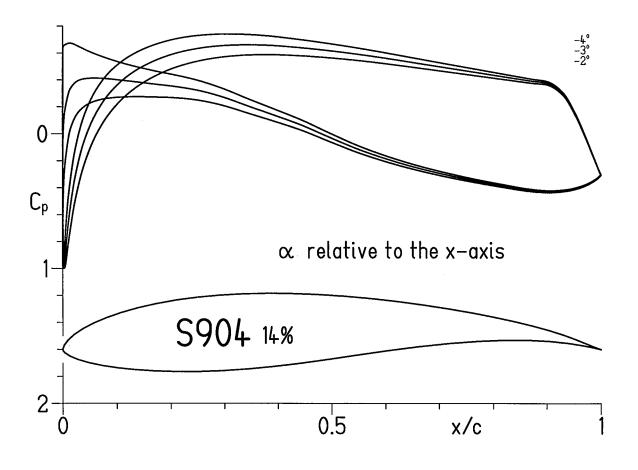
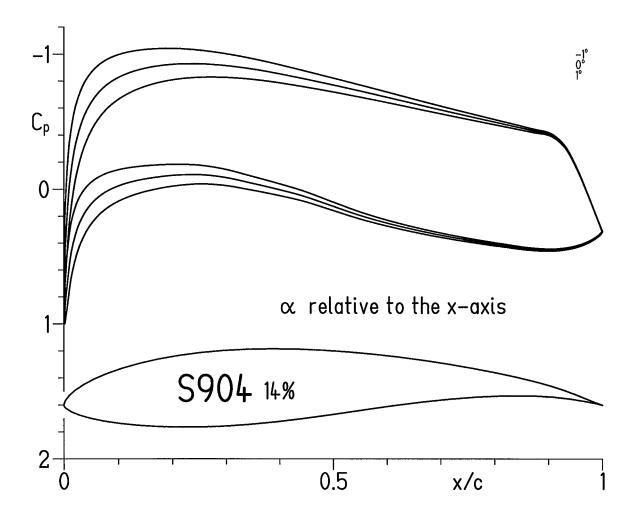


Figure 2.- Inviscid pressure distributions for S904 airfoil.



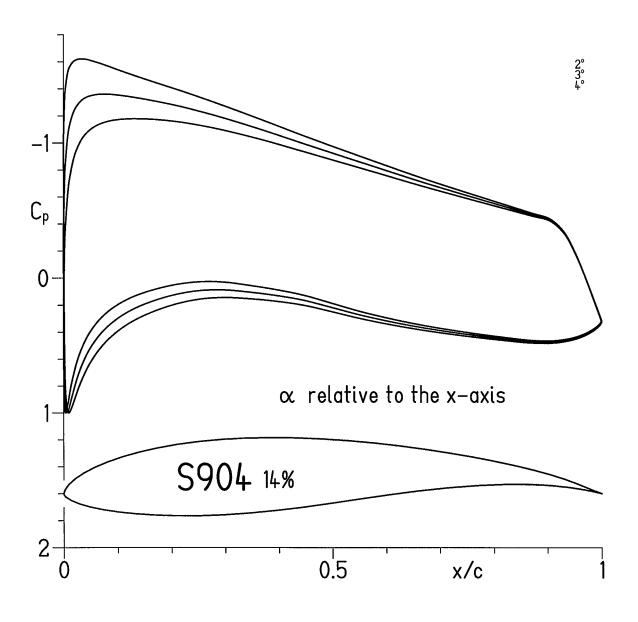
(b) $\alpha = -4^{\circ}, -3^{\circ}, \text{ and } -2^{\circ}.$

Figure 2.- Continued.



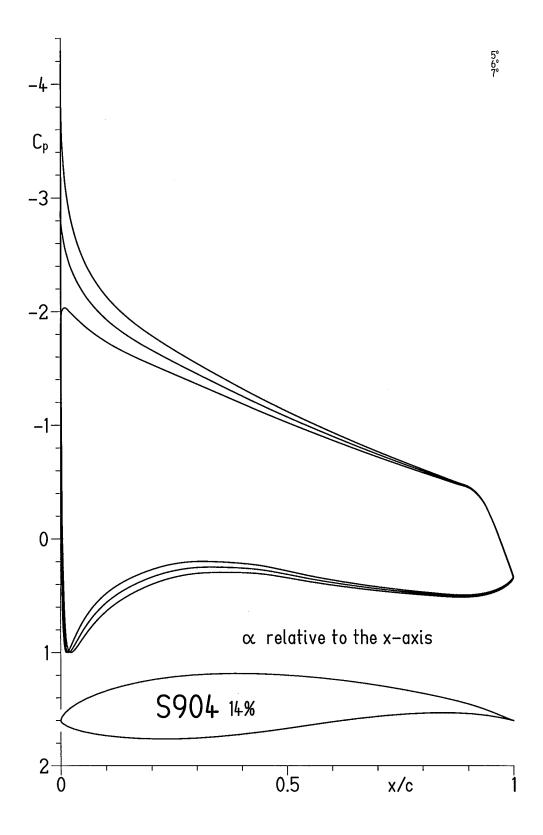
(c) $\alpha = -1^{\circ}$, 0° , and 1° .

Figure 2.- Continued.



(d) $\alpha = 2^{\circ}$, 3° , and 4° .

Figure 2.- Continued.



(e) $\alpha = 5^{\circ}$, 6° , and 7° .

Figure 2.- Continued.

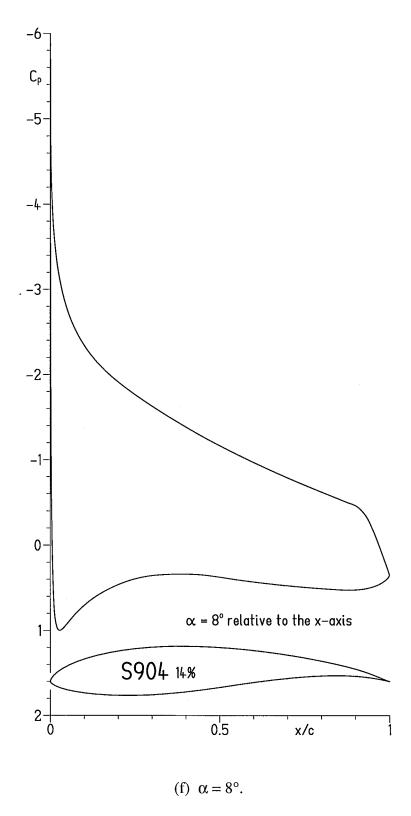


Figure 2.- Concluded.

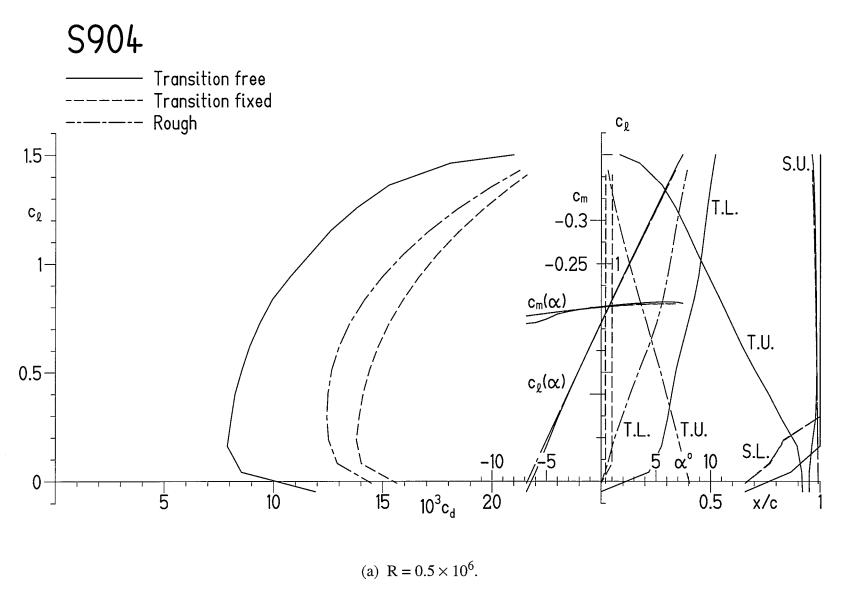
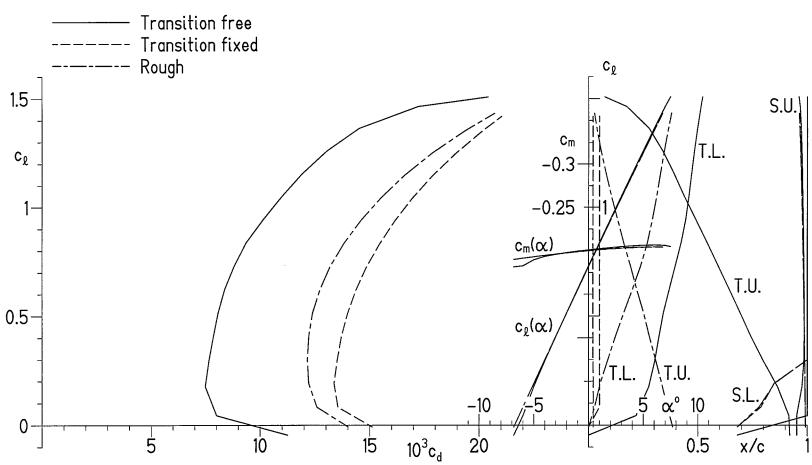
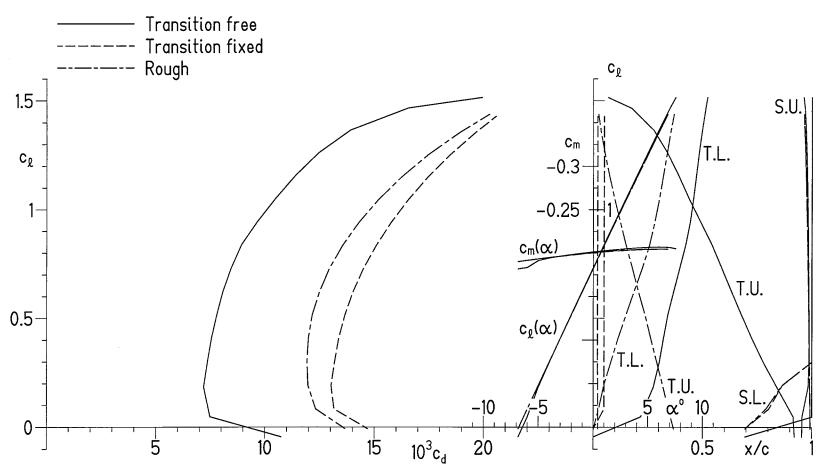


Figure 3.- Section characteristics of S904 airfoil with transition free, transition fixed, and rough.



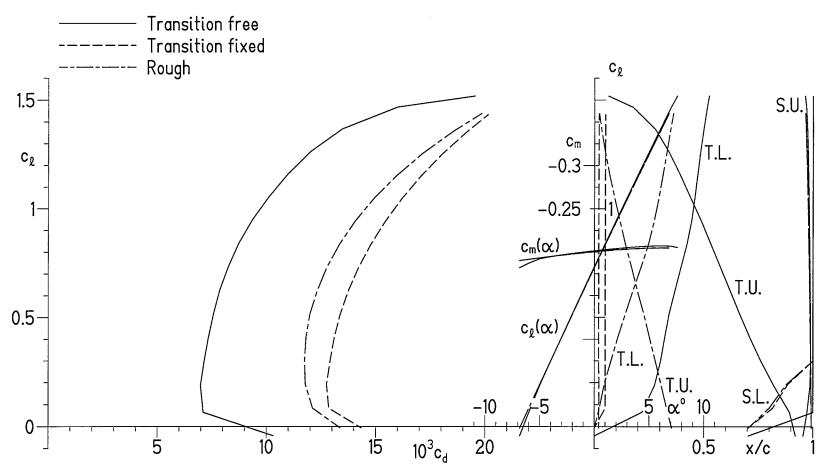
(b) $R = 0.6 \times 10^6$.

Figure 3.- Continued.



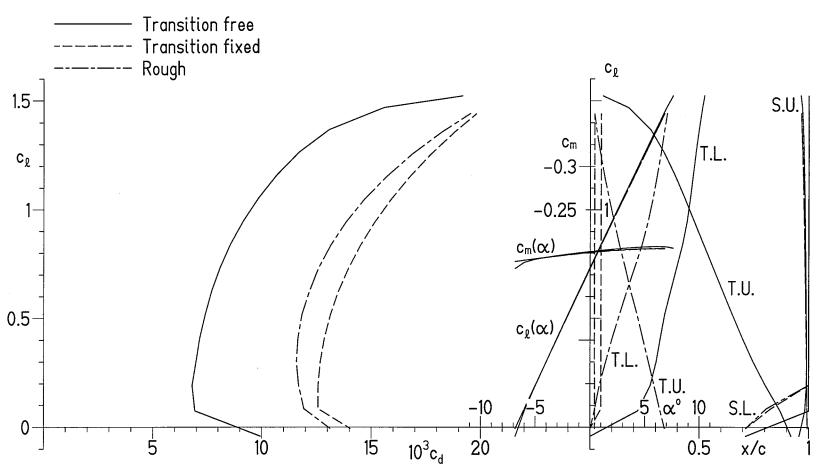
(c)
$$R = 0.7 \times 10^6$$
.

Figure 3.- Continued.



(d) $R = 0.8 \times 10^6$.

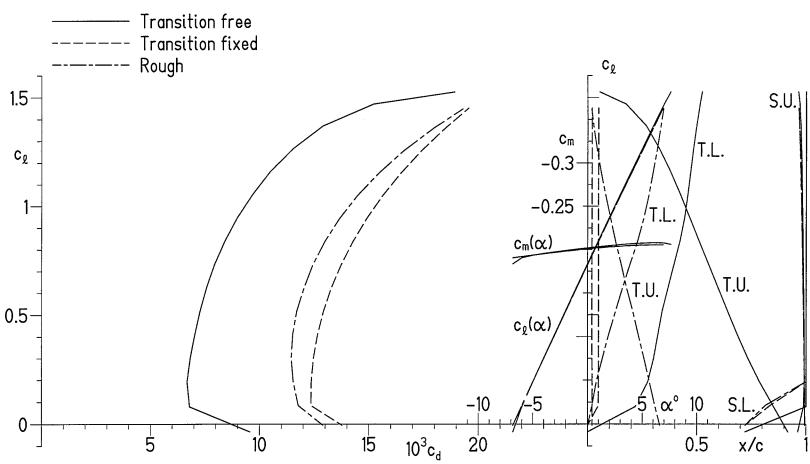
Figure 3.- Continued.



(e)
$$R = 0.9 \times 10^6$$
.

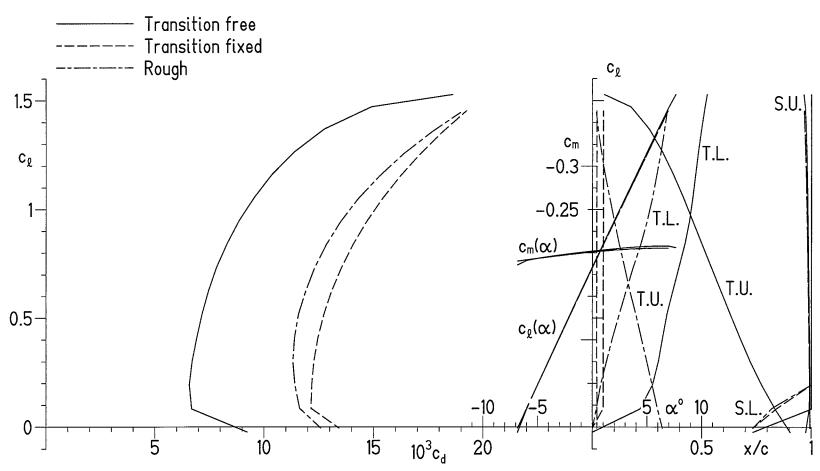
Figure 3.- Continued.





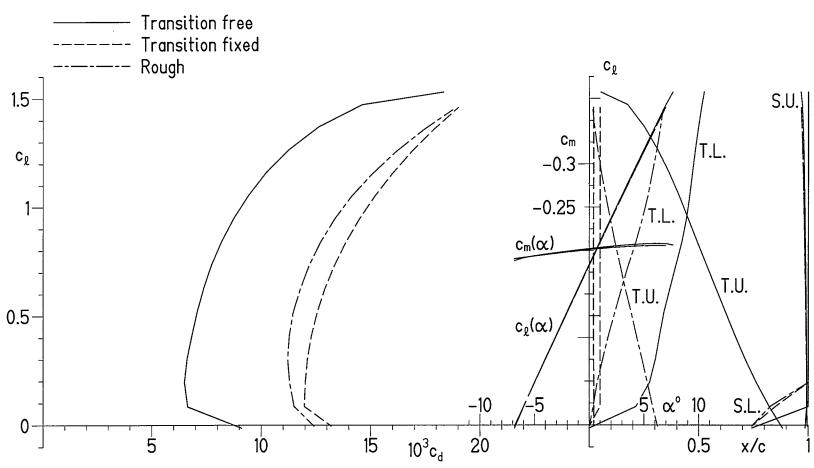
(f) $R = 1.0 \times 10^6$.

Figure 3.- Continued.



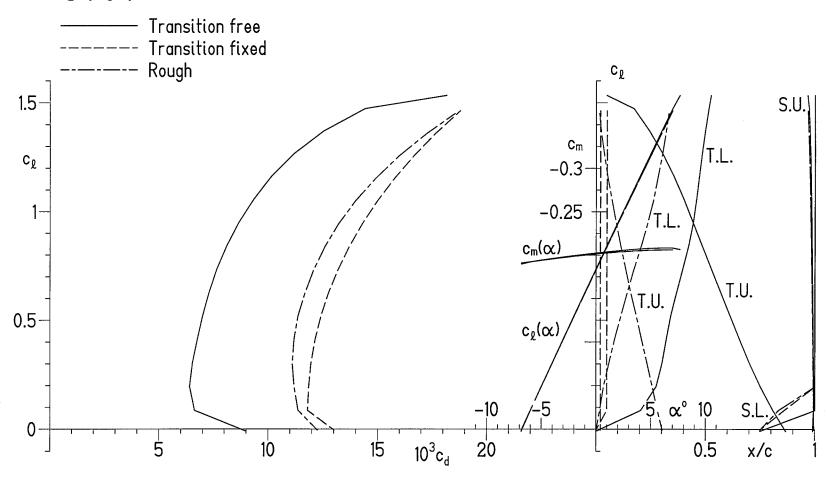
(g)
$$R = 1.1 \times 10^6$$
.

Figure 3.- Continued.



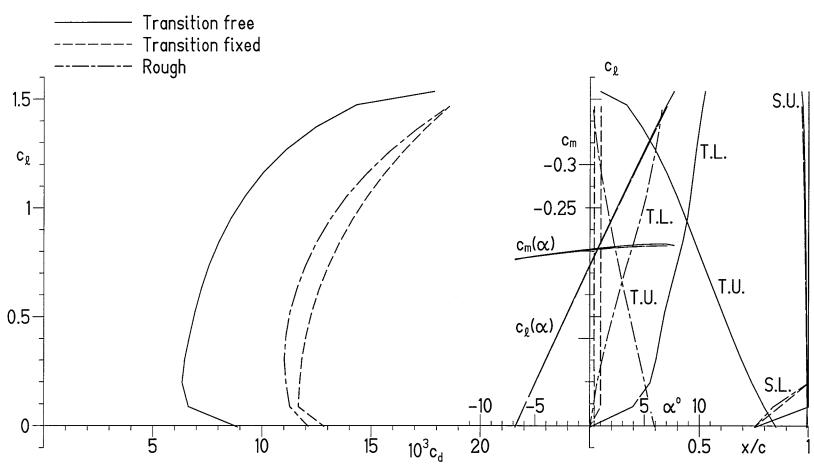
(h) $R = 1.2 \times 10^6$.

Figure 3.- Continued.



(i)
$$R = 1.3 \times 10^6$$
.

Figure 3.- Continued.



(j) $R = 1.4 \times 10^6$.

Figure 3.- Continued.

S904 Transition free Transition fixed Rough Cl 1.5-S.U. c_{m} $c_{\boldsymbol{\ell}}$ -0.3 -0.25 $c_m(\alpha)$ T.U. ÌT.U. 0.5 $c_{\ell}(\infty)$ α° 10 20

(k)
$$R = 1.5 \times 10^6$$
.

 $10^3 c_d$

0.5

x/c

15

10

5

Figure 3.- Concluded.

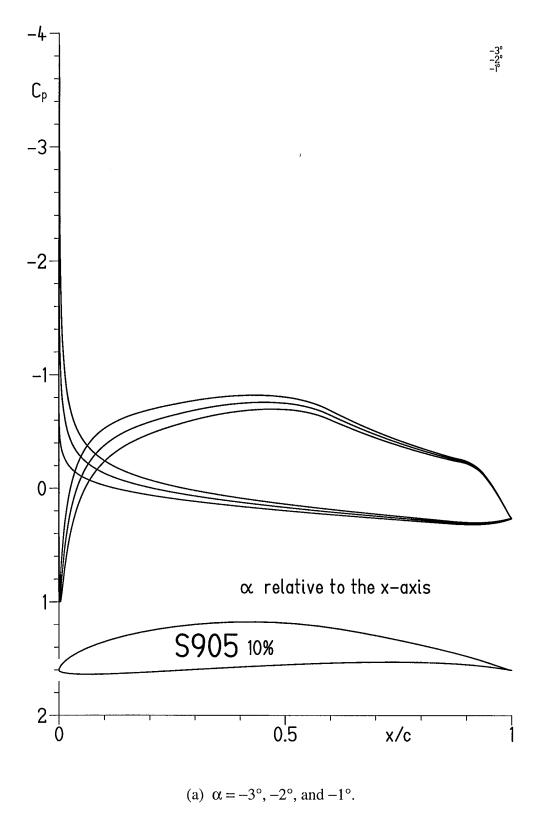
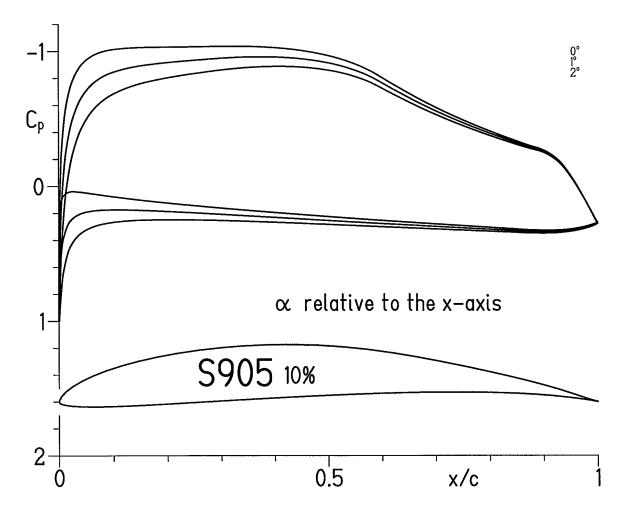
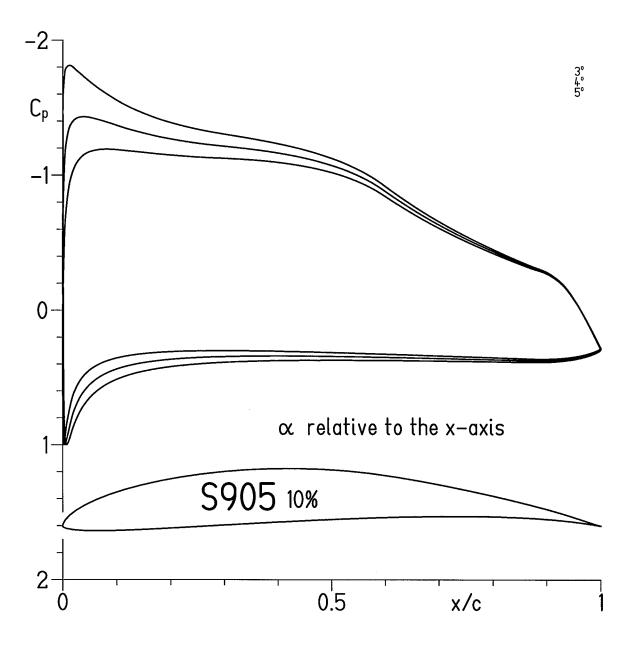


Figure 4.- Inviscid pressure distributions for S905 airfoil.



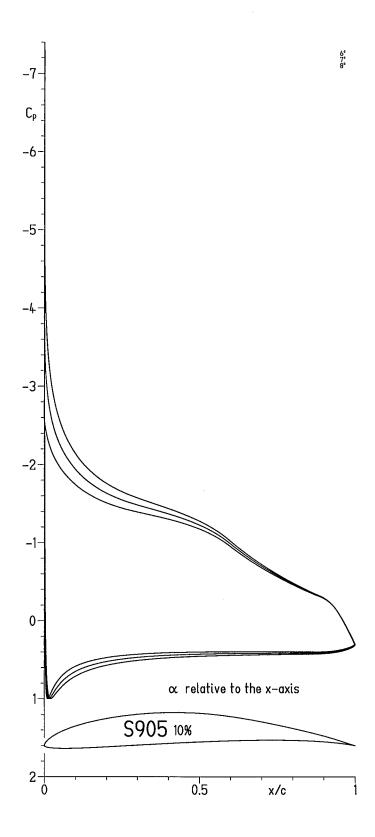
(b) $\alpha = 0^{\circ}$, 1° , and 2° .

Figure 4.- Continued.



(c) $\alpha = 3^{\circ}$, 4° , and 5° .

Figure 4.- Continued.



(d) $\alpha = 6^{\circ}$, 7° , and 8° .

Figure 4.- Concluded.

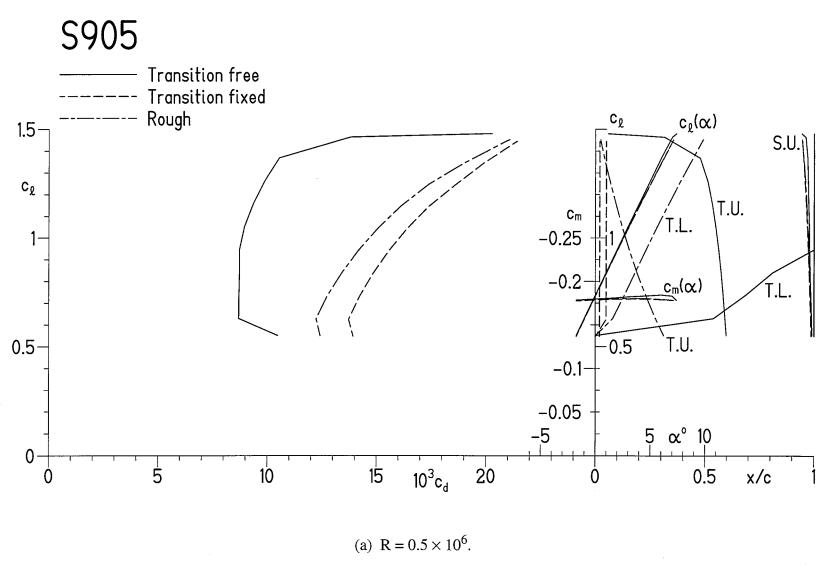
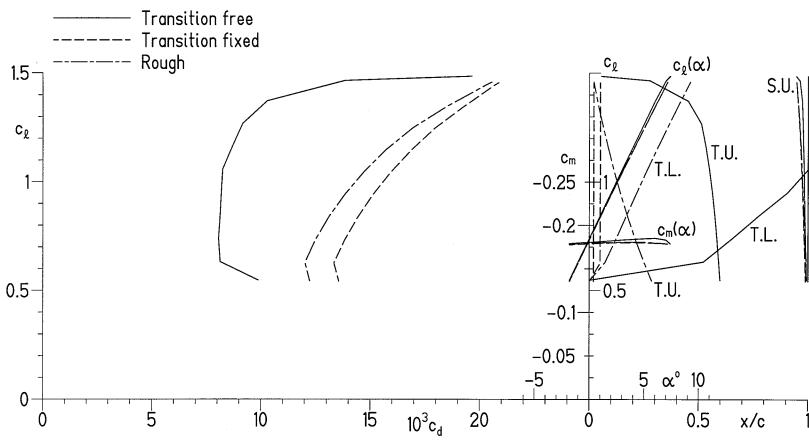


Figure 5.- Section characteristics of S905 airfoil with transition free, transition fixed, and rough.

S905



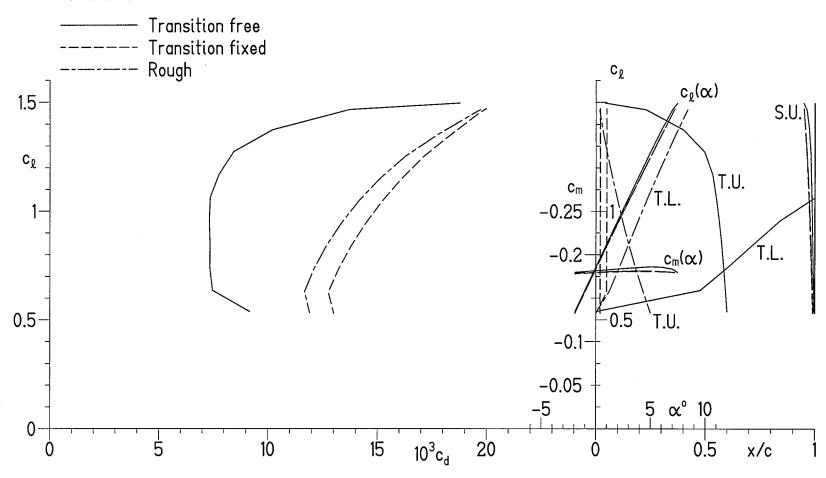
(b) $R = 0.6 \times 10^6$.

Figure 5.- Continued.

S905 Transition free Transition fixed Rough cl $c_{\ell}(\alpha)$ 1.5-S.U.) c_{ℓ} J.U. $\mathbf{C}_{\mathbf{m}}$ -0.25 -0.2 _c_m(∞) 0.5 0.5 T.U. -0.1 -0.05 -5 15 $10^3 c_d$ 20 0.5 10 x/c 5 0 (c) $R = 0.7 \times 10^6$.

Figure 5.- Continued.

S905



(d) $R = 0.8 \times 10^6$.

Figure 5.- Continued.

S905 Transition free Transition fixed Rough cl $c_{\ell}(\infty)$ 1.5-S.U.) c_{ℓ} T.U. $\mathbf{C}_{\mathbf{m}}$ -0.25 -0.2 $c_m(\alpha)$ 0.5 0.5 -0.1--0.05 -5 0 5 15 $10^3 c_d$ 20 0.5 10 x/c (e) $R = 0.9 \times 10^6$.

Figure 5.- Continued.

S905 Transition free Transition fixed Rough СĮ _{_c}(α) 1.5-S.U. Сl T.U. $\begin{array}{c} c_{\text{m}} \\ -0.25 \end{array}$ -0.2 $c_m(\infty)$ 0.5 0.5 -0.1--0.05 5 α° 10 -5 $10^3 c_d$ 20 0.5 5 10 15 x/c Ò

(f)
$$R = 1.0 \times 10^6$$
.

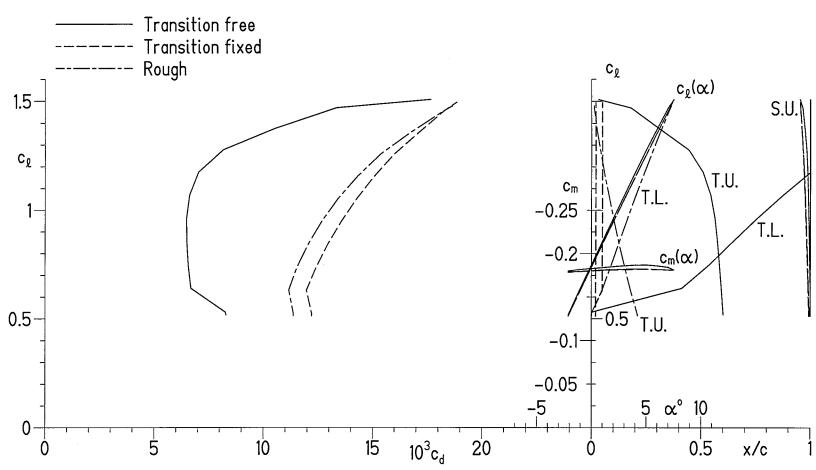
Figure 5.- Continued.

S905 Transition free Transition fixed Rough cl $c_{\ell}(\infty)$ 1.5-S.U. $c_{\boldsymbol{\ell}}$ T.U. C_{m} -0.25 -0.2 $c_m(\alpha)$ ⊬0.5 \T.U. 0.5 -0.1 -0.05 -5 α° 10 15 $10^3 c_d$ 0.5 5 20 10 x/c Ó

(g) $R = 1.1 \times 10^6$.

Figure 5.- Continued.

S905



(h) $R = 1.2 \times 10^6$.

Figure 5.- Continued.

S905 Transition free Transition fixed Rough \mathtt{c}_{ℓ} c_ℓ(α) 1.5-S.U. c_{ℓ} .U.T $\begin{array}{c} c_{\text{m}} \\ -0.25 \end{array}$ -0.2 $c_m(\alpha)$ 0.5 T.U. 0.5--0.1 -0.05 -5 α° 10 0 $10^3 c_d$ 20 15 0.5 5 10 x/c

(i) $R = 1.3 \times 10^6$.

Figure 5.- Continued.

S905 Transition free Transition fixed Rough CL $c_{\ell}(\infty)$ 1.5-S.U. c_{ℓ} T.U. $\begin{array}{c} c_m \\ -0.25 \end{array}$ -0.2 $c_m(\alpha)$ 0.5 T.U. 0.5 -0.1 -0.05 -5 α° 10 $10^3 c_d$ 20 5 15 0.5 10 x/c Ò 0

(j) $R = 1.4 \times 10^6$.

Figure 5.- Continued.

S905 Transition free Transition fixed Rough \mathtt{c}_{ℓ} $c_{\ell}(\alpha)$ 1.5-S.U. c_{ℓ} νT.U. $\mathbf{C}^{\mathbf{m}}$ -0.25 -0.2 $c_m(\alpha)$ -0.5[\]T.U. 0.5--0.1 -0.05 -5 α° 10

(k)
$$R = 1.5 \times 10^6$$
.

 $10^3 c_d$

20

0.5

x/c

15

10

5

Figure 5.- Concluded.

0

APPENDIX A

PRESSURE DISTRIBUTIONS, TRANSITION AND SEPARATION LOCATIONS, AND SECTION CHARACTERISTICS OF S904 AIRFOIL

	OIL S904	14%		-7.00	-6.00				-2.00	-1.00	0.00
N	X	Y		P(X) FOR							
1	1.00000	0.00000	0.00	0.302	0.302	0.302	0.303	0.305	0.306	0.309	0.311
2	0.99662	0.00114	1.00	0.275	0.274	0.274	0.273	0.273	0.274	0.275	0.276
4	0.97233	0.01078	2.00 3.00	0.187 0.050	0.184	0.182	0.180	0.179	0.178	0.178	0.178
5	0.95346	0.01078	4.00		0.045	0.040	0.036	0.033	0.030	0.028	0.026
6	0.93085	0.02701	5.00				-0.133				
7	0.90436	0.02701	6.00		-0.333					-0.311	
8	0.87375	0.04370	7.00			-0.347	-0.300	-0.373	-0.304	-0.419	-0.403
9	0.83919	0.05188	8.00	-0.325	-0 354	-0.333	-0.370	-0 412	-0 430	-0.447	-0.452
10	0.80116	0.05998	9.00							-0.477	
11	0.76012	0.06785	10.00							-0.510	
12	0.71657	0.07535	11,00							-0.545	
13	0.67101	0.08232	12.00	-0.380	-0.415	-0.450	-0.484	-0.517	-0.550	-0.583	-0.615
14	0.62395	0.08859	13.00	-0.392	-0.431	-0.470	-0.509	-0.547	-0.585	-0.622	-0.659
15	0.57590	0.09397	14.00	-0.401	-0.445	-0.489	-0.533	-0.576	-0.619	-0.662	-0.704
16	0.52735	0.09831	15.00							-0.700	
17	0.47876	0.10147	16.00							-0.735	
18	0.43059	0.10333	17.00	-0.398	-0.459	-0.520	-0.582	-0.644	-0.706	-0.768	-0.830
19	0.38330	0.10381	18.00	-0.384	-0.451	-0.519	-0.588	-0.657	-0.727	-0.797	-0.867
20	0.33728	0.10284	19.00							-0.817	
21	0.29293	0.10039	20.00							-0.828	
22 23	0.25059	0.09648	21.00							-0.827	
24	0.21061 0.17330	0.09119 0.08462	22.00 23.00							-0.815	
25	0.17330	0.07691	24.00							-0.787	
26	0.10792	0.06822	25.00	0.127						-0.745 -0.685	
27	0.08040	0.05875	26.00	0.283	0.158					-0.600	
28	0.05665	0.04869	27.00	0.467	0.341	0.202				-0.481	
29	0.03685	0.03828	28.00	0.678	0.558	0.420	0.264			-0.314	
30	0.02116	0.02780	29.00	0.889	0.796	0.676	0.529	0.354	0.152		
31	0.00968	0.01758	30.00	0.999	0.985	0.926	0.824	0.678	0.488		-0.021
32	0.00256	0.00808	31.00	0.610	0.817	0.947	0.999	0.973	0.870	0.689	0.431
33	0.00019	0.00179	31.75	-0.959	-0.305	0.218	0.607	0.864	0.988	0.978	0.835
34		-0.00004	32.00		-1.220		0.163	0.607	0.885	0.997	0.944
35		-0.00165	32.25			-1.574		0.091	0.606	0.909	0.999
36		-0.00316	32.50				-0.647		0.460	0.788	0.966
37		-0.00470	32.75				-0.654		0.339	0.669	0.885
38 39		-0.00627	33.00 34.00				-0.660		0.240	0.560	0.794
40		-0.01266 -0.01889	35.00				-0.674 -0.650			0.239	0.465 0.250
41		-0.02465	36.00				-0.612			-0.046	0.230
42		-0.02979	37.00				-0.574				0.030
43		-0.03414	38.00							-0.145	
44		-0.03759	39.00							-0.166	
45		-0.04003	40.00							-0.178	
46	0.20931	-0.04131	41.00	-0.698	-0.608	-0.520	-0.433	-0,348	-0.265	-0.183	-0.104
47		-0.04120	42.00							-0.176	
48		-0.03951	43.00							-0.148	
49		-0.03619	44.00							-0.100	
50		-0.03140	45.00							-0.047	
51		-0.02524	46.00				-0.102			0.013	0.051
52 53		-0.01784 -0.00978	47.00 48.00	-0.097 0.017	0.042	-0.035 0.067	0.004	0.028 0.118	0.059	0.091	0.122
54		-0.00378	49.00	0.017	0.042	0.067	0.092	0.118	0.144	0.170	0.196
55	0.66285	0.00525	50.00	0.111	0.131	0.132	0.172	0.155	0.213	0.230	0.258 0.310
56	0.71775	0.00323	51.00	0.254	0.267	0.222	0.295	0.309	0.323	0.338	0.353
57	0.77079	0.01508	52.00	0.307	0.318	0.329	0.341	0.352	0.364	0.377	0.389
58	0.82084	0.01719	53.00	0.351	0.360	0.369	0.378	0.388	0.398	0.408	0.419
59	0.86679	0.01718	54.00	0.387	0.394	0.401	0.409	0.417	0.425	0.434	0.443
60	0.90735	0.01506	55.00	0.403	0.409	0.415	0.421	0.428	0.435	0.442	0.450
61	0.94113	0.01136	56.00	0.395	0.399	0.404	0.410	0.415	0.421	0.427	0.434
62	0.96729	0.00713	57.00	0.370	0.374	0.378	0.382	0.387	0,392	0.397	0.403
63	0.98565	0.00340	58.00	0.339	0.341	0.344	0.347	0.351	0.355	0.360	0.365
64	0.99645	0.00088	59.00	0.311	0.313	0.315	0.317	0.320	0.323	0.326	0.330
65	1.00000	0.00000	60.00	0.302	0.302	0.302	0.303	0.305	0.306	0.309	0.311
ALPHA	A0= 6.83 I	DEGREES C	M0=-0.19	27 ETA= 1	1.109						

ATRE	OIL S904	14%		1.00	2.00	3.00	4.00	5.00	6.00	7.00	8.00
N	X	Y	NU	CP(X) FOR						7.00	0.00
1	1.00000	0.00000	0.00	0.315	0.318	0.322	0.326	0.331	0.336	0.341	0.347
2	0.99662	0.00114	1.00	0.278	0.281	0.283	0.287	0.290	0.294	0.299	0.304
3	0.98703	0.00476	2.00	0.178	0.180	0.181	0.183	0.186	0.189	0.193	0.197
4	0.97233	0.01078	3.00	0.025	0.025	0.025	0.026	0.027	0.029	0.032	0.035
5	0.95346	0.01852	4.00							-0.162	
6	0.93085	0.02701	5.00							-0.344	
7 8	0.90436 0.87375	0.03546	6.00 7.00							-0.452 -0.500	
9	0.83919	0.05188	8.00							-0.553	
10	0.80116	0.05998	9.00	-0.475	-0.433	-0.500	-0.515	-0.531	-0.592	-0.610	-0.502
11	0.76012	0.06785	10.00							-0.673	
12	0.71657	0.07535	11.00							-0.742	
13	0.67101	0.08232	12.00							-0.816	
14	0.62395	0.08859	13.00	-0.695	-0.731	-0.765	-0.799	-0.833	-0.865	-0.897	-0.927
15	0.57590	0.09397	14.00	-0.746	-0.787	-0.827	-0.867	-0.906	-0.944	-0.982	-1.018
16	0.52735	0.09831	15.00	-0.796	-0.843	-0.890	-0.936	-0.982	-1.027	-1.071	-1.114
17	0.47876	0.10147	16.00							-1.163	
18	0.43059	0.10333	17.00							-1.259	
19 20	0.38330	0.10381	18.00 19.00							-1.358	
21	0.33728	0.10284	20.00							-1.458	
22	0.25059	0.09648	21.00	-1.000	-1.037	-1.100	-1.200	-1 ///	-1 551	-1.558 -1.658	-1.031
23	0.21061	0.09119	22.00							-1.759	
24	0.17330	0.08462	23.00							-1.862	
25	0.13897	0.07691	24.00							-1.974	
26	0.10792	0.06822	25.00							-2.098	
27	0.08040	0.05875	26.00							-2.240	
28	0.05665	0.04869	27.00	-0.895	-1.119	-1.355	-1.601	-1.859	-2.126	-2.403	-2.690
29	0.03685	0.03828	28.00							-2.597	
30	0.02116	0.02780	29.00							-2.829	
31	0.00968	0.01758	30.00							-3.124	
32 33	0.00256	0.00808	31.00 31.75							-3.501	
33 34		-0.00004	32.00	0.558 0.724	0.148	0.394	-1.007	1.072	2.807	-3.871 -4.056	-5.062
35		-0.00165	32.25	0.724	0.533	-0.214	-0.323	-1 731	-2.032	-4.294	-5.420
36		-0.00316	32.50	0.992	0.868	0.592				-2.007	
37		-0.00470	32.75	0.990	0.981	0.860	0.627		-0.177	-0.746	
38		-0.00627	33.00	0.940	0.999	0.970	0.854	0.650	0.359		
39		-0.01266	34.00	0.651	0.798	0.905	0.972	0.999	0.986	0.933	0.839
40		-0.01889	35.00	0.421	0.571	0.698	0.804	0.886	0.947	0.984	1.000
41		-0.02465	36.00	0.266	0.402	0.524	0.633	0.728	0.809	0.875	0.928
42		-0.02979	37.00	0.160	0.281	0.393	0.495	0.589	0.673	0.748	0.813
43		-0.03414	38.00	0.087	0.194	0.295	0.389	0.477	0.558	0.633	0.701
44		-0.03759	39.00	0.036	0.130	0.221	0.307	0.388	0.464	0.536	0.603
45 46		-0.04003	40.00 41.00	0.000	0.084	0.165	0.242	0.317	0.388	0.455	0.519
47		-0.04131 -0.04120	42.00	-0.026 -0.037	0.049	0.122	0.192 0.158	0.260	0.325	0.388	0.448 0.393
48		-0.03951	43.00	-0.037	0.023	0.089	0.136	0.220	0.254	0.306	0.357
49		-0.03619	44.00	0.004	0.055	0.105	0.154	0.203	0.250	0.296	0.342
50		-0.03140	45.00	0.042	0.086	0.129	0.172	0.214	0.256	0.297	0.337
51		-0.02524	46.00	0.088	0.126	0.163	0.200	0.237	0.273	0.309	0.344
52		-0.01784	47.00	0.154	0.185	0.217	0.248	0.279	0.309	0.340	0.370
53		-0.00978	48.00	0.222	0.248	0.274	0.300	0.326	0.352	0.378	0.403
54		-0.00186	49.00	0.279	0.301	0.323	0.345	0.367	0.389	0.411	0.433
55	0.66285	0.00525	50.00	0.328	0.346	0.365	0.383	0.402	0.420	0.439	0.458
56	0.71775	0.01102	51.00	0.369	0.384	0.400	0.415	0.431	0.447	0.463	0.480
57	0.77079	0.01508	52.00	0.402	0.415	0.429	0.442	0.456	0.469	0.483	0.497
58	0.82084	0.01719	53.00	0.430	0.441	0.452	0.464	0.475	0.487	0.499	0.512
59 60	0.86679 0.90735	0.01718 0.01506	54.00 55.00	0.452 0.457	0.461	0.471	0.481	0.491 0.491	0.501	0.512	0.522 0.519
61	0.94113	0.01306	56.00	0.457	0.448	0.474	0.463	0.491	0.300	0.310	0.319
62	0.96729	0.01136	57.00	0.441	0.416	0.430	0.429	0.471	0.444	0.452	0.457
63	0.98565	0.00340	58.00	0.370	0.375	0.381	0.388	0.394	0.401	0.409	0.416
64	0.99645	0.00088	59.00	0.334	0.339	0.344	0.349	0.355	0.361	0.368	0.374
65	1.00000	0.00000	60.00	0.315	0.318	0.322	0.326	0.331	0.336		0.347
ALPH	A0= 6.83 I	DEGREES C	M0 = -0.1	.927 ETA=	1.109						

R= 500000 MU=900
S TURB S SEP CD
0.6085 0.0091 0.0060
1.0110 0.0000 0.0084*
CL=-0.008 CD=0.01448
CM=-0.1899
S TURB S SEP CD
0.6328 0.0102 0.0065
CL= 0.082 CD=0.01291
CM=-0.1913
S TURB S SEP CD
0.5959 0.0105 0.0075
0.9466 0.0000 0.0055
CL= 0.190 CD=0.01252
CM=-0.1929
S TURB S SEP CD
0.6599 0.0115 0.0070
0.9466 0.0000 0.0055
CL= 0.190 CD=0.01252
CM=-0.1929
S TURB S SEP CD
0.6876 0.0129 0.0075
0.9087 0.0000 0.0049
CL= 0.298 CD=0.01243
CM=-0.1945
S TURB S SEP CD ALPHA(DEG.) R= 500000 MU=300 R= 500000 MI=100 6.83 S TURB S SEP CD
UPPER 0.0853 0.0529 0.0035*
LOWER 1.0110 0.0000 0.0084* S TURB S SEP CD 1.0037 0.0093 0.0072 1.0110 0.0000 0.0084* LOWER 1.0110 0.0000 0.0084*
TOTAL CLE-0.047 CD-0.01192
CM=-0.1811
6.00 S TURB S SEP CD
UPPER 0.8991 0.0533 0.0036*
LOWER 0.7872 0.0000 0.0049*
TOTAL CLE 0.042 CD-0.00853
CM=-0.1822 CL=-0.008 CD=0.01564 CM=-0.1898 CM=-0.1898
S TURB S SEP CD
1.0037 0.0105 0.0076
0.9560 0.0000 0.0064*
CL= 0.082 CD=0.01402
CM=-0.1912
S TURB S SEP CD
1.0037 0.0119 0.0082
0.9560 0.0000 0.0056 TOTAL CLE - 0.42 CD=0.00853

CM=-0.1822

-5.00 S TURB S SEP CD

UPPER 0.1116 0.0407 0.0035

LOMER 0.7293 0.0000 0.0044*

TOTAL CLE - 0.161 CD=0.00789

-4.00 S TURB S SEP CD

UPPER 0.1856 0.0227 0.0040

LOWER 0.7021 0.0000 0.0040*

TOTAL CLE - 0.288 CD=0.00807

CM=-0.1921

-3.00 S TURB S SEP CD

UPPER 0.2451 0.0184 0.0046

LOWER 0.6831 0.0000 0.0037*

TOTAL CLE - 0.401 CD=0.00824

CM=-0.1950

-2.00 S TURB S SEP CD

UPPER 0.3098 0.0165 0.0052*

LOWER 0.6629 0.0000 0.0034*

TOTAL CLE - 0.521 CD=0.00854 0.9560 0.0000 0.0056 CL= 0.190 CD=0.01379 CM=-0.1928 S TURB S SEP CD 1.0053 0.0134 0.0088 0.9560 0.0000 0.0051 CL= 0.297 CD=0.01392 CM=-0.1944 S TURB S SEP CD 1.0053 0.0151 0.0094 0.9560 0.0000 0.0047 CL= 0.405 CD=0.01410 CM=-0.1959 S TURB S SEP CD 1.0053 0.0156 0.0101 0.9560 0.0000 0.0047 CL= 0.405 CD=0.01410 CM=-0.1959 S TURB S SEP CD 1.0053 0.0168 0.0101 0.9560 0.0000 0.0043 CL= 0.512 CD=0.01440 CL= 0.298 CD=0.01243
CM=-0.1945
S TORB S SEP CD
0.7170 0.0144 0.0082
0.8708 0.0000 0.0043
CL= 0.405 CD=0.01249
CM=-0.1960
S TURB S SEP CD
0.7441 0.0160 0.0088
0.8303 0.0000 0.0038
CL= 0.513 CD=0.01266
CM=-0.1975
S TORB S SEP CD
0.7761 0.0178 0.0096
0.7881 0.0000 0.0034
CL= 0.620 CD=0.01300
CM=-0.1988
S TORB S SEP CD 0.9560 0.0000 0.0043 CL= 0.512 CD=0.01440 CM=-0.1973 S TURB S SEP CD 1.0053 0.0186 0.0109 0.9560 0.0000 0.0039 CL= 0.619 CD=0.01479 CM=-0.1986 TOTAL CL= 0.512 CD=0.00856 CM=-0.1973 -1.00 S TURB S SEP CD UPPER 0.3678 0.0168 0.0059* LOWER 0.6358 0.0000 0.0030*
TOTAL CL= 0.621 CD=0.00891
CM=-0.1991 CM=-0.1986
S TURB S SEP CD
1.0053 0.0206 0.0117
0.9560 0.0000 0.0036
CL= 0.725 CD=0.01528
CM=-0.1998
S TURB S SEP CD
1.0053 0.0228 0.0126
0.9560 0.0000 0.0033
CL= 0.831 CD=0.01591
CM=-0.2009
S TURB S SEP CD CM=-0.1988
S TURB S SEP CD
0.8052 0.0196 0.0104
0.7521 0.0000 0.0031
CL= 0.727 CD=0.01349
CM=-0.2001
S TURB S SEP CD
0.8380 0.0217 0.0114
0.7243 0.0000 0.0028
CL= 0.833 CD=0.01415
CM=-0.2012
S TURB S SEP CD CM=-0.2019
S TURB S SEP CD
1.0053 0.0251 0.0136
0.9560 0.0000 0.0030
CL= 0.937 CD=0.01663
CM=-0.2018
S TURB S SEP CD
1.0053 0.0277 0.0147
0.9560 0.0000 0.0028
CL= 1.042 CD=0.01747
CM=-0.2026
S TURB S SEP CD
1.0053 0.0000 0.0025
CL= 1.046 CD=0.01844
CM=-0.2032
S TURB S SEP CD S TURB S SEP CD 0.8683 0.0240 0.0124 0.7031 0.0000 0.0025 CL= 0.938 CD=0.01496 0.7031 0.0000 0.0025
CL= 0.938 CD=0.01496
CM=-0.2022
S TURB S SEP CD
0.8985 0.0266 0.0136
0.6843 0.0000 0.0023
CM=-0.2030
S TURB S SEP CD
0.9262 0.0296 0.0149
0.6679 0.0000 0.0022
CL= 1.148 CD=0.01705
CM=-0.2036
S TURB S SEP CD
0.9527 0.0302 0.0164
0.6495 0.0000 0.0020
CL= 1.251 CD=0.01838
CM=-0.2040
S TURB S SEP CD
0.9768 0.0368 0.0181
0.6296 0.0000 0.0018
CL= 1.353 CD=0.01994
CM=-0.2041 3.00 S TURB S SEP CD UPPER 0.5746 0.0228 0.0094* LOWER 0.5453 0.0000 0.0023* TOTAL CLE 1.049 CD=0.01170

CM=-0.2042
4.00 S TURB S SEP CD

UPPER 0.6218 0.0251 0.0105*

LOWER 0.5326 0.0000 0.0021*
TOTAL CLE 1.154 CD=0.01261

CM=-0.2051 CM=-0.2051
5.00 STURE SSEP CD
UPPER 0.6736 0.0278 0.0119*
LOWER 0.5198 0.0000 0.0019*
TOTAL CLE 1.259 CD=0.01381
CM=-0.2058
6.00 STURE SSEP CD
UPPER 0.7356 0.0311 0.0135*
LOWER 0.5051 0.0000 0.0018*
TOTAL CLE 1.362 CD=0.01528 S TURB S SEP CD 1.0053 0.0340 0.0172 0.9560 0.0000 0.0023 CL= 1.249 CD=0.01956 CM=-0.2036 S TURB S SEP CD 1.0053 0.0376 0.0187 1.0053 0.0376 0.0187 0.9560 0.0000 0.0021 CL= 1.352 CD=0.02082 CM=-0.2038 S TURB S SEP CD 1.0053 0.0398 0.0195 0.9560 0.0000 0.0020 CL= 1.408 CD=0.02159 CL= 1.362 CD=0.01528 CM=-0.2061 6.55 CL= 1.408 CD=0.02159 CM=-0.2038 S TURB S SEP CD 0.9921 0.0402 0.0195 0.6131 0.0000 0.0017 6.75

CL= 1.428 CD=0.02126 CM=-0.2039

7.00 S TURB S SEP CD
UPPER 0.8382 0.0364 0.0165*
LOWER 0.4890 0.0000 0.0016*
TOTAL CLE 1.462 CD=0.01808
CM=-0.2056
7.43 S TURB S SEP CD
UPPER 0.9310 0.0413 0.0195*
LOWER 0.4822 0.0000 0.0015*
TOTAL CLE 1.500 CD=0.02099
CM=-0.2044

49

ALPHA(DEG.) R= 600000 MU=300 1.83 S TURB S SEP CD UPPER 0.0853 0.0511 0.0032* LOWER 1.0110 0.0000 0.0081* TOTAL CL=-0.045 CD=0.01125 CM=-0.1815 5.00 S TURB S SEP CD UPPER 0.0891 0.0514 0.0033* LOWER 0.7872 0.0000 0.0048*
TOTAL CL= 0.044 CD=0.00801
CM=-0.1826 TOTAL CLE - 0.1826

-5.00 S TURB S SEP CD
UPPER 0.1440 0.0257 0.0034
LOWER 0.7293 0.0000 0.0041*
TOTAL CLE 0.176 CD00.00748

-4.00 S TURB S SEP CD
UPPER 0.2104 0.0170 0.0039
LOWER 0.7021 0.0000 0.0038*
TOTAL CLE 0.294 CD00.00765
CM=-0.1935

-3.00 S TURB S SEP CD
UPPER 0.2668 0.0151 0.0044
LOWER 0.6831 0.0000 0.0035*
TOTAL CLE 0.495 CD=0.00765
CM=-0.1958

-2.00 S TURB S SEP CD
UPPER 0.3174 0.0147 0.0049
LOWER 0.6629 0.0000 0.0031*
TOTAL CLE 0.514 CD=0.00807 TOTAL CL= 0.514 CD=0.00807 CM=-0.1978 1.00 S TURB S SEP CD UPPER 0.3678 0.0154 0.0056 LOWER 0.6358 0.0000 0.0028* TOTAL CL= 0.623 CD=0.00837 CM=-0.1995 0.00 S TURB S SEP CD UPPER 0.603 CM-0.1995
0.00 S TURB S SEP CD UPPER 0.4188 0.0165 0.0063*
LOWER 0.6082 0.0000 0.0026*
TOTAL CLE 0.731 CD-0.00881
CM-0.2010
1.00 S TURB S SEP CD UPPER 0.4697 0.0179 0.0070*
LOWER 0.5809 0.0000 0.0023*
TOTAL CLE 0.838 CD-0.00936
CM-0.2024
2.00 S TURB S SEP CD UPPER 0.5223 0.0196 0.0079*
LOWER 0.5599 0.0000 0.0022*
TOTAL CLE 0.938 CD-0.0003
TOTAL CLE 0.938 CD-0.0033
0.00 S TURB S SEP CD UPPER 0.5223 0.0196 0.0079*
LOWER 0.5599 0.0000 0.0022*
TOTAL CLE 0.944 CD-0.01015
CM-0.2036
3.00 S TURB S SEP CD 0.00 CM=-0.2036 3.00 S TURB S SEP CD UPPER 0.5746 0.0216 0.0089* LOWER 0.5453 0.0000 0.0021* TOTAL CL= 1.051 CD=0.01099 3,00 TOTAL CL= 1.01 (D=0.01099 CM=-0.2047 4.00 S TURB S SEP CD UPPER 0.6218 0.0238 0.0100* LOWER 0.5326 0.0000 0.0019* TOTAL CL= 1.156 CD=0.01193 CM=-0.2056 CM=-U.2056
5.00 S TURB S SEP CD
UPPER 0.6736 0.0264 0.0113*
LOWER 0.5198 0.0000 0.0018*
TOTAL CL= 1.261 CD=0.01305
CM=-0.2062 CM=-0.2062 6.00 S TURB S SEP CD UPPER 0.7356 0.0297 0.0129* LOWER 0.5051 0.0000 0.0017* TOTAL CL= 1.364 CD=0.01452 CM=-0.2066 6.64 6.78

R= 600000 MU=100 R= 600000 MU=900 S TURB S SEP CD 1.0037 0.0085 0.0070 1.0110 0.0000 0.0081* S TURB S SEP CD 0.6277 0.0083 0.0059 1.0110 0.0000 0.0081* CL=-0.007 CD=0.01401 CM=-0.1900 S TURB S SEP CD CL=-0.008 CD=0.01510 CM=-0.1900 CM=-0.1900 S TURB S SEP CD 1.0037 0.0096 0.0074 0.9560 0.0000 0.0061* CL= 0.082 CD=0.01355 CM=-0.1914 0.6522 0.0094 0.0063 0.9794 0.0000 0.0063 CL= 0.083 CD=0.01259 CM=-0.1915 CH=-0.1914
S TURB S SEP CD
1.0037 0.0111 0.0080
0.9560 0.0000 0.0054
CL= 0.190 CD=0.01337
CM=-0.1930
S TURB S SEP CD
1.0053 0.0126 0.0085
0.9560 0.0000 0.0050
CL= 0.298 CD=0.01352
CM=-0.1946
S TURB S SEP CD
1.0053 0.0142 0.0092
0.9560 0.0000 0.0045
CL= 0.298 CD=0.01350
CM=-0.1946
S TURB S SEP CD
1.0053 0.0142 0.0092
0.9560 0.0000 0.0045
CL= 0.406 CD=0.01370
CM=-0.1961
S TURB S SEP CD
1.0053 0.0159 0.0098
0.9560 0.0000 0.0042
L= 0.513 CD=0.01339 CM=-0.1915
S TURB S SEP CD
0.6784 0.0107 0.0068
0.9525 0.0000 0.0054
CL= 0.191 CD=0.01221
CM=-0.1931
S TURB S SEP CD
0.7061 0.0121 0.0074
0.9171 0.0000 0.0048
CL= 0.299 CD=0.01215
CM=-0.1947
S TURB S SEP CD CM=-0.1947 S TURB S SEP CD 0.7345 0.0136 0.0080 0.8820 0.0000 0.0042 CL= 0.406 CD=0.01222 CM=-0.1962 S TURB S SEP CD 0.7609 0.0152 0.0086 0.7609 0.0152 0.0086 0.8439 0.0000 0.0038 CL= 0.514 CD=0.01239 CM=-0.1977 S TURB S SEP CD 0.7923 0.0169 0.0094 0.8045 0.0000 0.0033 CL= 0.621 CD=0.01273 CM=-0.1990 C TURB S SEP CD 0.9560 0.0000 0.0042 CL= 0.513 CD=0.01399 CM=-0.1975 S TURB S SEP CD 1.0053 0.0177 0.0106 0.9560 0.0000 0.0038 CL= 0.620 CD=0.01437 CM=-0.1988 CM=-0.1988
S TURB S SEP CD
1.0053 0.0197 0.0114
0.9560 0.0000 0.0035
CL= 0.726 CD=0.01485
CM=-0.2000
S TURB S SEP CD
1.0053 0.0218 0.0123
0.9560 0.0000 0.0032
CL= 0.833 CD=0.01545
CM=-0.2012
S TURB S SEP CD S TURB S SEP CD 0.8207 0.0188 0.0102 0.7673 0.0000 0.0030 CL= 0.728 CD=0.01319 CM=-0.2003 S TURB S SEP CD 0.8519 0.0209 0.0111 0.7365 0.0000 0.0027 CL= 0.834 CD=0.01382 CM=-0.2015 CM=-0.2012
S TURB S SEP CD
1.0053 0.0242 0.0132
0.9560 0.0000 0.0029
CL= 0.938 CD=0.01615
CM=-0.2021
S TURB S SEP CD
1.0053 0.0267 0.0143
0.9560 0.0000 0.0027
CL= 1.043 CD=0.01696
CM=-0.2029
S TURB S SEP CD
1.0053 0.0296 0.0154
0.9560 0.0000 0.0025
CL= 1.148 CD=0.01789
CM=-0.2018
S TURB S SEP CD CM=-0.2015 S TURE S SEP CD 0.8805 0.0231 0.0121 0.7139 0.0000 0.0025 CL= 0.940 CD=0.01459 CM=-0.2025 S TURB S SEP CD 0.9087 0.0257 0.0132 0.6941 0.0000 0.0023 0.0941 0.0000 0.0023 CL= 1.045 CD=0.01552 CM=-0.2033 S TURB S SEP CD 0.9349 0.0286 0.0145 0.6774 0.0000 0.0021 CL= 1.149 CD=0.01661 CM=-0.2039 CM=-0.2039
S TURB S SEP CD
0.9596 0.0319 0.0160
0.6600 0.0000 0.0019
CL= 1.252 CD=0.01788
CM=-0.2043
S TURB S SEP CD
0.9820 0.0358 0.0176
0.6414 0.0000 0.0018 S TURB S SEP CD 1.0053 0.0328 0.0167 0.9560 0.0000 0.0023 U.5580 U.0000 U.0023 CL= 1.251 CD=0.01896 CM=-0.2040 S TURB S SEP CD 1.0053 0.0364 0.0181 0.9560 0.0000 0.0021 CL= 1.354 CD=0.02017 CM=-0.2042 CL= 1.355 CD=0.01938 CM=-0.2044 CM=-0.2042 S TURB S SEP CD 1.0053 0.0389 0.0190 0.9560 0.0000 0.0020 CL= 1.419 CD=0.02102

> S TURB S SEP CD 0.9967 0.0392 0.0190 0.6252 0.0000 0.0017 CL= 1.433 CD=0.02071 CM=-0.2043

7.00 S TURB S SEP CD
UPPER 0.8382 0.0350 0.0157*
LOWER 0.4890 0.0000 0.0015*
TOTAL CLE 1.464 CD=0.01722
CM=-0.2061
7.49 S TURB S SEP CD
UPPER 0.9423 0.0404 0.0190*
LOWER 0.4812 0.0000 0.0014*
TOTAL CLE 1.508 CD=0.02041
CM=-0.2048

CM=-0.2042

R= 700000 MU=900 S TURB S SEP CD 0.6446 0.0076 0.0058 1.0110 0.0000 0.0078* CL=-0.007 CD=0.01367 CM=-0.1902 ALPHA(DEG.) R= 700000 MU=300 R= 700000 MU=100 6.83 S TURB S SEP CD UPPER 0.0853 0.0494 0.0029* LOWER 1.0110 0.0000 0.0078* S TURB S SEP CD 1.0037 0.0078 0.0068 UPER 0.0853 0.0494 0.0029*
LOWER 1.0110 0.0000 0.0078*
TOTAL CL=-0.044 CD=0.01074
CM=-0.1818

-6.00 S TURB S SEP CD
UPER 0.0906 0.0476 0.0029*
LOWER 0.7872 0.0000 0.0046*
TOTAL CL= 0.047 CD=0.00748
CM=-0.1834

-5.00 S TURB S SEP CD
UPER 0.1685 0.0181 0.0033
LOWER 0.7293 0.0000 0.0039*
TOTAL CL= 0.183 CD=0.00719
CM=-0.1914

-4.00 S TURB S SEP CD
UPER 0.2311 0.0137 0.0038
LOWER 0.7021 0.0000 0.0036*
TOTAL CL= 0.297 CD=0.00736
CM=-0.1943

-3.00 S TURB S SEP CD
UPER 0.2850 0.0127 0.0043
LOWER 0.6831 0.0000 0.0035*
TOTAL CL= 0.407 CD=0.00755
CM=-0.1965

-2.00 S TURB S SEP CD
UPER 0.3336 0.0132 0.0043
LOWER 0.6631 0.0000 0.0033*
TOTAL CL= 0.629 0.0000 0.0038*
TOTAL CL= 0.629 0.0000 0.0038*
TOTAL CL= 0.629 0.0000 0.0038*
TOTAL CL= 0.6529 0.0000 0.0038*
TOTAL CL= 0.6529 0.0000 0.0038*
TOTAL CL= 0.516 CD=0.00780 1.0110 0.0000 0.0078* CL=-0.007 CD=0.01469 CM=-0.1902 S TURB S SEP CD 1.0037 0.0089 0.0073 0.9560 0.0000 0.0059* CL= 0.083 CD=0.01316 CM=-0.1916 S TURB S SEP CD 1.0037 0.0103 0.0078 0.9560 0.0000 0.0053 CL= 0.191 CD=0.01303 1.0110 0.0000 0.0078* CLE-0.007 (201, 0138) CM=-0.1902 SF CD .0180 SF CD .0683 0.0087 0.0062 0.9820 0.0000 0.0061 CLE 0.083 CD=0.01233 CM=-0.1916 S TURB S SEP CD 0.6943 0.0100 0.0053 CLE 0.191 CD=0.01197 CM=-0.1933 S TURB S SEP CD 0.7213 0.0114 0.0072 0.9238 0.0000 0.0047 CLE 0.299 CD=0.01193 CM=-0.1949 S STURB S SEP CD STURB S SEP CD 0.7213 0.0000 0.0047 CLE 0.299 CD=0.01193 CM=-0.1949 S STURB S SEP CD 0.9560 0.0000 0.0053 CL= 0.191 CD=0.01303 CM=-0.1932 S TURB S SEP CD 1.0053 0.0118 0.0083 0.9560 0.0000 0.0049 CL= 0.299 CD=0.01319 CM=-0.1948 CLE 0.299 CDE-0.01193
CME-0.1949
S TURB S SEP CD
0.7489 0.0129 0.0078
0.8908 0.0000 0.0041
CLE 0.407 CDE-0.01199
CME-0.1964
S TURB S SEP CD
0.7750 0.0145 0.0085
0.8545 0.0000 0.0037
CLE 0.515 CDE-0.01217
CME-0.1979
S TURB S SEP CD
0.8054 0.0162 0.0092
0.8178 0.0000 0.0033
CLE 0.622 CDE-0.01251
CME-0.1992
S TURB S SEP CD
0.8332 0.0181 0.0100
0.7805 0.0000 0.0033
CLE 0.622 CDE-0.01295
CME-0.1992
S TURB S SEP CD
0.8332 0.0181 0.0100
0.7805 0.0000 0.0033
CLE 0.729 CDE-0.01295
CME-0.2005
S TURB S SEP CD
0.8631 0.0201 0.0109
0.7476 0.0000 0.0027
CLE 0.835 CDE-0.01355
CME-0.2017
S TURB S SEP CD CL= 0.299 CD=0.01319
CM=-0.1948
S TURB S SEP CD
1.0053 0.0134 0.0089
0.9560 0.0004 0.0044
CL= 0.407 CD=0.01337
CM=-0.1963
S TURB S SEP CD
1.0053 0.0152 0.0096
0.9560 0.0000 0.0041
CL= 0.514 CD=0.01366
CM=-0.1977
S TURB S SEP CD
1.0053 0.0170 0.0103
CM=-0.0950 0.0000 0.0037
CL= 0.621 CD=0.01403
CM=-0.1990
S TURB S SEP CD
1.0053 0.0170 0.0103
CM=-0.1990
S TURB S SEP CD
1.0053 0.0000 0.0037
CL= 0.621 CD=0.01403
CM=-0.1990
S TURB S SEP CD
1.0053 0.0189 0.0111
0.9560 0.0000 0.0034
CL= 0.727 CD=0.01450 LOWER 0.6629 0.0000 0.0030*
TOTAL CL= 0.516 CD=0.00780
CM=-0.1982
-1.00 S TURB S SEP CD
UPPER 0.3796 0.0142 0.0054
LOWER 0.6358 0.0000 0.0027*
TOTAL CL= 0.624 CD=0.00808
CM=-0.1998
0.00 S TURB S SEP CD
UPPER 0.4245 0.0155 0.0060
LOWER 0.6082 0.0000 0.0024*
TOTAL CL= 0.732 CD=0.00846 0.9560 0.0000 0.0034 CL= 0.727 CD=0.01450 CM=-0.2003 S TURB S SEP CD 1.0053 0.0210 0.0120 0.9560 0.0000 0.0031 CL= 0.834 CD=0.01508 CM=-0.2014 S TURB S SEP CD CL= 0.835 CD=0.01355
CM=-0.2017
S TURB S SEP CD
0.8900 0.0224 0.0119
0.7236 0.0000 0.0024
CL= 0.941 CD=0.01430
CM=-0.2027
S TURB S SEP CD
0.9167 0.0249 0.0130
0.7029 0.0000 0.0022
CL= 1.046 CD=0.01519
CM=-0.2035
S TURB S SEP CD
0.9418 0.0278 0.0142
0.6857 0.0000 0.0020
CL= 1.046 CD=0.01625
CM=-0.2042
S TURB S SEP CD
0.9458 0.0310 0.0120
CL= 1.150 CD=0.01625
CM=-0.2042
S TURB S SEP CD
0.9650 0.0311 0.0156
0.6683 0.0000 0.0019
CL= 1.254 CD=0.01748
CM=-0.2046
S TURB S SEP CD
0.9860 0.0349 0.0172
0.6510 0.0000 0.0017
CL= 1.356 CD=0.01893
CM=-0.2047 CM=-0.2014
S TURB S SEP CD
1.0053 0.0234 0.0129
0.9560 0.0000 0.0029
CL= 0.939 CD=0.01576
CM=-0.2024
S TURB S SEP CD
1.0053 0.0259 0.0139
0.9560 0.0000 0.0026
CL= 1.044 CD=0.01654
CM=-0.2032
S TURB S SEP CD
1.0053 0.0287 0.0150
0.9560 0.0000 0.0024
CL= 1.149 CD=0.01744
CM=-0.2039
S TURB S SEP CD
1.0053 0.0319 0.0162
0.9560 0.0000 0.0022
CL= 1.255 CD=0.01847 TOTAL CLE 1.052 CD=0.01049

CM=-0.2050
4.00 S TURB S SEP CD
UPPER 0.6218 0.0227 0.0096*
LOWER 0.5326 0.0000 0.0018*
TOTAL CLE 1.158 CD=0.01140
CM=-0.2059
5.00 S TURB S SEP CD CM=-0.2059 CD-0.0110 CM=-0.2059 CD-0.0110 CM=-0.2059 CD-0.0108* LOWER 0.5198 0.0000 0.0017* TOTAL CLE 1.262 CD-0.01247 CM=-0.2066 CM-0.7356 0.0285 0.0124* LOWER 0.7356 0.0285 0.0124* LOWER 0.5051 0.0000 0.0016* TOTAL CLE 1.366 CD=0.01392 CM=-0.2070 0.9560 0.0000 0.0022 CL= 1.252 CD=0.01847 CM=-0.2043 S TURE S SEP CD 1.0053 0.0354 0.0176 0.9560 0.0000 0.0020 CL= 1.355 CD=0.01964 CM=-0.2046 S TURE S SEP CD 1.0053 0.0381 0.0186 0.9560 0.0000 0.0019 CL= 1.428 CD=0.02057 6.72 CL= 1.428 CD=0.02057 CM=-0.2046 S TURB S SEP CD 1.0003 0.0383 0.0186 0.6350 0.0000 0.0016 6.81 7.00 S TURE S SEP CD
UPPER 0.8382 0.0337 0.0151*
LOWER 0.4890 0.0000 0.0014*
TOTAL CL= 1.466 CD=0.01656
CM=-0.2066

CM=-0.2066
7.54 S TURB S SEP CD
UPPER 0.9491 0.0396 0.0186*
LOMER 0.4804 0.0000 0.0014*
TOTAL CL= 1.515 CD=0.01993
CM=-0.2052

CL= 1.438 CD=0.02027 CM=-0.2046

ALPHA (DEG.) R= 800000 MU=300 PHA(DEG.) R= 800000 MU=300 6.83 S TURB S SEP CD UPPER 0.0853 0.0478 0.0027* LOWER 1.0110 0.0000 0.0076* TOTAL CL=-0.042 CD=0.01030 CM=-0.1821 CM=-0.1821

-6.00 S TURB S SEP CD

UPPER 0.1134 0.0284 0.0027

LOWER 0.7872 0.0000 0.0044*

TOTAL CL= 0.065 CD=0.00710

CM=-0.1873

-5.00 S TURB S SEP CD

UPPER 0.1890 0.0136 0.0032

LOWER 0.7293 0.0000 0.0038* LOWER 0.7293 0.0000 0.0038*
TOTAL CLE 0.188 CD=0.00698
CM=-0.1924
4.00 S TURE S SEP CD
UPPER 0.2487 0.0115 0.0037
LOWER 0.7021 0.0000 0.0034*
TOTAL CLE 0.299 CD=0.00715
CM=-0.1949 TOTAL CL= 0.299 CD=0.00715 CM=0.1949 -3.00 S TURB S SSP CD UPPER 0.3006 0.0113 0.0042 CM=0.1949 CD=0.00734 CM=0.195 CM=0 LOMER 0.6082 0.0000 0.0023*
TOTAL CLE 0.733 CD-0.00826
CM=-0.2016
1.00 S TURB S SEP CD
UPPER 0.4819 0.0161 0.0066
LOWER 0.5809 0.0000 0.0021*
CM=-0.2029 0.0873
CM=-0.2029 CD TOTAL CL= 0.840 CD=0.00873 CM=-0.2029 2.00 S TURB S SEP CD UPPER 0.5261 0.0178 0.0073 CM=-0.2042 CM=-0.2053 CM=-0.2054 CM=-0.2074 CM 6.75 6.80

R= 800000 MU=100 S TURB S SEP CD 1.0037 0.0071 0.0067 1.0110 0.0000 0.0076* CL=-0.006 CD=0.01434 CM=-0.1903 CM=-0.1903
S TURB S SEP CD
1.0037 0.0083 0.0071
0.9560 0.0000 0.0057*
CL= 0.084 CD=0.01285
CM=-0.1917
S TURB S SEP CD
1.0037 0.0097 0.0076
0.9560 0.0000 0.0051
CL= 0.192 CD=0.01275
CM=-0.1933
S TURB S SEP CD
1.0053 0.0112 0.0082
0.9560 0.0000 0.0047
CL= 0.300 CD=0.01291
CM=-0.1949
S TURB S SEP CD CM=-0.1949

S TURB S SEP CD
1.0053 0.0128 0.0088
0.9560 0.0000 0.0043
CL= 0.407 CD=0.01310
CM=-0.1964
S TURB S SEP CD
1.0053 0.0145 0.0094
0.9560 0.0000 0.0040
CL= 0.515 CD=0.01337
CM=-0.1979
S TURB S SEP CD
1.0053 0.0163 0.0104
0.9560 0.0000 0.0036
CL= 0.622 CD=0.01374
CM=-0.1979
S TURB S SEP CD
1.0053 0.0163 0.0103
CL= 0.622 CD=0.01374
CM=-0.1992
S TURB S SEP CD
1.0053 0.0183 0.0109
0.9560 0.0000 0.0033
CL= 0.728 CD=0.01421
CM=-0.2005
S TURB S SEP CD
1.0053 0.0204 0.017
0.9560 0.0000 0.0031
CL= 0.835 CD=0.01477
CM=-0.2016
S TURB S SEP CD
1.0053 0.0226 0.0126
0.9560 0.0000 0.0028
CL= 0.940 CD=0.01543
CM=-0.2026
S TURB S SEP CD
1.0053 0.0226 0.0126
0.9560 0.0000 0.0028
CL= 0.940 CD=0.01543
CM=-0.2026
S TURB S SEP CD
1.0053 0.0279 0.0147
0.9560 0.0000 0.0022
CL= 1.046 CD=0.01619
CM=-0.2035
S TURB S SEP CD
1.0053 0.0279 0.0147
0.9560 0.0000 0.0022
CL= 1.150 CD=0.01706
CM=-0.2041
S TURB S SEP CD
1.0053 0.0311 0.0159
0.9560 0.0000 0.0022
CL= 1.254 CD=0.01806
CM=-0.2046
S TURB S SEP CD
1.0053 0.0345 0.0172
0.9560 0.0000 0.0022
CL= 1.257 CD=0.01919
CM=-0.2049 S TURB S SEP CD 1.0053 0.0373 0.0182 0.9558 0.0000 0.0019 CL= 1.433 CD=0.02013 CM=-0.2049

R= 800000 MU=900 S TURB S SEP CD 0.6588 0.0070 0.0057 1.0110 0.0000 0.0076* CL=-0.006 CD=0.01337 CM=-0.1903 CL=-0.006 CD=-0.01337
CM=-0.1903
S TURE S SEP CD
0.6820 0.0081 0.0061
0.9841 0.0000 0.0060
CL= 0.084 CD=-0.01211
CM=-0.1918
S TURE S SEP CD
0.7079 0.0094 0.0066
0.9506 0.0000 0.0052
CL= 0.192 CD=-0.01178
CM=-0.1934
S TURE S SEP CD
0.7342 0.0108 0.0071
0.9292 0.0000 0.0046
CL= 0.300 CD=-0.0174
CM=-0.1950
S TURE S SEP CD
0.7609 0.0123 0.0077
0.7609 0.0123 0.0071
0.7609 0.0123 0.0071
0.7609 0.0123 0.0071
0.7609 0.0123 0.0071
0.7609 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0123 0.0071
0.7509 0.0139 0.0084
0.7509 0.0139 0.0084
0.7509 0.0139 0.0084
0.7509 0.0139 0.0084
0.7509 0.0139 0.0084 CM=-0.1981
S TURB S SEP CD
0.8169 0.0156 0.0091
0.8285 0.0000 0.0032
CL= 0.622 CD=0.01232
CM=-0.1994
S TURB S SEP CD
0.8435 0.0175 0.0098
0.7920 0.0000 0.0029
CL= 0.729 CD=0.01276
CM=-0.2007
S TURB S SEP CD CM=-0.2007
S TURB S SEP CD
0.8723 0.0195 0.0107
0.7581 0.0000 0.0026
CL= 0.836 CD=0.01334
CM=-0.2019
S TURB S SEP CD
0.8979 0.0217 0.0117
0.7323 0.0000 0.0024 0.8979 0.0217 0.0117 0.7323 0.0000 0.0024 CL= 0.942 CD=0.01405 CM=-0.2029 CD=0.2024 0.0127 0.7029 0.0000 0.0022 CL= 1.047 CD=0.01491 CM=-0.2038 STURE SEP CD 0.9473 0.0271 0.0139 0.6930 0.0000 0.0020 CL= 1.151 CD=0.01594 CM=-0.2044 STURE SEP CD 0.9693 0.0303 0.0153 0.6755 0.0000 0.0019 CL= 1.255 CD=0.01714 CM=-0.2049 STURE SEP CD 0.9693 0.0303 0.0153 TURE SEP CD 0.9694 0.0001 0.0019 CL= 1.255 CD=0.01714 CM=-0.2049 STURE SEP CD 0.9894 0.0341 0.0168 0.6589 0.0000 0.0017 CL= 1.357 CD=0.01856 CM=-0.2050

S TURB S SEP CD 1.0026 0.0374 0.0182 0.6442 0.0000 0.0016 CL= 1.438 CD=0.01984 CM=-0.2049

7.00 S TURB S SEP CD UPPER 0.8382 0.0327 0.0146* LOWER 0.4890 0.0000 0.0014* TOTAL CLE 1.468 CD=0.01601 CM=-0.2070 7,56 S TURB S SEP CD UPPER 0.9533 0.0388 0.0182* LOWER 0.4800 0.0000 0.0013* TOTAL CL= 1.518 CD=0.01953 CM=-0.2055

ALPHA (DEG.) R= 900000 MU=300 R= 900000 MU=900 S TURB S SEP CD 0.6711 0.0064 0.0057 1.0110 0.0000 0.0075* R= 900000 MU=100 6.83 S TURB S SEP CD UPPER 0.0853 0.0464 0.0025* LOWER 1.0110 0.0000 0.0075* S TURB S SEP CD 1.0037 0.0066 0.0066 1.0110 0.0000 0.0075* 1.0110 0.0000 0.0075
CL=-0.006 CD=0.01312
CM=-0.1905
S TURB S SEP CD
0.6944 0.0075 0.0061
0.9859 0.0000 0.0059
CL= 0.084 CD=0.01193
CM=-0.1919
CM=-0.1919
CME-0.1919
CME-0.1919 TOTAL CL=-0.041 CD=0.00994 CM=-0.1824 6.00 S TURB S SEP CD UPPER 0.1375 0.0183 0.0027 CL=-0.006 CD=0.01404 CL=-0.006 CD=0.01404 CM=-0.1904 S TURB S SEP CD 1.0037 0.0077 0.0070 0.9560 0.0000 0.0056* CL= 0.084 CD=0.01258 CM=-0.1918 UPPER 0.1375 0.0183 0.0027 LOWER 0.7872 0.0000 0.0043* TOTAL CL= 0.074 CD=0.00693 CM=-0.1895 SEP CD UPPER 0.2066 0.0109 0.0031 LOWER 0.7293 0.0000 0.003* TOTAL CL= 0.191 CD=0.00681 CM=-0.1931 CM=-0.1918
S TURB S SEP CD
1.0037 0.0091 0.0075
0.9560 0.0000 0.0051
CL= 0.192 CD=0.01258
CM=-0.1935
S TURB S SEP CD
1.0053 0.0106 0.0080
0.9560 0.0000 0.0047
CL= 0.300 CD=0.01267
CM=-0.1951
S TURB S SEP CD
1.0053 0.0122 0.0086
0.9560 0.0000 0.0047
CL= 0.308 CD=0.01286
CM=-0.1966
S TURB S SEP CD
1.0053 0.0129 0.01286
CM=-0.1966
S TURB S SEP CD
1.0053 0.0139 0.0092
0.9560 0.0000 0.0033
CM=0.515 CD=0.01313 CH=-0.1919 S TURB S SEP CD 0.7196 0.0088 0.0065 0.9636 0.0000 0.0052 CL= 0.193 CD=0.01168 CM=-0.1936 S TURB S SEP CD 0.7454 0.0102 0.0071 0.9336 0.0000 0.0045 CL= 0.301 CD=0.01158 CM=-0.1952 S TURB S SEP CD 0.7716 0.0117 0.0076 0.9039 0.0000 0.0046 CL= 0.408 CD=0.01165 CM=-0.1952 S TURB S SEP CD 0.7716 0.0117 0.0076 0.9039 0.0000 0.0046 CL= 0.408 CD=0.01165 CM=-0.1967 S TURB S SEP CD 0.7975 0.0133 0.0082 0.8707 0.0000 0.0036 CL= 0.516 CD=0.01183 -5.00 CM=-0.1931 4.00 S TURB S SEP CD UPPER 0.2640 0.0101 0.0037 LOWER 0.7021 0.0000 0.0033* LOWER 0.7021 0.0000 0.0033**
TOTAL CLE 0.301 CD-0.0698
CM=-0.1952
3.00 S TURB S SEP CD
UPPER 0.3141 0.0104 0.0041
LOWER 0.6831 0.0000 0.0030**
CM=-0.1971
CM=-0.1971
CM=-0.1971
CM=-0.1971 TOTAL CL= 0.410 CD=0.00715 CM=0.01715 CM=0.1971
-2.00 S TURB S SEP CD UPPER 0.3603 0.0114 0.0027*
TOTAL CL= 0.518 CD=0.00741 CM=0.1987
-1.00 S TURB S SEP CD UPPER 0.4049 0.0126 0.0052 LOWER 0.6358 0.0000 0.0025*
TOTAL CL= 0.626 CD=0.00770 CM=0.2030 0.00 S TURB S SEP CD UPPER 0.4490 0.0139 0.0058 LOWER 0.6082 0.0000 0.0023*
TOTAL CL= 0.734 CD=0.00809 CM=0.2018 S CD UPPER 0.4490 0.0139 0.0058 LOWER 0.5082 0.0000 0.0023*
TOTAL CL= 0.734 CD=0.00809 CM=0.2018 S CD UPPER 0.4490 0.0155 0.0065 LOWER 0.5089 0.0000 0.0021*
TOTAL CL= 0.841 CD=0.00856 CM=0.2031 0.0055 0.0065 0.8707 0.0000 0.0036 CL= 0.516 CD=0.01183 CM=-0.1982 S TURB S SEP CD 0.8267 0.0151 0.0090 0.8373 0.0000 0.0032 CL= 0.623 CD=0.01217 CM=-0.1996 CL= 0.515 CD=0.01313 CM=-0.1980 S TURB S SEP CD 1.0053 0.0157 0.0099 0.9560 0.0000 0.0036 CL= 0.622 CD=0.01349 CM=-0.1994 CL= 0.823 CD=0.01217
CM=-0.1996
S TURB S SEP CD
0.8522 0.0169 0.0097
0.8022 0.0000 0.0029
CL= 0.730 CD=0.01259
CM=-0.2009
S TURB S SEP CD
0.8799 0.0189 0.0106
0.7678 0.0000 0.0026
CL= 0.836 CD=0.01315
CM=-0.2020
S TURB S SEP CD
0.9046 0.0212 0.0115
0.7406 0.0000 0.0024
CL= 0.942 CD=0.01384
CM=-0.2031 CM=-0.1994
S TURB S SEP CD
1.0053 0.0177 0.0107
0.9560 0.0000 0.0033
CL= 0.729 CD=0.01396
CM=-0.2006
S TURB S SEP CD
1.0053 0.0197 0.0115
0.9560 0.0000 0.0030 0.9560 0.0000 0.0030 CL= 0.835 CD=0.01450 CM=-0.2018 S TURE S SEP CD 1.0053 0.0220 0.0124 0.9560 0.0000 0.0028 CL= 0.941 CD=0.01514 CM=-0.2028 S TURE S SEP CD 1.0053 0.0245 0.0133 0.9560 0.0000 0.0025 CL= 1.046 CD=0.01589 TOTAL CLE 0.948 CD=0.00915

CM=-0.2044
3.00 S TURB S SEP CD

UPPER 0.5795 0.0190 0.0081

LOWER 0.5453 0.0000 0.0018*

TOTAL CLE 1.054 CD=0.00984

CM=-0.2055
4.00 S TURB S SEP CD

UPPER 0.6247 0.0211 0.0099

LOWER 0.5326 0.0000 0.0017*

TOTAL CLE 1.160 CD=0.01067

CM=-0.2065
5.00 S TURB S SEP CD

UPPER 0.6754 0.0237 0.0102

LOWER 0.5198 0.0000 0.0015*

TOTAL CLE 1.265 CD=0.01169

CM=-0.2072

6.00 S TURB S SEP CD S TURB S SEP CD 0.9288 0.0236 0.0125 0.7183 0.0000 0.0022 CL= 1.046 CD=0.01589 CM=-0.2037 S TURB S SEP CD 1.0053 0.0272 0.0144 0.9560 0.0000 0.0023 CL= 1.151 CD=0.01674 CM=-0.2044 0.7183 0.0000 0.0022 CL= 1.048 CD=0.01468 CM=-0.2040 S TURB S SEP CD 0.9520 0.0264 0.0137 0.6998 0.0000 0.0020 CL= 1.152 CD=0.01568 CM=-0.2046 CM=-0.2044
S TURB S SEP CD
1.0053 0.0303 0.0156
0.9560 0.0000 0.0022
CL= 1.255 CD=0.01771
CM=-0.2049
S TURB S SEP CD
1.0053 0.0337 0.0168
0.9560 0.0000 0.0020
CL= 1.358 CD=0.01881
CM=-0.2051
S TURB S SEP CD
1.0053 0.0368 0.0179
0.9559 0.0000 0.0019
CL= 1.440 CD=0.01979
CM=-0.2052 CM=-0.2046
S TURB S SEP CD
0.9730 0.0297 0.0150
0.6818 0.0000 0.0018
CL= 1.256 CD=0.01685
CM=-0.2051
S TURB S SEP CD
0.9922 0.0334 0.0166
0.6656 0.0000 0.0017
CL= 1.358 CD=0.01823
CM=-0.2053 CM=-0.2072
6.00 S TURB S SEP CD
UPPER 0.7356 0.0268 0.0116
LOWER 0.5051 0.0000 0.0014*
TOTAL CL= 1.369 CD=0.01308
CM=-0.2076 6.81 CM=-0.2052 S TURB S SEP CD 1.0050 0.0368 0.0179 0.6519 0.0000 0.0016 6.82 CL= 1.441 CD=0.01952 CM=-0.2052 7.00 S TURB S SEP CD
UPPER 0.8382 0.0318 0.0143
LOWER 0.4890 0.0000 0.0013*
TOTAL CLE 1.469 CD=0.01558
CM=-0.2073
7.59 S TURB S SEP CD
UPPER 0.9591 0.0382 0.0179*
LOWER 0.4795 0.0000 0.0012*
TOTAL CLE 1.522 CD=0.01917
CM=-0.2057

53

LPHA(DEG.) R= 1000000 MU=300
-6.83 S TURB S SEP CD
UPPER 0.0888 0.0401 0.0023*
LOWER 1.0110 0.0000 0.0073*
TOTAL CL.-0.035 CD=0.00956
-6.00 S TURB S SEP CD
UPPER 0.1563 0.0129 0.0026
LOWER 0.7872 0.0000 0.0042*
TOTAL CL.= 0.079 CD=0.00680
CM=-0.1907
-5.00 S TURB S SEP CD
UPPER 0.2221 0.0001 0.0031
LOWER 0.7293 0.0000 0.0036*
TOTAL CL.= 0.192 CD=0.00680
TOTAL CL.= 0.192 CD=0.00680 ALPHA (DEG.) R= 1000000 MH=300 R= 1000000 MU=100 R= 100000 M0=100 S TURB S SEP CD 1.0037 0.0060 0.0065 1.0110 0.0000 0.0073* CL=-0.005 CD=0.01377 CM=-0.1905 S TURB S SEP CD 1.0037 0.0072 0.0069 0.9560 0.0000 0.0055* CL= 0.085 CD=0.01235 CL= 0.085 CD=0.01235
CM=-0.1919
S TURE S SEP CD
1.0037 0.0086 0.0074
0.9560 0.0000 0.0050
CL= 0.193 CD=0.01237
CM=-0.1936
S TURE S SEP CD
1.0053 0.0101 0.0079
0.9560 0.0000 0.0046
CL= 0.301 CD=0.01246
CM=-0.1952
S TURE S SEP CD LOWER 0.7293 0.0000 0.0036*
TOTAL CLE 0.192 CD=0.00668
CM=-0.1935
4.00 S TURB S SEP CD
UPPER 0.2775 0.0088 0.0036
LOWER 0.7021 0.0000 0.0032*
TOTAL CLE 0.302 CD=0.00682
CM=-0.1955 S TURB S SEP CD 1.0053 0.0117 0.0085 0.9560 0.0000 0.0042 0.9560 0.0000 0.0042 CL= 0.408 CD=0.01265 CM=-0.1967 S TURB S SEP CD 1.0953 0.0134 0.0991 0.9560 0.0000 0.0038 CL= 0.516 CD=0.01292 CM=-0.1982 S TURB S SEP CD 1.0053 0.0152 0.0098 0.9560 0.0000 0.0035 CL= 0.623 CD=0.01328 CM=-0.1995 S TURB S SEP CD 1.0053 0.0152 0.0098 0.9560 0.0000 0.0035 CL= 0.623 CD=0.01328 CM=-0.1995 S TURB S SEP CD 1.0053 0.0171 0.0105 0.9560 0.0000 0.0032 CL= 0.730 CD=0.01373 CM=-0.2005 0.00 S TURB S SEP CD UPPER 0.4593 0.0134 0.0058 LOWER 0.6082 0.0000 0.0022* 0.9560 0.0000 0.0032 CL= 0.730 CD=0.01373 CM=-0.2008 S TURB S SEP CD 1.0053 0.0192 0.0113 0.9560 0.0000 0.0030 CL= 0.836 CD=0.01427 CM=-0.2020 S TURB S SEP CD LOWER 0.5082 0.0000 0.0022*
TOTAL CLE 0.734 CD-0.00795
CM=-0.2019
1.00 S TURB S SEP CD
UPPER 0.5029 0.0149 0.0064
LOWER 0.5809 0.0000 0.0020*
CM=-0.2033
CM=-0.2033
CM=-0.2035 CL= 0.836 CD=0.01427
CM=-0.2020
S TURB S SEP CD
1.0053 0.0214 0.0122
0.9560 0.0000 0.0027
CL= 0.942 CD=0.01489
CM=-0.2030
S TURB S SEP CD
1.0053 0.0239 0.0131
0.9560 0.0000 0.0025
CL= 1.047 CD=0.01562
CM=-0.2039
S TURB S SEP CD
1.0053 0.0266 0.0141
0.9560 0.0000 0.0023
CL= 1.152 CD=0.01645
CM=-0.2046
S TURB S SEP CD
1.0053 0.0267 0.0153
0.9560 0.0000 0.0021
CL= 1.152 CD=0.01645
CM=-0.2046
S TURB S SEP CD
1.0053 0.0297 0.0153
0.9560 0.0000 0.0021
CL= 1.256 CD=0.01740
CM=-0.2051
S TURB S SEP CD
1.0053 0.0331 0.0165
0.9560 0.0000 0.0020
CL= 1.359 CD=0.01847
CM=-0.2054 2.00 S TURE S SEP CD UPER 0.5326 0.0000 0.0015*

TOTAL CL= 1.266 CD= 0.0032

2.01 S TURE S SEP CD UPER 0.5599 0.0000 0.0018*

TOTAL CL= 0.949 CD=0.00899

CM=-0.2045

2.00 S TURE S SEP CD CD CM=-0.2057

4.00 S TURE S SEP CD CD CM=-0.2057

4.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2057

4.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2057

4.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2057

4.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2066

5.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2066

5.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2066

5.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2066

5.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2066

5.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2066

5.00 S TURE S SEP CD CD CD=-0.0068

CM=-0.2066

5.00 S TURE S SEP CD CD CD=-0.0068 LOWER 0.5198 0.0000 0.00153 TOTAL CLE 1.266 CD=0.01153 CM=-0.2074 0.00 S TURE S SEP CD UPPER 0.7441 0.0263 0.0115 LOWER 0.5051 0.0000 0.0014* TOTAL CLE 1.370 CD=0.01289 CM=-0.2078 6.87

R= 1000000 MU=900 S TURB S SEP CD 0.6819 0.0059 0.0056 1.0110 0.0000 0.0073* CL=-0.005 CD=0.01290 CM=-0.1906 S TURB S SEP CD 0.7052 0.0070 0.0060 0.9873 0.0000 0.0058 CL= 0.085 CD=0.01177 CL= 0.085 CD=0.01177 CM=-0.1920 S TURB S SEP CD 0.7299 0.0083 0.0065 0.9662 0.0000 0.0051 CL= 0.193 CD=0.01154 CM=-0.1937 CM=-0.1937 S TURB S SEP CD 0.7552 0.0097 0.0070 0.9374 0.0000 0.0045 CL= 0.301 CD=0.01144 CM=-0.1953 S TURB S SEP CD 0.7811 0.0112 0.0075 0.9089 0.0000 0.0040 0.7811 0.0112 0.0075
0.9089 0.0000 0.0040
CL= 0.409 CD=0.01151
CM=-0.1969
S TURB S SEP CD
0.8066 0.0128 0.0081
0.8770 0.0000 0.0035
CL= 0.517 CD=0.01170
CM=-0.1983
S TURB S SEP CD
0.8351 0.0146 0.0088
0.8447 0.0000 0.0032
CL= 0.624 CD=0.01203
CM=-0.1997
S TURB S SEP CD
0.8598 0.0164 0.0096
0.8113 0.0000 0.0029
CL= 0.731 CD=0.01244
CM=-0.2010
S TURB S SEP CD
0.8864 0.0184 0.0104
0.7766 0.0000 0.0026
CL= 0.837 CD=0.01298
CM=-0.2022
S TURB S SEP CD CL= 0.837 CD=0.01298 CM=-0.2022 S TURB S SEP CD 0.9102 0.0206 0.0113 0.7483 0.0000 0.0023 CL= 0.943 CD=0.01365 CM=-0.2032 S TURB S SEP CD 0.9335 0.0231 0.0123 0.7250 0.0000 0.0021 CL= 1.048 CD=0.01447 CM=-0.2041 S TURB S SEP CD 0.9561 0.0259 0.0135 0.7062 0.0000 0.0020 CL= 1.153 CD=0.01546 CM=-0.2048 S TURB S SEP CD 0.9762 0.0291 0.0148 0.6875 0.0000 0.0018 CL= 1.257 CD=0.01660 CM=-0.2053 S TURB S SEP CD 0.9964 0.0327 0.0163 0.6713 0.0000 0.0017 CL= 1.359 CD=0.01795 CM=0.2055 S TURB S SEP CD 0.9964 0.0327 0.0163 0.6713 0.0000 0.0017 CL= 1.359 CD=0.01795 CM=0.2055 S TURB S SEP CD S TURB S SEP CD 1.0073 0.0364 0.0177 0.6575 0.0000 0.0015

CL= 1.448 CD=0.01929 CM=-0.2054

6.91

7.00 S TURB S SEP CD UPPER 0.8382 0.0311 0.0139 LOWER 0.4890 0.0000 0.0013* TOTAL CL= 1.470 CD=0.01522 CM=-0.2076

CM=-0.2076
7.61 S TURB S SEP CD
UPPER 0.9628 0.0377 0.0177*
LOWER 0.4792 0.0000 0.0012*
TOTAL CL= 1.525 CD=0.01891
CM=-0.2060

S TURB S SEP CD 1.0053 0.0364 0.0177 0.9559 0.0000 0.0018 CL= 1.452 CD=0.01956 CM=-0.2055

R= 1100000 MU=900

R= 1100000 MU=900 S TURB S SEP CD 0.6918 0.0054 0.0056 1.0110 0.0000 0.0070* CL=-0.005 CD=0.01259 CM=-0.1907

CM=-0.1907
S TURB S SEP CD
0.7149 0.0065 0.0059
0.9886 0.0000 0.0057
CL= 0.085 CD=0.01163
CM=-0.1921
S TURB S SEP CD
0.7390 0.0079 0.0064
0.9684 0.0000 0.0050
CL= 0.193 CD=0.01141
CM=-0.1938
S TURB S SEP CD

CMI=-U.1938
S TURB S SEP CD
0.7639 0.0093 0.0069
0.9408 0.0000 0.0044
CL= 0.302 CD=0.01132
CM=-0.1954
S TURB S SEP CD

CM=-0.1954
S TURB S SEP CD
0.7895 0.0108 0.0075
0.9132 0.0000 0.0039
CL= 0.409 CD=0.01139
CM=-0.1970
S TURB S SEP CD
0.8146 0.0124 0.0081
0.8823 0.0000 0.0035
CL= 0.517 CD=0.01157
CM=-0.1985
S TURB S SEP CD

CM=-0.1985
S TURB S SEP CD
0.8424 0.0141 0.0087
0.8512 0.0000 0.0032
CL= 0.624 CD=0.01190
CM=-0.1999
S TURB S SEP CD
0.8664 0.0160 0.0095
0.8192 0.0000 0.0028
CL= 0.731 CD=0.01231
CM=-0.2012
S TURB S SEP CD

CL= 0.731 CD=0.01231
CM=-0.2012
S TURB S SEP CD
0.8920 0.0180 0.0103
0.7846 0.0000 0.0025
CL= 0.838 CD=0.01284
CM=-0.2023
S TURB S SEP CD
0.9516 0.0000 0.0023
CL= 0.944 CD=0.01349
CM=-0.2037
S TURB S SEP CD
0.9374 0.0226 0.0112
CM=-0.2034
S TURB S SEP CD
0.7313 0.0000 0.0021
CL= 1.049 CD=0.01429
CM=-0.2043
S TURB S SEP CD
0.9596 0.0224 0.0133
S TURB S SEP CD
0.9596 0.0224 0.0133
S TURB S SEP CD
0.9596 0.0254 0.0133
CM=-0.2050
S TURB S SEP CD
0.9790 0.0265 0.0126
CM=-0.2050
S TURB S SEP CD
0.9790 0.0285 0.0146
0.6929 0.0000 0.0018
CL= 1.258 CD=0.01638
CM=-0.2055
S TURB S SEP CD
0.9966 0.0322 0.0161
0.6765 0.0000 0.0016
CL= 1.360 CD=0.01770
CM=-0.2057
S TURB S SEP CD

S TURB S SEP CD 1.0084 0.0356 0.0174 0.6638 0.0000 0.0015

CL= 1.446 CD=0.01896 CM=-0.2057

ALPHA (DEG.) R= 1100000 MU=300 R= 1100000 MU=100 PHA (DEGS.) R= 1100000 MO=300 6.83 S TURB S SEP CD UPPER 0.1019 0.0265 0.0022 LOWER 1.0110 0.0000 0.0070* TOTAL CL=-0.023 CD=0.00923 CM=-0.1863 R= 110000 M0=100 S TURB S SEP CD 1.0037 0.0056 0.0064 1.0110 0.0000 0.0070* CL=-0.005 CD=0.01342 CM=-0.1906 CM=-0.1863
6.00 S TURB S SEP CD
UPPER 0.1727 0.0097 0.0026
LOWER 0.7872 0.0000 0.0041
TOTAL CL= 0.082 CD=0.0069
CM=-0.1914
5.00 S TURB S SEP CD
UPPER 0.2359 0.0078 0.0031
LOWER 0.7293 0.0000 0.0035
CM=-0.194 CD=0.00658
CM=-0.1938
4.00 S TURB S SEP CD -6.00 S TURB S SEP CD 1.0037 0.0067 0.0068 0.9560 0.0000 0.0054* CL= 0.085 CD=0.01215 CL= 0.085 CD=0.01215 CM=-0.1921 S TURB S SEP CD 1.0037 0.0082 0.0073 0.9560 0.0000 0.0049 CL= 0.193 CD=0.01218 CM=-0.1937 -5.00 4.00 S TURB S SEP CD
UPPER 0.2895 0.0080 0.0036
LOWER 0.7021 0.0000 0.0031*
TOTAL CL= 0.303 CD=0.00671
CM=-0.1957 CM=-U.1937
S TURB S SEP CD
1.0053 0.0096 0.0078
0.9560 0.0000 0.0045
CL= 0.301 CD=0.01228
CM=-0.1953 -4.00 CM=-0.1953
S TURB S SEP CD
1.0053 0.0112 0.0083
0.9560 0.0000 0.0041
CL= 0.409 CD=0.01246
CM=-0.1969
S TURB S SEP CD
1.0053 0.0129 0.0090
0.9560 0.0000 0.0038
CL= 0.516 CD=0.01273
CM=-0.1983
S TURB S SEP CD 3.00 S TURB S SEP CD UPPER 0.3369 0.0090 0.0041 LOWER 0.6831 0.0000 0.0029* -3.00 TOTAL CL= 0.411 CD=0.00693 CM=-0.1975 2.00 S TURB S SEP CD UPPER 0.3816 0.0101 0.0046 LOWER 0.6629 0.0000 0.0026*
TOTAL CL= 0.520 CD=0.00717
CM=-0.1991 CL= 0.516 CD=0.01273
CM=-0.1983
S TURB S SEP CD
1.0053 0.0147 0.0096
0.9560 0.0000 0.0035
CL= 0.624 CD=0.01308
CM=-0.1997
S TURB S SEP CD
1.0053 0.0166 0.0103
0.9560 0.0000 0.0032
CL= 0.730 CD=0.01353
CM=-0.2010
S TURB S SEP CD
1.0053 0.0187 0.0111
0.9560 0.0000 0.0022
CL= 0.837 CD=0.01405
CM=-0.2021
S TURB S SEP CD
1.0053 0.0187 0.0111
0.9560 0.0000 0.0022
CL= 0.837 CD=0.01405
CM=-0.2021
S TURB S SEP CD
1.0053 0.0299 0.0120
0.9560 0.0000 0.0027
CL= 0.943 CD=0.01467
CM=-0.2032
S TURB S SEP CD
1.0053 0.0294 0.0129
0.9560 0.0000 0.0025
CL= 1.048 CD=0.01538
CM=-0.2040
S TURB S SEP CD
1.0053 0.0261 0.013
0.9560 0.0000 0.0025
CL= 1.048 CD=0.0133 CD=0.0133
0.9560 0.0000 0.0023
CL= 1.153 CD=0.01638
CD=0.2048 -1.00 S TURB S SEP 1.00 S TURB S SEP CD UPPER 0.4254 0.0114 0.0051 LOWER 0.6358 0.0000 0.0024* TOTAL CL= 0.627 CD=0.00747 CM=-0.2006 CD UPPER 0.4688 0.0129 0.0057 LOWER 0.6082 0.0000 0.0021* 0.00 LOWER 0.6082 0.1000 0.00218
TOTAL CLE 0.735 CD=0.00783
CM=-0.2021
1.00 S TURB S SEP CD
UPPER 0.5119 0.0145 0.0064
LOWER 0.5809 0.0000 0.0019*
CM=-0.2034
CM=-0.2034 1.00 CM=-0.2034 2.00 S TURB S SEP CD UPPER 0.5543 0.0162 0.0071 LOWER 0.5599 0.0000 0.0018* TOTAL CLE -0.949 CD=0.00886 CM=-0.2047 3.00 S TURB S SEP CD UPPER 0.5964 0.0180 0.0079 LOWER 0.5453 0.0000 0.0017* TOTAL CL= 1.056 CD=0.00955 CM=-0.2058 4.00 S TURB S SEP CD 2.00 CM=-0.2058
4.00 S TURB S SEP CD
UPPER 0.6419 0.0202 0.0088
LOMER 0.5326 0.0000 0.0016*
CM=-0.2068
5.00 S TURB S SEP CD
UPPER 0.6393 0.0227 0.0099
LOWER 0.5198 0.0000 0.0015* 4.00 CL= 1.153 CD=0.01620 CM=-0.2048 S TURB S SEP CD 1.0053 0.0291 0.0150 0.9560 0.0000 0.0021 CL= 1.257 CD=0.01713 CM=-0.2053 S TURB S SEP CD 1.0053 0.0324 0.0162 0.9560 0.0000 0.0019 CL= 1.360 CD=0.01817 CM=-0.2056 LOWER 0.5198 0.10000 1.10010 1.001139 CM=-0.2076 6.00 S TURB S SEP CD UPPER 0.7528 0.0259 0.0114 LOWER 0.5051 0.0000 0.0013* TOTAL CL. = 1.370 CD=0.01275 CM=-0.2080 6.84

S TURB S SEP CD 1.0053 0.0358 0.0174 0.9559 0.0000 0.0018 CL= 1.453 CD=0.01924 CM=-0.2057

S TURB S SEP UPPER 0.8382 0.0304 0.0137 LOWER 0.4890 0.0000 0.0012* TOTAL CL= 1.471 CD=0.01491 CM=-0.2078

CM=-0.2078
7.62 S TURB S SEP CD
UPPER 0.9644 0.0370 0.0174*
LOWER 0.4789 0.0000 0.0012*
TOTAL CL= 1.527 CD=0.01861
CM=-0.2062

55

ALPHA(DEG.) R= 1200000 MU=300 R= 1200000 MH=100 6.83 S TURB S SEP CD UPPER 0.1244 0.0152 0.0022 LOWER 1.0110 0.0000 0.0069* S TURB S SEP CD 1.0037 0.0051 0.0063 1.0110 0.0000 0.0069* TOTAL CL=-0.013 CD=0.00910 CM=-0.1886 CL=-0.005 CD=0.01321 CM=-0.1907 TOTAL CLE-0.013 CD=0.00910 CM=-0.1886 ...

6.00 S TURB S SEP CD UPPER 0.1874 0.0077 0.0026 LOWER 0.7915 0.0000 0.0040 TOTAL CLE 0.084 CD=0.00664 CM=-0.1918 ...

5.00 S TURB S SEP CD UPPER 0.2481 0.0069 0.0031 LOWER 0.7293 0.0000 0.0034* TOTAL CLE 0.194 CD=0.00650 CM=-0.1940 ...

4.00 S TURB S SEP CD UPPER 0.3040 0.0074 0.0036 LOWER 0.7021 0.0000 0.0031* TOTAL CLE 0.304 CD=0.00661 CM=-0.1959 ...

3.00 S TURB S SEP CD UPPER 0.3467 0.0085 0.0040 LOWER 0.6831 0.0000 0.0028* TOTAL CLE 0.412 CD=0.00684 CM=-0.1976 ...

2.00 S TURB S SEP CD UPPER 0.3909 0.0097 0.0045* COWER 0.0629 0.0097 0.0045* TOTAL CLE 0.520 CD=0.00708 CH=-0.1907
S TURB S SEP CD
1.0037 0.0063 0.0067
0.9560 0.0000 0.0053*
CL= 0.085 CD=0.01197
CM=-0.1922
S TURB S SEP CD
1.0037 0.0077 0.0072
0.9560 0.0000 0.0049
CL= 0.194 CD=0.01201
CM=-0.1938
S TURB S SEP CD
1.0053 0.0092 0.0077
0.9560 0.0000 0.0044
CL= 0.302 CD=0.01211
CM=-0.1954
S TURB S SEP CD -6.00 -5.0n CM=-0.1954
S TURB S SEP CD
1.0053 0.0108 0.0082
0.9560 0.0000 0.0041
CL= 0.409 CD=0.01229
CM=-0.1970
S TURB S SEP CD
1.0053 0.0125 0.0088
0.9560 0.0000 0.0037
CL= 0.517 CD=0.01256
CM=-0.1984
S TURB S SEP CD
1.0053 0.0143 0.0095
0.9560 0.0000 0.0034
CL= 0.624 CD=0.01256
CM=-0.1998
S TURB S SEP CD
1.0053 0.0162 0.0102
0.9560 0.0000 0.0034
CL= 0.624 CD=0.01291
CM=-0.1998
S TURB S SEP CD
1.0053 0.0162 0.0102
0.9560 0.0000 0.0031 -3.00 LOWER 0.6629 0.0000 0.0026*
TOTAL CLE 0.520 CD-0.0708
CM=-0.1992
1.00 S TURB S SEP CD
UPPER 0.4343 0.0110 0.0051
LOWER 0.6358 0.0000 0.0023*
CM=-0.2008
CM=-0.2008
0.00 S TURB S SEP CD CM=-0.2008
0.00 S TURB S SEP CD
UPPER 0.4774 0.0124 0.0057
LOWER 0.6082 0.0000 0.0021*
TOTAL CLE -0.736 CD=0.00774
CM=-0.2022
1.00 S TURB S SEP CD
UPPER 0.5201 0.0140 0.0063
LOWER 0.5809 0.0000 0.0019*
TOTAL CL= 0.843 CD=0.00820
CM=-0.2036
2.00 S TURB S SEP CD U.9560 0.0000 0.0031 CL= 0.731 CD=0.01335 CM=-0.2011 S TURB S SEP CD 1.0053 0.0182 0.0110 0.9560 0.0000 0.0029 CL= 0.837 CD=0.01386 CM=-0.2023 CL= 0.837 CD=0.01386
CM=-0.2023
STURB S SEP CD
1.0053 0.0205 0.0118
0.9560 0.0000 0.0027
CL= 0.943 CD=0.01447
CM=-0.2033
S TURB S SEP CD
1.0053 0.0229 0.0127
0.9560 0.0000 0.0024
CL= 1.049 CD=0.01517
CM=-0.2042
S TURB S SEP CD
1.0053 0.0229 0.0127
0.9560 0.0000 0.0024
CL= 1.049 CD=0.01517
CM=-0.2042
S TURB S SEP CD
1.0053 0.0256 0.0137
0.95560 0.0000 0.0022
CL= 1.154 CD=0.01597
CM=-0.2050
S TURB S SEP CD
1.0053 0.0285 0.0148
0.9560 0.0000 0.0021
CL= 1.258 CD=0.01688
CM=-0.2055
S TURB S SEP CD
1.0053 0.0318 0.0160
0.9560 0.0000 0.0019
CL= 1.361 CD=0.01791
CM=-0.2058 CM=-0.2036
2.00 S TURB S SEP CD
UPPER 0.5620 0.0157 0.0070
LOWER 0.5599 0.0000 0.0017*
TOTAL CLE 0.950 CD=0.00875
CM=-0.2048
3.00 S TURB S SEP CD
UPPER 0.5637 0.0176 0.0078
LOWER 0.5453 0.0000 0.0016* 6.86

6.96

7.00 S TURE S SEP CD
UPPER 0.8382 0.0298 0.0134
LOWER 0.4890 0.0000 0.0012*
TOTAL CL= 1.472 CD=0.01463
CM=-0.2080

CM=-0.2080 7.63 S TURB S SEP CD UPPER 0.9660 0.0365 0.0172* LOWER 0.4787 0.0000 0.0011* TOTAL CL= 1.529 CD=0.01834 CM=-0.2064

R= 1200000 MU=900 S TURB S SEP CD 0.7006 0.0050 0.0055 1.0110 0.0000 0.0069 CL=-0.004 CD=0.01241 CM=-0.1908 CM=-0.1908
S TURB S SEP CD
0.7235 0.0061 0.0059
0.9896 0.0000 0.0056
CL= 0.086 CD=0.01150
CM=-0.1922
S TURB S SEP CD
0.7472 0.0075 0.0063
0.9703 0.0000 0.0055
CL= 0.194 CD=0.01130
CM=-0.1939
S TURB S SEP CD S TURB S SEP CD 0.7718 0.0089 0.0068 0.9437 0.0000 0.0044 CL= 0.302 CD=0.01121 CM=-0.1955 S TURB S SEP CD 0.7970 0.0104 0.0074 0.9170 0.0000 0.0039 0.9170 0.0000 0.0039
CL= 0.410 CD=0.01128
CM=-0.1971
S TURE S SEP CD
0.8217 0.0119 0.0080
0.8870 0.0000 0.0035
CL= 0.518 CD=0.01146
CM=-0.1986
S TURE S SEP CD
0.8488 0.0137 0.0087
0.8570 0.0000 0.0031
CL= 0.625 CD=0.01179
CM=-0.2000
S TURE S SEP CD
0.8724 0.0155 0.0094
0.8261 0.0000 0.0028
CL= 0.732 CD=0.01219
CM=-0.2013
S TURE S SEP CD
0.8772 CD=0.01219
CM=-0.2013
S TURE S SEP CD
0.8977 0.0175 0.0102
0.7918 0.0000 0.0025
CL= 0.838 CD=0.01271
CM=-0.2025
S TURE S SEP CD CL= 0.838 CD=0.01271
CM=-0.2025
S TURB S SEP CD
0.9194 0.0197 0.0111
0.7627 0.0000 0.0023
CL= 0.944 CD=0.01335
CM=-0.2035
S TURB S SEP CD
0.9411 0.0221 0.0120
0.7374 0.0000 0.0021
CL= 1.050 CD=0.01413
CM=-0.2045
S TURB S SEP CD
0.9626 0.0249 0.0132
0.7178 0.0000 0.0019
CL= 1.154 CD=0.01508
CM=-0.2052
S TURB S SEP CD
0.9626 0.0249 0.0132
0.7178 0.0000 0.0019
CL= 1.154 CD=0.01508
CM=-0.2052
S TURB S SEP CD
0.9814 0.0280 0.0144
0.6979 0.0000 0.0018
CL= 1.258 CD=0.01618
CM=-0.2057
S TURB S SEP CD
0.9984 0.0316 0.0159
0.6812 0.0000 0.0016
CL= 1.361 CD=0.01748
CM=-0.2059
S TURB S SEP CD S TURB S SEP CD 1.0100 0.0352 0.0172 0.6685 0.0000 0.0015 CL= 1.448 CD=0.01875 CM=-0.2059

S TURB S SEP CD 1.0053 0.0354 0.0172 0.9559 0.0000 0.0018 CL= 1.459 CD=0.01901 CM=-0.2059

ALPHA (DEG.) R= 1300000 MU=300 R= 1300000 MU=100 5.83 S TURB S SEP CD UPPER 0.1409 0.0103 0.0022 LOWER 1.0110 0.0000 0.0068 S TURB S SEP CD 1.0037 0.0047 0.0062 1.0110 0.0000 0.0068* CL=-0.004 CD=0.01301 CM=-0.1908 S TURB S SEP CD 1.0037 0.0059 0.0066 TOTAL CL=-0.009 CD=0.00899 CM=-0.1896 5.00 S TURB S SEP CD UPPER 0.2005 0.0062 0.0026 LOWER 0.8002 0.0000 0.0040 TOTAL CL= 0.085 CD=0.00663 CM=-0.1922 0.9560 0.0000 0.0052* CL= 0.086 CD=0.01180 CM=-0.1922 CM=-0.1922
S TURB S SEP CD
1.0037 0.0073 0.0071
0.9560 0.0000 0.0048
CL= 0.194 CD=0.01186
CM=-0.1939
S TURB S SEP CD
1.0053 0.0088 0.0076
0.9560 0.0000 0.0044
CL= 0.102 CD=0.01196
CM=-0.1955
S TURB S SEP CD
1.0053 0.0104 0.0081
0.9560 0.0000 0.0044
CL= 0.410 CD=0.01194
CM=-0.1971
S TURB S SEP CD
1.0053 0.0104 0.0081
0.9560 0.0000 0.0047
CL= 0.410 CD=0.01214
CM=-0.1971
S TURB S SEP CD
1.0053 0.0121 0.0087
0.9560 0.0000 0.0037 CMR-0.1922
5.00 S TURB S SEP CD
UPPER 0.2593 0.0059 0.0031
LOMER 0.7293 0.0000 0.0033*
TOTAL CL= 0.195 CD=0.00640
CMR-0.1942 ~5.00 4.00 S TURB S SEP CD UPPER 0.3102 0.0069 0.0035 LOWER 0.7021 0.0000 0.0030* UPPER 0.3102 1.0069 0.0035
LOWER 0.7021 0.0000 0.0030*
TOTAL CL= 0.304 CD=0.00653
CM=-0.1960
-3.00 S TURB S SEP CD
UPPER 0.3558 0.0080 0.0028*
TOTAL CL= 0.412 CD=0.00676
CM=-0.1977
-2.00 S TURB S SEP CD
UPPER 0.3996 0.0093 0.0028*
TOTAL CL= 0.412 CD=0.00676
CM=-0.1977
-2.100 S TURB S SEP CD
UPPER 0.3996 0.0093 0.0025*
TOTAL CL= 0.521 CD=0.00700
CM=-0.1993
-1.00 S TURB S SEP CD
UPPER 0.4427 0.0106 0.0023*
TOTAL CL= 0.628 CD=0.00730
CM=-0.2009
0.00 S TURB S SEP CD 0.9560 0.0000 0.0037 CL= 0.517 CD=0.01241 CM=-0.1985 S TURB S SEP CD 1.0053 0.0138 0.0094 0.9560 0.0000 0.0034 CL= 0.625 CD=0.01275 CM=-0.1999 CM=-0.1999
S TURB S SEP CD
1.0053 0.0158 0.0101
0.9560 0.0000 0.0031
CL= 0.731 CD=0.01318
CM=-0.2012
S TURB S SEP CD
1.0053 0.0178 0.0108
0.9560 0.0000 0.0029
CL= 0.838 CD=0.01369
CM=-0.2024
S TURB S SEP CD
1.0053 0.0200 0.0117
0.9560 0.0000 0.00226
CL= 0.944 CD=0.01369
CM=-0.2024
S TURB S SEP CD
1.0053 0.0200 0.0117
0.9560 0.0000 0.00126
CL= 0.944 CD=0.01429
CM=-0.2034
S TURB S SEP CD CM=-0.2009

0.00 S TURB S SEP CD

UPPER 0.4853 0.0120 0.0056

LOWER 0.6082 0.0000 0.0020*

TOTAL CL= 0.736 CD=0.00765

CM=-0.2023

1.00 S TURB S SEP CD

LOWER 0.5276 0.0136 0.0063

LOWER 0.5276 0.0136 0.0061 0.00 LOWER 0.5809 0.0000 0.0019*
TOTAL C.E. 0.843 CD-0.0811
CM=-0.2037
2.00 S TORB S SEP CD
UPPER 0.5691 0.0154 0.0069
LOWER 0.5599 0.0000 0.0017*
TOTAL C.E. 0.950 CD-0.0066
CM=-0.2050
3.00 S TOTBD C SEP CD CM=-0.2050
S TURE S SEP CD
UPPER 0.6107 0.0172 0.0077
LOWER 0.5453 0.0000 0.0016*
TOTAL CL= 1.057 CD=0.00933
CM=-0.2061
4.00 S TURE S SEP CD
UPPER 0.6565 0.0194 0.0087
LOWER 0.5326 0.0000 0.0015*
TOTAL CL= 1.163 CD=0.01014
CM=-0.2071
5.00 S TURE S SEP CD CM=-0.2034
S TURB S SEP CD
1.0053 0.0224 0.0126
0.9560 0.0000 0.0024
CL= 1.049 CD=0.01498
CM=-0.2044
S TURB S SEP CD
1.0053 0.0251 0.0135
0.9560 0.0000 0.0022
CL= 1.154 CD=0.01577
CM=-0.2051
S TURB S SEP CD CM=-0.2071
5.00 S TURB S SEP CD
UPPER 0.7081 0.0219 0.0098
LOWER 0.5198 0.0000 0.0014*
TOTAL CL= 1.268 CD=0.01118
CM=-0.2078 CM=-U.2051 S TURB S SEP CD 1.0053 0.0280 0.0146 0.9560 0.0000 0.0020 CL= 1.258 CD=0.01666 CM=-0.2057 5.00 CM=-0.2078 6.00 S TURB S SEP CD UPPER 0.7684 0.0251 0.0113 LOWER 0.5051 0.0000 0.0013* TOTAL CL= 1.371 CD=0.01253 CM=-0.2083 CM=-0.2057 S TURE S SEP CD 1.0053 0.0313 0.0158 0.9560 0.0000 0.0019 CL= 1.362 CD=0.01767 CM=-0.2060 6.87

R= 1300000 MU=900 S TURB S SEP CD 0.7087 0.0046 0.0055 1.0110 0.0000 0.0068* CL=-0.004 CD=0.01225 CM=-0.1908 CM=-0.1908 S TURB S SEP CD 0.7313 0.0057 0.0058 0.9906 0.0000 0.0055 CL= 0.086 CD=0.01137 CM=-0.1923 CH=-0.1923
S TURB S SEP CD
0.7547 0.0071 0.0063
0.9720 0.0000 0.0049
CL= 0.194 CD=-0.0119
CM=-0.1940
S TURB S SEP CD
0.7789 0.0085 0.0068
0.9463 0.0000 0.0043
CL= 0.192 CD=-0.01111
CM=-0.1956
S TURB S SEP CD
0.8038 0.0100 0.0073
0.9204 0.0000 0.0033
CL= 0.410 CD=-0.01118
CM=-0.1972
S TURB S SEP CD
0.8282 0.0116 0.0079
0.8913 0.0000 0.0034
CL= 0.450 CD=-0.0118
CM=-0.1972
S TURB S SEP CD U.8913 U.0000 0.0034 CL= 0.518 CD=0.01136 CM=-0.1987 S TURB S SEP CD 0.8545 0.0133 0.0086 0.8621 0.0000 0.0031 CL= 0.625 CD=0.01168 CM=-0.2001 CM=-0.2001
S TURB S SEP CD
0.8776 0.0151 0.0093
0.8321 0.0000 0.0028
CL= 0.732 CD=0.01208
CM=-0.2014
S TURB S SEP CD
0.9015 0.0172 0.0101
0.7986 0.0000 0.0025
CL= 0.839 CD=0.01259
CM=-0.2026
S TURB S SEP CD
0.9232 0.0193 0.0109
0.7693 0.0000 0.0023
CL= 0.945 CD=0.01321
CM=-0.2037
S TURB S SEP CD S TURB S SEP CD 0.9443 0.0217 0.0119 0.7431 0.0000 0.0021 0.7431 0.0000 0.0021 CL= 1.050 CD=0.01398 CM=-0.2046 S TURB S SEP CD 0.9653 0.0245 0.0130 0.7230 0.0000 0.0019 CL= 1.155 CD=0.01491 CM=-0.2053 CM=-0.2053
S TURE S SEP CD
0.9836 0.0276 0.0143
0.7027 0.0000 0.0017
CL= 1.259 CD=0.01600
CM=-0.2058
S TURE S SEP CD
1.0001 0.0312 0.0157
0.6855 0.0000 0.0016
CL= 1.362 CD=0.01727
CM=-0.2061
S TURE S SEP CD
1.0112 0.0347 0.0170
0.6729 0.0000 0.0015
CL= 1.450 CD=0.01854
CM=-0.2060

CM=-0.2060

S TURB S SEP 1.0053 0.0349 0.0170 0.9559 0.0000 0.0017 CL= 1.463 CD=0.01878

CM=-0.2061

6.99

7.00 S TURE S SEP CD
UPPER 0.8405 0.0293 0.0132
LOWER 0.4890 0.0000 0.0012*
TOTAL CLE 1.473 CD=0.01442
CM=-0.2082
7.66 S TURE S SEP CD
UPPER 0.9705 0.0361 0.0170*
LOWER 0.4783 0.0000 0.0011*
TOTAL CLE 1.533 CD=0.01816
CM=-0.2066

ALPHA (DEG.) R= 1400000 MU=300 FIRACLES, R = 1400000 MU=300 6.83 S TURB S SEP CD UPPER 0.1553 0.0073 0.0022 LOWER 1.0110 0.0000 0.0067* TOTAL CL=-0.007 CD=0.00889 CM=-0.1903 CM=-0.1903 6.00 S TURB S SEP CD UPPER 0.2124 0.0052 0.0026 -6.00 S TURB S SEP CD UPPER 0.2124 4 0.0025 0.0026 LOWER 0.8083 0.0000 0.0040 TOTAL CLE 0.086 CD=0.00663 CM=-0.1924 -5.00 S TURB S SEP CD UPPER 0.2695 0.054 0.0031 LOWER 0.7293 0.0000 0.0033* TOTAL CLE 0.196 CD=0.00634 CM=-0.1944 -4.00 S TURB S SEP CD UFFER 0.3192 0.0064 0.0035 LOWER 0.7021 0.0000 0.0029* TOTAL CLE 0.305 CD=0.0064 0.0035 LOWER 0.7021 0.0000 0.0029* TOTAL CLE 0.305 CD=0.0064 0.0029* TOTAL CLE 0.305 CD=0.0064 0.0027* TOTAL CLE 0.413 CD=0.0064 0.0027* TOTAL CL= 0.413 CD=0.0065 CD=0.0064 LOWER 0.6631 0.0000 0.0027* TOTAL CL= 0.413 CD=0.00669 CD=0.0064 LOWER 0.6639 0.0000 0.0025* TOTAL CL= 0.6529 0.0000 0.0045 LOWER 0.6629 0.0000 0.0055* TOTAL CL= 0.5121 CD=0.00693 LOWER 0.5629 0.0000 0.0025*
TOTAL CLE 0.521 CD=0.00693
CM=-0.1994
1.00 S TURE S SEP CD
UPPER 0.4505 0.0102 0.0050
LOWER 0.6358 0.0000 0.0022*
TOTAL CLE 0.629 CD=0.00723
CM=-0.2010 CM=-0.2010

0.00 S TURB S SEP CD
UPPER 0.4928 0.0117 0.0056
LOWER 0.6082 0.0000 0.0020*
TOTAL CL= 0.737 CD=0.00758
CM=-0.2024

1.00 S TURB S SEP CD
UPPER 0.5346 0.0133 0.0062*
TOTAL CL= 0.844 CD=0.00803
CM=-0.2038

2.00 S TURB S SEP CD
UPPER 0.5756 0.0150 0.0069*
CM=-0.2038

2.00 S TURB S SEP CD
UPPER 0.5756 0.0150 0.0069*
CM=-0.2038

1.00 S TURB S SEP CD
UPPER 0.5756 0.0150 0.0069*
CM=-0.2038

2.00 S TURB S SEP CD
UPPER 0.5759 0.0000 0.0017*
TOTAL CL= 0.951 CD=0.00857
CM=-0.2051

3.00 S TURB S SEP CD TOTAL CL= 0.951 CD=0.00857 CM=0.2051
3.00 S TURB S SEP CD UPPER 0.6172 0.0169 0.0077 COWER 0.5453 0.0000 0.0016* TOTAL CL= 1.057 CD=0.00924 CM=0.2052 CM=0.0000 0.0016* CM=0.2052 CM=0.0000 0.0015* CM=0.2052 CM=0.0000 0.0015* CM=0.2072 CM=0.2052 CM=0.2052 CM=0.2052 CM=0.2052 CM=0.2052 CM=0.2052 CM=0.2052 CM=0.2052 CM=0.2072 CM=0.2084 CM=0.2079 CM=0.2079 CM=0.2084 CM 6.86 S TURB S SEP 7.00 S TORB S SEP CD UPPER 0.8465 0.0290 0.0132 LOWER 0.4890 0.0000 0.0012* TOTAL CL= 1.474 CD=0.01432 CM=-0.2083

7.66 S TURB S SEP CD UPPER 0.9705 0.0355 0.0168* LOWER 0.4783 0.0000 0.0011* TOTAL CL= 1.534 CD=0.01789 CM=-0.2068

R= 1400000 MU=100 S TURB S SEP CD 1.0037 0.0043 0.0062 1.0110 0.0000 0.0067* 1.0110 0.0000 0.0067* CL=-0.004 CD=0.01283 CM=-0.1909 S TURB S SEP CD 1.0037 0.0055 0.0065 0.9560 0.0000 0.0051* CL= 0.086 CD=0.01166 CM=-0.1923 CM=-0.1923
S TORB S SEP CD
1.0037 0.0070 0.0970
0.9560 0.0000 0.0047
CL= 0.194 CD=0.01172
CM=-0.1940
S TURB S SEP CD
1.0053 0.0084 0.0075
0.9560 0.0000 0.0043
CL= 0.302 CD=0.0182
CM=-0.1956
S TURB S SEP CD
1.0053 0.0100 0.0080
0.9560 0.0000 0.0040
CL= 0.410 CD=0.01200
CM=-0.1972
S TURB S SEP CD
1.0053 0.0100 0.0080
0.9560 0.0000 0.0040
CL= 0.410 CD=0.01200
CM=-0.1972
S TURB S SEP CD
1.0053 0.0117 0.0086
0.9560 0.0000 0.0036 U.9560 U.0000 U.0036 CL= 0.518 CD=0.01226 CM=-0.1987 S TURB S SEP CD 1.0053 0.0135 0.0093 0.9560 0.0000 0.0033 CL= 0.625 CD=0.01260 CM=-0.2000 CM=-0.2000
S TURB S SEP CD
1.0053 0.0154 0.0100
0.9560 0.0000 0.0031
CL= 0.732 CD=0.01303
CM=-0.2013
S TURB S SEP CD
1.0053 0.0174 0.0107
0.9560 0.0000 0.0028
CL= 0.838 CD=0.01353
CM=-0.2025
TURB S SEP CD CM=-0.2025 S TURB S SEP CD 1.0053 0.0196 0.0115 0.9560 0.0000 0.0026 CL= 0.944 CD=0.01412 CM=-0.2036 S SEP CD 1.0053 0.0220 0.0124 0.9560 0.0000 0.0024 CL= 1.050 CD=0.01480 CL= 1.050 CD=0.01480 CM=-0.2045 S TURB S SEP CD 1.0053 0.0246 0.0134 0.9560 0.0000 0.0022 CL= 1.155 CD=0.01558 CM=-0.2053 CM=-0.2053 S TURB S SEP CD 1.0053 0.0276 0.0144 0.9560 0.0000 0.0020 CL= 1.259 CD=0.01646 CM=-0.2058 CM=-0.2058 S TURB S SEP CD 1.0053 0.0308 0.0156 0.9560 0.0000 0.0019 CL= 1.362 CD=0.01745 CM=-0.2062

S TURB S SEP

S TURB S SEP CD 1.0053 0.0344 0.0168 0.9560 0.0000 0.0017 CL= 1.465 CD=0.01855 CM=-0.2063 S TURB S SEP CD 1.0053 0.0345 0.0168

0.9560 0.0000 0.0017 CL= 1.466 CD=0.01857 CM=-0.2063

R= 1400000 MII=900 S TURB S SEP CD 0.7162 0.0042 0.0054 1.0110 0.0000 0.0067* CL=-0.004 CD=0.01211 CM=-0.1909 CM=-0.1909 S TURB S SEP CD 0.7383 0.0054 0.0058 0.9914 0.0000 0.0055 CL= 0.086 CD=0.01127 CM=-0.1924 CL= 0.086 CD=0.01127
CM=-0.1924
S TURB S SEP CD
0.7614 0.0067 0.0062
0.7935 0.0000 0.0049
CL= 0.195 CD=0.01109
CM=-0.1941
S TURB S SEP CD
0.7855 0.0081 0.0067
0.7855 0.0081 0.0067
0.7855 0.0081 0.0067
0.7855 0.0081 0.0067
0.7855 0.0081 0.0067
0.7855 0.0081 0.0067
0.7855 0.0081 0.0067
0.8101 0.0096 0.0073
0.9235 0.0000 0.0038
CL= 0.411 CD=0.01109
CM=-0.1973
S TURB S SEP CD
0.8342 0.0112 0.0079
0.8952 0.0000 0.0034
CL= 0.518 CD=0.01127
CM=-0.1988
S TURB S SEP CD
0.8566 0.0129 0.0085
0.8668 0.0000 0.0031
CL= 0.626 CD=0.01159
CM=-0.0002
S TURB S SEP CD CM=-0.2002 S TURB S SEP CD 0.8822 0.0148 0.0092 0.8375 0.0000 0.0028 CL= 0.733 CD=0.01198 CM=-0.2015 S TURE S SEP CD 0.9054 0.0168 0.0100 0.8048 0.0000 0.0025 CL= 0.839 CD=0.01248 CM=-0.2027 CM=-0.202/ S TURB S SEP CD 0.9267 0.0190 0.0108 0.7754 0.0000 0.0023 CL= 0.945 CD=0.01309 CM=-0.2038 CM=-0.2038
S TURB S SEP CD
0.9472 0.0213 0.0118
0.7485 0.0000 0.0021
CL= 1.051 CD=0.01385
CM=-0.2047
S TURB S SEP CD
0.9677 0.0241 0.0129
0.7279 0.0000 0.0019
CL= 1.156 CD=0.01477
CM=-0.2055
S TURB S SEP CD S TURB S SEP CD 0.9855 0.0271 0.0141 0.7073 0.0000 0.0017 CL= 1.260 CD=0.01583 CL= 1.260 CD=0.01583 CM=-0.2060 S TURB S SEP CD 1.0015 0.0307 0.0155 0.6899 0.0000 0.0016 CL= 1.363 CD=0.01709 CM=-0.2062 S TURB S SEP CD 1.0121 0.0342 0.0168 0.6773 0.0000 0.0015 CL= 1.450 CD=0.01832 CM=-0.2062 CM=-0.2062

ALPHA (DEG.) R= 1500000 MH=300 R= 1500000 MII=100 -6.83 S TURB S SEP CD UPPER 0.1683 0.0053 0.0022 LOWER 1.0110 0.0000 0.0066* S TURB S SEP CD 1.0037 0.0039 0.0061 1.0110 0.0000 0.0066* TOTAL CL=-0.005 CD=0.00880 CM=-0.1907 CL=-0.004 CD=0.01267 CM=-0.1910 CM=-0.1910
S TURB S SEP CD
1.0037 0.0051 0.0065
0.9560 0.0000 0.0051*
CL= 0.086 CD=0.01152
CM=-0.1924
S TURB S SEP CD
1.0037 0.0066 0.0069
0.9560 0.000 0.0047
CL= 0.195 CD=0.01159
CM=-0.1941
S TURB S SEP CD CM=-0.1907 -6.00 S TURB S SEP CD UPPER 0.2234 0.0043 0.0026 LOWER 0.8155 0.0000 0.0040 TOTAL CL= 0.087 CD=0.00663 CM=-0.1926 5.00 S TURB S SEP CD UPPER 0.2790 0.0049 0.0031 LOWER 0.7293 0.0000 0.0032* ~5 00 LOWER 0.7293 0.0000 0.0032*
TOTAL CLE 0.196 CD=0.0629
CM=-0.1945
4.00 S TURB S SEP CD
UPPER 0.3276 0.0060 0.0035
LOWER 0.7021 0.0000 0.0029*
TOTAL CLE 0.305 CD=0.00640
CM=-0.1962 CM=-0.1941 S TURB S SEP CD 1.0053 0.0081 0.0074 0.9560 0.0000 0.0043 CL= 0.303 CD=0.01169 CM=-0.1957 CM=-0.1962
3.00 S TURB S SEP CD
UPPER 0.3718 0.0073 0.0040
LOWER 0.6831 0.0000 0.0027*
TOTAL CL.= 0.413 CD=0.00663
CM=-0.1979
2.00 S TURB S SEP CD
UPPER 0.4150 0.0085 0.0045
LOWER 0.6629 0.0000 0.0024* S TURB S SEP CD 1.0053 0.0097 0.0080 0.9560 0.0000 0.0039 -3.00 0.9560 0.0000 0.0038 CL= 0.411 CD=0.01188 CM=-0.1973 S TURB S SEP CD 1.0053 0.0113 0.0085 0.9560 0.0000 0.0036 CL= 0.518 CD=0.01213 CM=-0.1988 LOWER 0.6629 0.0000 0.0024*
TOTAL CL= 0.521 CD=0.00687
CM=-0.1995
-1.00 S TURB S SEP CD
UPPER 0.4577 0.0099 0.0050
LOWER 0.6358 0.0000 0.0022*
TOTAL CL= 0.629 CD=0.00717 S TURB S SEP CD S TURB S SEP CD 1.0053 0.0131 0.0092 0.9560 0.0000 0.0033 CL= 0.625 CD=0.01247 CM=-0.2001 S TURB S SEP CD 1.0053 0.0150 0.0098 CM=-0.2011 0.00 S TURB S SEP CD UPPER 0.4997 0.0114 0.0056 LOWER 0.6082 0.0000 0.0020* 0.9560 0.0000 0.0030 TOTAL CL= 0.737 CD=0.00752 CM=-0.2025
1.00 S TURB S SEP CD UPPER 0.5411 0.0130 0.0062 CL= 0.732 CD=0.01289 CM=-0.2014 S TURB S SEP CD 1.0053 0.0170 0.0106 UNPER 0.5411 0.0130 0.0001 0.0018*

TOTAL CL= 0.844 CD=0.00797 CM=-0.2039

2.00 S TURB S SEP CD
UPPER 0.5817 0.0147 0.006

LOMER 0.5599 0.0000 0.0016*

TOTAL CL= 0.951 CD=0.00850 0.9560 0.0000 0.0028 CL= 0.839 CD=0.01339 CM=-0.2026 2.00 S TURB S SEP CD 1.0053 0.0192 0.0114 0.9560 0.0000 0.0026 CL= 0.945 CD=0.01397 CM=-0.2037 S TURB S SEP CD 1.0053 0.0216 0.0123 0.9560 0.0000 0.0024 CM=-0.2052 CM=-0.2052 3.00 S TURB S SEP CD UPPER 0.6233 0.0166 0.0076 LOWER 0.5453 0.0000 0.0015* 0.9560 0.0000 0.0024 CL= 1.051 CD=0.01464 CM=-0.2046 S TURE S SEP CD 1.0053 0.0242 0.0132 0.9560 0.0000 0.0022 CL= 1.155 CD=0.01541 CM=-0.2054 S TURE S SEP CD 1.0053 0.0271 0.0143 0.9560 0.0000 0.0022 CL= 1.260 CD=0.01541 CM=-0.2054 S TURE S SEP CD 1.0053 0.0271 0.0143 0.9560 0.0000 0.0020 CL= 1.260 CD=0.01627 LOWER 0.5453 0.1000 0.10015*
TOTAL CLE 1.058 CD=0.0017
CM=-0.2063
4.00 S TURB S SEP CD
UPPER 0.6692 0.0187 0.0085
LOWER 0.5326 0.0000 0.0014*
TOTAL CLE 1.164 CD=0.0098
CM=-0.2073 4.00 CM=-0.2073 5.00 S TURB S SEP CD UPPER 0.7211 0.0213 0.0097 LOWER 0.5198 0.0000 0.0013* LOWER 0.5198 0.1000 0.1001 TOTAL CLE 1.269 CD=0.01101 CM=-0.2081 6.00 S TURE S SEP CD UPPER 0.7819 0.0245 0.0111 LOWER 0.5051 0.0000 0.0012* TOTAL CLE 1.372 CD=0.01237 CM=-0.2085 0.9560 0.0000 0.0020 CL= 1.260 CD=0.01627 CM=-0.2060 S TURB S SEP CD 1.0053 0.0304 0.0154 0.9560 0.0000 0.0019 CL= 1.363 CD=0.01724 CM=-0.2064 6.91 7.00 S TURB S SEP CD UPPER 0.8520 0.0286 0.0131 LOWER 0.4890 0.0000 0.0011* TOTAL CL= 1.474 CD=0.01422 CM=-0.2085 7.09

7.69 S TURB S SEP CD UPPER 0.9745 0.0354 0.0167* LOWER 0.4778 0.0000 0.0011* TOTAL CL= 1.538 CD=0.01782 CM=-0.2069

7.69

S TURB S SEP CD 1.0053 0.0340 0.0166 0.9560 0.0000 0.0017 CL= 1.466 CD=0.01834 CM=-0.2055 S TURB S SEP CD 1.0053 0.0343 0.0167 0.9560 0.0000 0.0017 CL= 1.475 CD=0.01844 CM=-0.2065

CL= 0.087 CD=0.01117 CM=-0.1924 S TURB S SEP CD 0.7676 0.0064 0.0062 0.9749 0.0000 0.0048 CL= 0.195 CD=0.01100 CM=-0.1941 CM=-U.1941 S TURB S SEP CD 0.7915 0.0078 0.0067 0.9507 0.0000 0.0042 CL= 0.303 CD=0.01093 CM=-0.1958 CL= 0.303 CD=0.01093 CM=-0.1958 S TURB S SEP CD 0.8158 0.0093 0.0072 0.9263 0.0000 0.0038 CL= 0.411 CD=0.01101 CM=-0.1974 S TURB S SEP CD 0.8397 0.0109 0.0078 CL= 0.519 CD=0.01119 CM=-0.1989 0.0000 0.0034 CL= 0.519 CD=0.01119 CM=-0.1989 S TURB S SEP CD 0.8643 0.0126 0.0084 0.8710 0.0026 CD=0.01150 CM=-0.2003 S TURB S SEP CD 0.8644 0.0091 0.8422 0.0000 0.0028 CL= 0.733 CD=0.01188 CM=-0.2016 S TURB S SEP CD 0.9090 0.0164 0.0099 0.8105 0.0164 0.0099 0.8105 0.0164 0.0099 0.8105 0.0164 0.0095 CL= 0.846 CD=0.0128 CM=-0.2016 S TURB S SEP CD 0.9090 0.0164 0.0099 0.8105 0.0000 0.0025 CL= 0.846 CD=0.01238 CM=-0.2028 S TURB S SEP CD 0.9990 0.0164 0.0099 0.8105 0.0000 0.0025 CL= 0.846 CD=0.01238 CM=-0.2028 S TURB S SEP CD 0.9990 0.0185 0.0107 CL= 0.840 CD=0.01238 CM=-0.2028 S TURB S SEP CD 0.9299 0.0186 0.0107 0.7811 0.0000 0.0022 CL= 0.946 CD=0.01299 CM=-0.2039 S TURB S SEP CD 0.9499 0.0210 0.0117 0.7538 0.0000 0.0020 CL= 1.051 CD=0.01373 CM=-0.2048 S TURB S SEP CD 0.9699 0.0217 0.0128 0.7325 0.0000 0.0019 CL= 1.156 CD=0.01463 CM=-0.2056 S TURB S SEP CD 0.9873 0.0267 0.0140 0.7116 0.0000 0.0017 CL= 1.260 CD=0.01568 CM=-0.2061 S TURB S SEP CD 1.0028 0.0303 0.0153 0.6940 0.0000 0.0016 CL= 1.363 CD=0.01692 CM=-0.2064 S TURB S SEP CD 1.0028 0.0303 0.0153 0.6940 0.0000 0.0016 CL= 1.363 CD=0.01692 CM=-0.2064 S TURB S SEP CD 1.0028 0.0303 0.0153 0.6940 0.0000 0.0016 CL= 1.363 CD=0.01692 CM=-0.2064 S TURB S SEP CD 1.0028 0.0340 0.0167 S TURB S SEP CD 1.0136 0.0340 0.0167 0.6801 0.0000 0.0015 CL= 1.456 CD=0.01821 CM=-0.2064

R= 1500000 MU=900 R= 1500000 MU=900 S TURB S SEP CD 0.7231 0.0038 0.0054 1.0110 0.0000 0.0066' CL=-0.003 CD=0.01197 CM=-0.1910

CM=-0.1910 S TURB S SEP CD 0.7448 0.0050 0.0058 0.9922 0.0000 0.0054 CL= 0.087 CD=0.01117

APPENDIX B

PRESSURE DISTRIBUTIONS, TRANSITION AND SEPARATION LOCATIONS, AND SECTION CHARACTERISTICS OF S905 AIRFOIL

		10%				-1.00	0.00	1.00	2.00	3.00	4.00	5.00	6.00	7.00	8.00
N	X	Y		CP(X) FOR '											
1	1.00000	0.00000	0.00	0.262	0.263	0.266	0.269	0.272	0.276		0.284	0.289			0.307
2	0.99670	0.00088	1.00	0.244	0.245	0.246	0.247	0.249	0.252	0.254	0.258	0.262			0.275
3	0.98716	0.00373	2.00	0.177	0.176	0.176	0.176	0.177	0.178	0.180	0.182	0.184	0.187	0.191	0.195
4	0.97222	0.00863	3.00	0.073	0.071	0.069	0.067	0.066		0.066	0.067	0.068			0.075
5	0.95269	0.01521	4.00											-0.068	
6	0.92905	0.02278	5.00	-0.157	-0.164	-0.171	-0.178	-0.183	-0.188	-0.192	-0.196	-0.198	-0.200	-0.201	-0.202
7	0.90137	0.03076	6.00											-0.290	
8	0.86962	0.03901	7.00											-0.345	
9	0.83410	0.04761	8.00	-0.283	-0.299	-0.314	-0.329	-0.343	-0.356	-0.369	-0.380	-0.391	-0.401	-0.411	-0.419
10	0.79539	0.05651	9.00	-0.325	-0.345	-0.363	-0.381	-0.399	~0.415	-0.431	-0.446	-0.461	-0.474	-0.487	-0.498
11	0.75405	0.06552	10.00	-0.375	-0.398	-0.421	-0.443	-0.464	-0.484	-0.504	-0.523	-0.541	-0.558	~0.575	-0.590
12	0.71067	0.07440	11.00	-0.432	-0.460	-0.487	-0.513	-0.539	-0.564	-0.588	-0.611	-0.634	-0.655	-0.676	-0.696
13	0.66582	0.08287	12.00	-0.498	-0.530	-0.562	-0.594	-0.624	-0.654	-0.684	-0.712	-0.740	-0.767	-0.793	-0.818
14	0.62009	0.09058	13.00	-0.571	-0.609	-0.647	-0.684	-0.721	-0.757	-0.792	-0.827	-0.861	-0.894	-0.926	-0.957
15	0.57397	0.09708	14.00	-0.645	-0.689	-0.734	-0.778	-0.821	-0.864	-0.907	-0.948	-0.989	-1.029	-1.068	-1.106
16	0.52766	0.10192	15.00											-1.177	
17	0.48128	0.10496	16.00	-0.698	-0.756	-0.813	-0.870	-0.927	-0.984	-1.040	-1.096	-1.151	-1.206	-1.260	-1.313
18	0.43504	0.10625	17.00											-1.327	
19	0.38928	0.10586	18.00	-0.675	-0.745	-0.816	-0.887	-0.958	-1.029	-1.100	-1.171	-1.242	-1.313	-1.384	-1.454
20	0.34435	0.10391	19.00	-0.644	-0.721	-0.799	-0.878	-0.956	-1.036	-1.115	-1.195	-1.275	-1.355	-1.435	-1.514
21	0.30064	0.10051	20.00											-1.484	
22	0.25854	0.09581	21.00											-1.536	
23	0.21849	0.08997	22.00											-1.600	
24	0,18089	0.08313	23.00											-1.676	
25	0.14614	0.07541	24.00											-1.768	
26	0.11457	0.06695	25.00											-1.877	
27	0.08648	0.05789	26.00											-2.009	
28	0.06211	0.04839	27.00	-0.175	-0.320	-0.374	-0.561	-0.023	-0 967	-1 186	-1 415	-1 654	-1 902	-2.160	-2.223
29	0.04163	0.03863	28.00											-2.339	
30	0.02516	0.02886	29.00	0.402	0.215									-2.553	
31	0.01280	0.01937	30.00	0.703	0.527	0.311								-2.826	
32	0.00455	0.01054	31.00	0.765	0.881	0.714	0.475							-3.174	
33	0.00433	0.00297	32.00	0.633	0.892	0.997	0.948	0.745						-3.174	
34	0.00003	0.00257	32.36	-0.196	0.422	0.818	0.992	0.743	0.568						
35		-0.00070	32.50	-1.440		0.381	0.841	1.000						-4.026	
36		-0.00179	32.86		-2.061				0.857					-4.365	
37		-0.00275	33.11	-2.703			0.322	0.871	0.989	0.677				-4.855	
38		-0.00346	33.36		-1.168		0.163	0.717			0.736			-1.431	
39		-0.00536	34.00						0.873	0.994	0.959	0.768		-0.082	
					-0.773		0.075	0.397	0.651	0.836	0.952	0.999		0.886	0.726
40 41		-0.00762	35.00 36.00	-0.783			0.040	0.259	0.450	0.613	0.748	0.854		0.980	1.000
42		-0.00898 -0.00945	37.00	-0.527			0.043	0.205	0.352	0.485	0.602	0.705		0.865	0.922
43		-0.00945		-0.372			0.056	0.182	0.300	0.409	0.509	0.600		0.754	0.818
44		-0.00909	38.00 39.00	-0.264			0.074	0.176	0.272	0.363	0.448	0.527	0.601	0.668	0.730
44		-0.00627	40.00	-0.182		0.004	0.092	0.176	0.257	0.334	0.407	0.477	0.542	0.603	0.660
46		-0.00402	41.00	-0.117 -0.063		0.037	0.111	0.182	0.251	0.317	0.380	0.441	0.499	0.554	0.606
47			42.00		0.002	0.067	0.129	0.190	0.249	0.307	0.362	0.416		0.517	0.564
48	0.30519	-0.00138 0.00152	43.00	-0.017 0.023	0.039	0.094	0.147	0.200	0.252	0.302	0.351	0.398		0.489	0.532
48	0.35772	0.00152	44.00	0.023		0.119	0.165	0.211	0.256	0.300	0.344	0.386		0.467	0.506
					0.101	0.142	0.183	0.223	0.263	0.302	0.340	0.378	0.415	0.451	0.486
50	0.41227	0.00755	45.00	0.092	0.128	0.164	0.200	0.235	0.270	0.305	0.339	0.373	0.406	0.439	0.471
51	0.46821	0.01041	46.00	0.123	0.154	0.186	0.217	0.248	0.279	0.310	0.340	0.370	0.400	0.430	0.459
52	0.52486	0.01296	47.00	0.151	0.178	0.206	0.233	0.261	0.288	0.316	0.343	0.370	0.397	0.424	0.450
53	0.58152	0.01510	48.00	0.177	0.201	0.226	0.250	0.274	0.298	0.323	0.347	0.371	0.395	0.419	0.443
54	0.63745	0.01667	49.00	0.201	0.222	0.243	0.265	0.286	0.308	0.329	0.351	0.373	0.395	0.416	0.438
55	0.69190	0.01759	50.00	0.223	0.242	0.260	0.279	0.298	0.317	0.336	0.356	0.375		0.414	0.434
56	0.74412	0.01779	51.00	0.244	0.260	0.276	0.292	0.309	0.326	0.343	0.360	0.378		0.413	0.431
57	0.79336	0.01725	52.00	0.263	0.276	0.290	0.305	0.319	0.334	0.349	0.365	0.380	0.396	0.412	0.428
58	0.83888	0.01593	53.00	0.280	0.291	0.303	0.316	0.329	0.342	0.355	0.369	0.382		0.411	0.425
59	0.87997	0.01390	54.00	0.295	0.305	0.315	0.326	0.337	0.348	0.360	0.372	0.384		0.409	0.422
60	0.91590	0.01120	55.00	0.302	0.310	0.319	0.328	0.338	0.348	0.358	0.368	0.379	0.390	0,402	0.413
61	0.94594	0.00809	56.00	0.298	0.305	0.313	0.321	0.329	0.337	0.346	0.356	0.365			0.396
62	0.96955	0.00501	57.00	0.287	0.293	0.300	0.306	0.313	0.321	0.329	0.337	0.345		0.363	0.373
63	0.98647	0.00240	58.00	0.274	0.279	0.284	0.289	0.295	0.302	0.308	0.315	0.323	0.330	0.339	0.347
64	0.99662	0.00063	59.00	0.264	0.267	0.271	0.275	0.280	0.285	0.290	0.296	0.302	0.309	0.316	0.323
65	1.00000	0.00000	60.00	0.262	0.263	0.266	0.269	0.272	0.276	0.280	0.284	0.289	0.295	0.301	0.307
ALPHA	AU≃ 6.82 I	DEGREES C	:MU=-0.1	740 ETA= 1	1.084										

*-WARNING 1996 ALPHA REL. CH
ALPHA (DEG.) R= 500000 MU=300
-1.73 S TURB S SEP CD
UPPER 0.4135 0.0998 0.0061*
LOWER 1.0017 0.0000 0.0043*
TOTAL CL= 0.551 CD=0.01047
CM=-0.1784
-1.00 S TURB S SEP CD
UPPER 0.4193 0.0117 0.0604*
LOWER 0.4619 0.0000 0.0023
TOTAL CL= 0.652 CD=0.00870
CM=-0.1790
0.00 S TURB S SEP CD
UPPER 0.4276 0.0149 0.0669*
LOWER 0.3161 0.0000 0.0018
TOTAL CL= 0.629 CD=0.00871
CM=-0.1797
1.00 S TURB S SEP CD
UPPER 0.4372 0.0186 0.0073*
LOWER 0.3161 0.0000 0.0018
TOTAL CL= 0.4372 0.0186 0.0073*
LOWER 0.1902 0.0000 0.0015
TOTAL CL= 0.4840 CD=0.00873
CM=-0.1801
3.00 S TURB S SEP CD
UPPER 0.4487 0.0212 0.0077*
LOWER 0.0000 0.0000 0.0010
TOTAL CL= 0.946 CD=0.00873
CM=-0.1811
3.00 S TURB S SEP CD
UPPER 0.46487 0.0212 0.0077*
LOWER 0.0000 0.0000 0.0010
TOTAL CL= 0.946 CD=0.00896
CM=-0.1821
4.00 S TURB S SEP CD
UPPER 0.4625 0.0228 0.0080*
LOWER 0.0000 0.0000 0.0010
TOTAL CL= 1.158 CD=0.00896
CM=-0.1821
4.00 S TURB S SEP CD
UPPER 0.4788 0.0259 0.0084*
LOWER 0.0000 0.0000 0.0009
TOTAL CL= 1.158 CD=0.00997
CM=-0.1825
5.00 S TURB S SEP CD
UPPER 0.4997 0.0285 0.0090*
LOWER 0.0000 0.0000 0.0009
TOTAL CL= 1.263 CD=0.00989
CM=-0.1835
6.00 S TURB S SEP CD
UPPER 0.5345 0.0310 0.0097*
LOWER 0.0000 0.0000 0.0009
TOTAL CL= 1.368 CD=0.01055
CM=-0.1831
7.03

R= 500000 MU=100
S TURB S SEP CD
1.0049 0.0136 0.0096
1.0017 0.0000 0.0043*
CL= 0.547 CD=0.01393
CM=-0.1775
S TURB S SEP CD
1.0049 0.0161 0.0101
0.9516 0.0000 0.0036
CL= 0.625 CD=0.01373
CM=-0.1780
S TURB S SEP CD
1.0049 0.0196 0.0109
0.9516 0.0000 0.0033
CL= 0.730 CD=0.01423
CM=-0.1786
S TURB S SEP CD
1.0049 0.0233 0.0118
0.9516 0.0000 0.0033
CL= 0.730 CD=0.01443
CM=-0.1791
S TURB S SEP CD
1.0049 0.0233 0.0118
0.9516 0.0000 0.0036
CL= 0.835 CD=0.01484
CM=-0.1791
S TURB S SEP CD
1.0049 0.0393 CD=0.01556
CM=-0.1795
S TURB S SEP CD
1.0049 0.0319 0.0138
0.9516 0.0000 0.0022
CL= 1.042 CD=0.01641
CM=-0.1797
S TURB S SEP CD
1.0049 0.0369 0.0150
0.9516 0.0000 0.0022
CL= 1.144 CD=0.0173
CM=-0.1797
S TURB S SEP CD
1.0049 0.0428 0.0164
0.9516 0.0000 0.0022
CL= 1.245 CD=0.01861
CM=-0.1797
S TURB S SEP CD
1.0049 0.0491 0.0179
0.9516 0.0000 0.0022
CL= 1.344 CD=0.01895
CM=-0.1798
S TURB S SEP CD
1.0049 0.0546 0.0195*
0.9516 0.0000 0.0022
CL= 1.444 CD=0.01985
CM=-0.1798
S TURB S SEP CD
1.0049 0.0564 0.0195*
0.9516 0.0000 0.0021
S TURB S SEP CD
1.0049 0.0564 0.0195*
0.9516 0.0000 0.00195*
0.9516 0.0000 0.00195
S TURB S SEP CD
1.0049 0.0566 0.0195*
0.9516 0.0000 0.00195
S TURB S SEP CD
1.0049 0.0566 0.0195*
0.9516 0.0000 0.00195
S TURB S SEP CD
1.0049 0.0566 0.0195*
0.9516 0.0000 0.00195
S TURB S SEP CD
1.0049 0.0566 0.0195*

R= 500000 MU=900
S TURB S SEP CD
0.7005 0.0106 0.0081
1.0017 0.0000 0.0043*
CL= 0.550 CD= 0.01242
CM=-0.1782
S TURB S SEP CD
0.7372 0.0132 0.0087
0.9224 0.0000 0.0035
CL= 0.627 CD=0.01224
CM=-0.1786
S TURB S SEP CD
0.7814 0.0169 0.0096
0.8699 0.0000 0.0031
CL= 0.733 CD=0.01275
CM=-0.1792
S TURB S SEP CD
0.8221 0.0209 0.0106
0.8208 0.0000 0.0028
CL= 0.838 CD=0.01341
CM=-0.1797
S TURB S SEP CD
0.8251 0.0116
0.7717 0.0000 0.0025
CL= 0.942 CD=0.01417
CM=-0.1801
S TURB S SEP CD
0.8578 0.0257 0.0128
0.7226 0.0000 0.0023
CL= 1.045 CD=0.01508
CM=-0.1803
S TURB S SEP CD
0.9193 0.0348 0.0140
0.6720 0.0000 0.0021
CL= 1.147 CD=0.01615
CM=-0.1803
S TURB S SEP CD
0.9193 0.0348 0.0140
0.6720 0.0000 0.0021
CL= 1.147 CD=0.01613
CM=-0.1803
S TURB S SEP CD
0.9193 0.0348 0.0140
0.6720 0.0000 0.0021
CL= 1.248 CD=0.01615
S TURB S SEP CD
0.9474 0.0406 0.0155
0.6212 0.0000 0.0017
CM=-0.1803
S TURB S SEP CD
0.9739 0.0478 0.0173
0.5687 0.0000 0.0017
CL= 1.248 CD=0.01740
CM=-0.1803
S TURB S SEP CD
0.9739 0.0478 0.0173
0.5687 0.0000 0.0017
CL= 1.346 CD=0.01902
CM=-0.1783
S TURB S SEP CD
0.9739 0.0478 0.0173
0.5687 0.0000 0.0017
CL= 1.346 CD=0.01902
CM=-0.1783
S TURB S SEP CD
0.9978 0.0555 0.0193
0.5160 0.0000 0.0016
CL= 1.442 CD=0.02086
CM=-0.1783

S TURB S SEP CD 1.0000 0.0569 0.0195 0.5097 0.0000 0.0015 CL= 1.452 CD=0.02108 CM=-0.1781

7.38 S TURB S SEP CD UPPER 0.9594 0.0578 0.0195* LOWER 0.0000 0.0000 0.0008 TOTAL CL= 1.480 CD=0.02028 CM=-0.1782

**AWAINING 1995 ** ALPHA REL. CF.

LUPHA (DEG.) R= 600000 ** MU=300 1.79 S TURB S SEP CD UPPER 0. 4130 0. 0.066 0.0056 LOWER 1.0017 0.0000 0.0043** TOTAL CL= 0.547 CD=0.00987
-1.00 S TURB S SEP CD UPPER 0. 4193 0.0088 0.0059** LOWER 0.4799 0.0000 0.0022
TOTAL CL= 0.632 CD=0.00813
CM=-0.1797

0.00 S TURB S SEP CD UPPER 0. 4276 0.0118 0.0063** LOWER 0.4276 0.0118 0.0063** LOWER 0.4376 0.018 0.0063** LOWER 0.4372 0.0447 0.0063** LOWER 0.4372 0.0447 0.0067** LOWER 0.4372 0.0147 0.0067** LOWER 0.4252 0.0000 0.0011** CD=0.00812
CM=-0.1813
2.00 S TURB S SEP CD UPPER 0.4487 0.0170 0.0070** LOWER 0.0488 0.0000 0.0011** TOTAL CL= 0.844 CD=0.00812
CM=-0.1813
2.00 S TURB S SEP CD UPPER 0.4487 0.0170 0.0070** LOWER 0.0948 0.0000 0.0011** TOTAL CL= 0.951 CD=0.00818
CM=-0.1822
3.00 S TURB S SEP CD UPPER 0.4625 0.189 0.0073** LOWER 0.0000 0.0000 0.0009** TOTAL CL= 1.058 CD=0.00823
CM=-0.1832
4.00 S TURB S SEP CD UPPER 0.4788 0.0220 0.0078** LOWER 0.0000 0.0000 0.0009** TOTAL CL= 1.163 CD=0.00868
TOTAL CL= 1.163 CD=0.00864
TOTAL CL= 1.163 CD=0.00868
TOTAL CL= 1.163 CD=0.00864
TOTAL CL= 1.163 CD=0.00864
TOTAL CL= 1.163 CD=0.00868
TOTA R= 600000 MU=900 S TURB S SEP CD 0.7278 0.0096 0.0080 1.0017 0.0000 0.0043* CL= 0.544 CD=0.01223 CM=-0.1783 ALPHA(DEG.) R= 600000 MU=300 R= 600000 MU=100 S TURB S SEP CD 1.0049 0.0122 0.0093 1.0017 0.0000 0.0043* 1.0017 0.0000 0.0043.
CL= 0.542 CD=0.01356
CM=-0.1777
S TURB S SEP CD
1.0049 0.0149 0.0099
0.9516 0.0000 0.0035
CL= 0.626 CD=0.01334
CM=-0.1783
S TURB S SEP CD
1.0049 0.0183 0.0106
0.9516 0.0000 0.0032
CL= 0.731 CD=0.01383
CM=-0.1789
S TURB S SEP CD
1.0049 0.0221 0.0115
0.9516 0.0000 0.0029
CL= 0.836 CD=0.01442
CM=-0.1794
S TURB S SEP CD
1.0049 0.0260 0.0124
CM=-0.1794
S TURB S SEP CD
1.0049 0.0260 0.0124
CM=-0.1794
S TURB S SEP CD
1.0049 0.0260 0.0124
0.9516 0.0000 0.0027
CL= 0.941 CD=0.01512
CM=-0.1794
CM=-0.1798
S TURB S SEP CD
1.0049 0.0304 0.0134
0.9516 0.0000 0.0025
CL= 1.044 CD=0.01593
CM=-0.1801
S TURB S SEP CD
1.0049 0.0353 0.0146
0.9516 0.0000 0.0023
CL= 1.146 CD=0.01687
CM=-0.1802
S TURB S SEP CD
1.0049 0.0405 0.0128
CM=-0.1802
S TURB S SEP CD CM=-0.1785
S TURE S SEP CD
0.7620 0.0123 0.0086
0.9299 0.0000 0.0034
CL= 0.628 CD=0.01202
CM=-0.1788
S TURE S SEP CD
0.8021 0.0160 0.0095
0.8806 0.0000 0.0030
CL= 0.734 CD=0.01250
CM=-0.1794
S TURE S SEP CD
0.8326 0.0000 0.0030
CL= 0.734 CD=0.01250
CM=-0.1794
CM=-0.1800
S TURE S SEP CD
0.8346 0.0000 0.0027
CL= 0.839 CD=0.01311
CM=-0.1800
S TURE S SEP CD
0.8710 0.0239 0.0114
0.7883 0.0000 0.0025
CL= 0.943 CD=0.01384
CM=-0.1804
S TURE S SEP CD
0.9013 0.0284 0.0125
0.7421 0.0000 0.0025
CL= 1.047 CD=0.01471
CM=-0.1806
S TURE S SEP CD
0.9281 0.0334 0.0127
0.9281 0.0334 0.0137
0.6943 0.0000 0.0020
CL= 1.149 CD=0.01572
CM=-0.1807
S TURE S SEP CD CM=-0.1839
5.00 S TURB S SEP CD
UPPER 0.4997 0.0246 0.0084*
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.268 CD=0.00915
CM=-0.1847
6.00 S TURB S SEP CD
UPPER 0.5599 0.0280 0.0095 5.00 0.6453 0.0000 0.0019 CL= 1.250 CD=0.01695 CM=-0.1805 S TURB S SEP CD 0.9791 0.0460 0.0168 0.5959 0.0000 0.0017 CL= 1.348 CD=0.01851 CM=-0.1799 0.9516 0.0000 0.0021 CL= 1.248 CD=0.01795 CM=-0.1801 S TURB S SEP CD 1.0049 0.0471 0.0173 0.9516 0.0000 0.0020 CL= 1.347 CD=0.01927 CM=-0.1796 LOWER 0.0000 0.0000 0.0007 TOTAL CL= 1.372 CD=0.01028 CM=-0.1852 CM=-0.1796
S TURB S SEP CD
1.0049 0.0541 0.0188*
0.9516 0.0000 0.0018
CL= 1.444 CD=0.2067
CM=-0.1788
S TURB S SEP CD
1.0049 0.0550 0.0199*
0.9516 0.0000 0.0018
CL= 1.455 CD=0.02085
CM=-0.1787 7.00 7.00 S TURB S SEP CD UPPER 0.7365 0.0393 0.0131 LOWER 0.0000 0.0000 0.0007 TOTAL CL= 1.465 CD=0.01385 S TURB S SEP CD 1.0012 0.0539 0.0187 0.5465 0.0000 0.0015 CL= 1.445 CD=0.02028 CM = -0.1833CM=-0.1789 S TURB S SEP CD 1.0038 0.0550 0.0190 0.5390 0.0000 0.0015 CL= 1.458 CD=0.02054 CM=-0.1787 7.14

7.40 S TURB S SEP CD UPPER 0.9641 0.0557 0.0189* LOWER 0.0000 0.0000 0.0007 TOTAL CL= 1.485 CD=0.01962 CM=-0.1788

ALPHA(DEG.) R= 700000 MU=300 R= 700000 MU=100 R= 700000 MU=100 S TURB S SEP CD 1.0049 0.0111 0.0090 1.0018 0.0000 0.0042* CL= 0.536 CD=0.01326 CM=-0.1779 S TURB S SEP CD 1.0049 0.0138 0.0096 0.9515 0.0000 0.0034 CL= 0.627 CD=0.01302 CM=-0.1785 S TURB S SEP CD 1.85 S TURB S SEP CD UPPER 0.4126 0.0043 0.0052* LOWER 1.0018 0.0000 0.0042* CL= 0.627 CD=0.01302
CM=-0.1785
S TURB S SEP CD
1.0049 0.0173 0.0104
0.9516 0.0000 0.0031
CL= 0.732 CD=0.01350
CM=-0.1791
S TURB S SEP CD
1.0049 0.0210 0.0112
0.9516 0.0000 0.0029
CL= 0.838 CD=0.01408
CM=-0.1797
S TURB S SEP CD
1.0049 0.0249 0.0121
0.9516 0.0000 0.0026
CL= 0.838 CD=0.01475
CM=-0.1801
S TURB S SEP CD
1.0049 0.0249 0.0121
0.9516 0.0000 0.0026
CL= 0.942 CD=0.01475
CM=-0.1801
S TURB S SEP CD
1.0049 0.0292 0.0131
0.9516 0.0000 0.0024
CL= 1.046 CD=0.01554
CM=-0.1804
S TURB S SEP CD
1.0049 0.0339 0.0142
0.9516 0.0000 0.0023
CL= 1.148 CD=0.01644
CM=-0.1805
S TURB S SEP CD
1.0049 0.0339 0.0142
0.9516 0.0000 0.0023
CL= 1.148 CD=0.01644
CM=-0.1805
S TURB S SEP CD CM=-0.1811 1.00 S TURB S SEP CD UPPER 0.4372 0.0120 0.0063* LOWER 0.2545 0.0000 0.0014 UPPER 0.4372 0.0120 0.0063*
LOMER 0.2545 0.0000 0.0014
TOTAL CL= 0.847 CD=0.00768
CM=-0.1820
2.00 S TURB S SEP CD
UPPER 0.4487 0.0141 0.0066*
LOMER 0.1314 0.0000 0.0011
TOTAL CL= 0.954 CD=0.00769
CM=-0.1830
3.00 S TURB S SEP CD
UPPER 0.4625 0.0163 0.0069*
LOMER 0.0000 0.0000 0.0008
TOTAL CL= 1.061 CD=0.00774
CM=-0.1840
4.00 S TURB S SEP CD
UPPER 0.4788 0.0193 0.0074*
LOWER 0.0000 0.0000 0.0008
TOTAL CL= 1.166 CD=0.00816
CM=-0.1847
5.00 S TURB S SEP CD
UPPER 0.5033 0.0215 0.0079*
LOWER 0.5033 0.0215 0.0079* CM=-0.1805 S TURB S SEP CD 1.0049 0.0391 0.0154 0.9516 0.0000 0.0021 CL= 1.250 CD=0.01749 CM=-0.1805 S TURB S SEP CD 1.0049 0.0454 0.0168 0.9516 0.0000 0.0019 CM=-1.349 CD=0.01876 CM=-0.1856
6.00 S TURB S SEP CD
UPPER 0.5858 0.0267 0.0095
LOWER 0.0000 0.0000 0.0007
TOTAL CL= 1.374 CD=0.01021
CM=-0.1856
7.00 S TURB S SEP CD
UPPER 0.7635 0.0387 0.0131
LOWER 0.0000 0.0000 0.0007
TOTAL CL= 1.466 CD=0.01379
CM=-0.1834 0.9516 0.0000 0.0019 CL= 1.349 CD=0.01876 CM=-0.1800 S TURB S SEP CD 1.0049 0.0522 0.0183* 0.9516 0.0000 0.0018 CL= 1.447 CD=0.02011 CM=-0.1794 7.18

> S TURB S SEP CD 1.0049 0.0536 0.0186* 0.9516 0.0000 0.0018 CL= 1.465 CD=0.02041 CM=-0.1792

R= 700000 MU=900 S TURB S SEP CD 0.7484 0.0087 0.0078 1.0018 0.0000 0.0042* CL= 0.539 CD=0.01206 CM=-0.1784 S SEP CD 0.7811 0.0115 0.0085 0.9358 0.0000 0.0034 CL= 0.629 CD=0.01184 CM=-0.1790 S SEP CD CM=-0.1790
S TURB S SEP CD
0.8180 0.0151 0.0093
0.8891 0.0000 0.0030
CL= 0.735 CD=0.01229
CM=-0.1797
S TURB S SEP CD
0.8509 0.0189 0.0102
0.8454 0.0000 0.0027
CL= 0.8464 CD=0.01287
CM=-0.1802
S TURB S SEP CD
0.8816 0.0229 0.0111
0.8014 0.0000 0.0024
CL= 0.944 CD=0.01358
CM=-0.1806
S TURB S SEP CD
0.9094 0.0273 0.0122
0.7575 0.0000 0.0022
CL= 1.048 CD=0.01440 CL= 1.048 CD=0.01440 CM=-0.1809 S TURB S SEP CD 0.9351 0.0322 0.0134 0.7120 0.0000 0.0020 CL= 1.150 CD=0.01539 CM=-0.1810 CM=-0.1810 S TURB S SEP CD 0.9599 0.0377 0.0147 0.6654 0.0000 0.0018 CL= 1.251 CD=0.01658 CM=-0.1809 S TURB S SEP CD 0.9832 0.0445 0.0164 0.6184 0.0000 0.0017 CL= 1.350 CD=0.01809 CM=-0.1803 S TURB S SEP CD 1.0039 0.0521 0.0183 0.5707 0.0000 0.0015 CL= 1.477 CD=0.01803 CM=-0.1794 S TURB S SEP CD CM=-0.1794 S TURB S SEP CD 1.0070 0.0536 0.0186 0.5615 0.0000 0.0015 CL= 1.464 CD=0.02013 CM=-0.1792

R= 700000 MU=900

7.19

7.44 S TURB S SEP CD UPPER 0.9718 0.0543 0.0186* LOWER 0.0000 0.0000 0.0006 TOTAL CL= 1.491 CD=0.01921 CM=-0.1793

*-WARNII	NG 1996 ALPHA REL. CHO	RD LINE	
ALPHA (DEC -1.91 UPPER LOWER TOTAL -1.00 UPPER LOWER TOTAL 1.00 UPPER LOWER TOTAL 1.00 UPPER LOWER TOTAL 3.00 UPPER LOWER TOTAL 4.00 UPPER LOWER TOTAL 5.00 UPPER LOWER TOTAL 6.00 UPPER LOWER TOTAL 1.00 UPPER LOWER LOWE		R= 800000 MU=100 STURE S SEP CD 1.0049 0.0101 0.0088 1.0018 0.0000 0.0042* CL= 0.531 CD=0.01300 CM=-0.1780 STURE S SEP CD 1.0049 0.0130 0.0094 0.9516 0.0000 0.0033 CL= 0.628 CD=0.01275 CM=-0.1787 STURE S SEP CD 1.0049 0.0154 0.0102 0.9516 0.0000 0.0031 CL= 0.733 CD=0.01322 CM=-0.1793 STURE S SEP CD 1.0049 0.0200 0.0110 0.9516 0.0000 0.0012 STURE S SEP CD 1.0049 0.0210 0.0110 0.9516 0.0000 0.0028 CL= 0.839 CD=0.01378 CM=-0.1799 STURE S SEP CD 1.0049 0.0239 0.0118 0.9516 0.0000 0.0026 CL= 0.943 CD=0.01444 CM=-0.1804 STURE S SEP CD 1.0049 0.0281 0.0128 0.9516 0.0000 0.0024 CL= 1.047 CD=0.01521 CM=-0.1793 STURE S SEP CD 1.0049 0.0328 0.0119 0.9516 0.0000 0.0024 CL= 1.051 CD=0.01609 CM=-0.1809 STURE S SEP CD 1.0049 0.0328 0.0151 0.9516 0.0000 0.0022 CL= 1.151 CD=0.01609 CM=-0.1809 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0024 CL= 1.511 CD=0.01609 CM=-0.1809 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0024 CL= 1.511 CD=0.01609 CM=-0.1808 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0024 CL= 1.511 CD=0.01710 CM=-0.1808 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0020 CL= 1.511 CD=0.01710 CM=-0.1808 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0020 CL= 1.511 CD=0.01710 CM=-0.1808 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0020 CM=-0.1808 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0020 CM=-0.1808 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0020 CM=-0.1808 STURE S SEP CD 1.0049 0.0379 0.0151 0.9516 0.0000 0.0020 CM=-0.1808 STURE S SEP CD 1.0049 0.0400 0.0164 CM=-0.1808 STURE S SEP CD 1.0049 0.0400 0.0164 CM=-0.1808 STURE S SEP CD	R= 800000 MU=900 S TURE S SEP CD 0.7628 0.0079 0.0077 1.0018 0.0000 0.0042* CL= 0.533 CD=0.01190 CM=-0.1785 S TURE S SEP CD 0.7960 0.0108 0.0083 CL= 0.630 CD=0.01167 CM=-0.1792 S TURE S SEP CD 0.8304 0.0143 0.0092 CL= 0.630 CD=0.01167 CM=-0.1792 S TURE S SEP CD 0.8304 0.0143 0.0092 CL= 0.735 CD=0.01210 CM=-0.1798 S TURE S SEP CD 0.8613 0.0181 0.0100 0.8541 0.0000 0.0026 CL= 0.841 CD=0.01266 CM=-0.1804 S TURE S SEP CD 0.8120 0.0000 0.0024 CL= 0.045 CD=0.01335 CM=-0.1804 S TURE S SEP CD 0.8120 0.0000 0.0024 CL= 0.049 CD=0.01415 CM=-0.1819 S TURE S SEP CD 0.9458 0.0120 0.0120 0.7700 0.0000 0.0022 CL= 1.049 CD=0.01415 CM=-0.1812 S TURE S SEP CD 0.9408 0.012 0.0131 0.7265 0.0000 0.0022 CL= 1.049 CD=0.01511 CM=-0.1813 S TURE S SEP CD 0.9643 0.0366 0.0151 CM=-0.1812 S TURE S SEP CD 0.9646 0.0432 0.0161 0.6371 0.0000 0.0018 CL= 1.552 CD=0.01774 CM=-0.1812 S TURE S SEP CD 0.9866 0.0432 0.0161 0.6371 0.0000 0.0018 CL= 1.449 CD=0.01774 CM=-0.1807 S TURE S SEP CD 0.9866 0.0432 0.0161 0.6371 0.0000 0.0018 CL= 1.449 CD=0.01774 CM=-0.1807 S TURE S SEP CD 0.9866 0.0432 0.0161 0.6371 0.0000 0.0018 CL= 1.449 CD=0.01940 CM=-0.1798 S TURE S SEP CD 1.0061 0.0506 0.0179
7.22		S TURB S SEP CD 1.0049 0.0522 0.0182* 0.9516 0.0000 0.0017 CL= 1.471 CD=0.01997 CM=-0.1797	CL= 1.465 CD=0.01971 CM=-0.1796
LOWER	S TURB S SEP CD 0.9773 0.0529 0.0182* 0.0000 0.0000 0.0006 CL= 1.496 CD=0.01877 CM=-0.1798		

ALPHA(DEG.) R= 900000 MU=300 R= 900000 MU=100 1.96 S TURB S SEP CD UPPER 0.4117 0.0003 0.0048* LOWER 1.0018 0.0000 0.0041* S TURB S SEP CD 1.0049 0.0092 0.0086 1.0018 0.0000 0.0041* 1.0018 0.0000 0.0041*
CL= 0.526 CD=0.01277
CM=-0.1781
S TURB S SEP CD
1.0049 0.0122 0.0093
0.9516 0.0000 0.0033
CL= 0.628 CD=0.01252
CM=-0.1789
S TURB S SEP CD TOTAL CL= 0.534 CD=0.00891 CM=-0.1801 1.00 S TURB S SEP CD UPPER 0.4193 0.0034 0.0050* LOWER 0.5440 0.0000 0.0022 TOTAL CL= 0.637 CD=0.00718 CM=-0.1809 CH=-0.1789 SEP CD
1.0049 0.0156 0.0100
0.9516 0.0000 0.0030
CL= 0.734 CD=0.01298
CM=-0.1795
S TURB S SEP CD
1.0049 0.0192 0.0108
0.9516 0.0000 0.0028
CL= 0.840 CD=0.01353
CM=-0.1801
S TURB S SEP CD
1.0049 0.0230 0.0116
0.9516 0.0000 0.0028
CL= 0.844 CD=0.01418
CM=-0.1806
S TURB S SEP CD
1.0049 0.0230 0.0116
0.9516 0.0000 0.0026
CL= 0.944 CD=0.01418
CM=-0.1806
S TURB S SEP CD
1.0049 0.0271 0.0126
0.9516 0.0000 0.0024
CL= 1.048 CD=0.01498 TOTAL CL = 1.065 CD=0.00704

CM=-0.1850
4.00 S TURB S SEP CD
UPPER 0.4798 0.0153 0.0067*
LOWER 0.0000 0.0000 0.0007
TOTAL CL = 1.171 CD=0.00742
CM=-0.1859
5.00 S TURB S SEP CD 0.9516 0.0000 0.0024 CL= 1.048 CD=0.01492 CM=-0.1810 S TURB S SEP CD 1.0049 0.0318 0.0136 0.9516 0.0000 0.0022 CL= 1.151 CD=0.01578 CM=-0.1811 CM=-0.1859
5.00 S TURB S SEP CD
UPPER 0.5290 0.0188 0.0077
LOWER 0.0000 0.0000 0.0006
TOTAL CL= 1.276 CD=0.00830
CM=-0.1865
6.00 S TURB S SEP CD
UPFER 0.6370 0.0260 0.0097
LOWER 0.0000 0.0000 0.0006
TOTAL CL= 1.375 CD=0.01028
CM=-0.1859
7.00 S TURB S SEP CD
UPFER 0.8001 0.0377 0.0131
LOWER 0.0000 0.0000 0.0006
TOTAL CL= 1.467 CD=0.01363
CM=-0.1858 CM=-0.1811 S TURB S SEP CD 1.0049 0.0368 0.0148 0.9516 0.0000 0.0020 CL= 1.253 CD=0.01677 CM=-0.1812 S TURB S SEP CD 1.0049 0.0428 0.0161 0.9516 0.0000 0.0019 CL= 1.353 CD=0.01797 CM=-0.1808 S TURB S SEP CD 1.0049 0.0491 0.0175* 0.9516 0.0000 0.0017 0.9516 0.0000 0.0017 0.9516 0.0000 0.0017 CL= 1.451 CD=0.01923 CM=-0.1803 7.19

R= 900000 MU=900 S TURE S SEP CD 0.7750 0.0071 0.0076 1.0018 0.0070 0.0076 1.0018 0.0000 0.0041* CL= 0.528 CD= 0.01176 CM=-0.1786 S TURE S SEP CD 0.8083 0.9443 0.0000 0.0032 CL= 0.630 CD=0.01153 CM=-0.1793 S TURE S SEP CD 0.8404 0.0137 0.0090 0.9017 0.0000 0.0029 CL= 0.736 CD=0.01194 CM=-0.1806 S TURE S SEP CD 0.8698 0.0173 0.0099 0.8616 0.0000 0.0026 CL= 0.841 CD=0.01248 CM=-0.1806 S TURE S SEP CD 0.8970 0.0213 0.0108 0.8211 0.0000 0.0024 CL= 0.946 CD=0.01315 CM=-0.1811 S TURE S SEP CD 0.9216 0.0255 0.0118 0.9216 0.0255 0.0118 0.7809 0.0000 0.0022 CL= 1.050 CD=0.0133 CM=-0.1814 S TURE S SEP CD 0.9216 0.0255 0.0118 0.7809 0.0000 0.0022 CL= 1.050 CD=0.0133 CM=-0.1814 S TURE S SEP CD 0.9456 0.0303 0.0129 0.7389 0.0000 0.0022 CL= 1.153 CD=0.01315 CM=-0.1814 S TURE S SEP CD 0.9456 0.0303 0.0129 0.7389 0.0000 0.0022 CL= 1.153 CD=0.01487 CM=-0.1816 CD=0.0000 0.0022 CD=0.01487 CM=-0.1816 CD=0.014 CM=-0.1816
S TURB S SEP CD
0.9680 0.0356 0.0142
0.6961 0.0000 0.0018
CL= 1.254 CD=0.01599
CM=-0.1815
S TURB S SEP CD
0.9894 0.0421 0.0158
0.6528 0.0000 0.0016
CL= 1.353 CD=0.01744
CM=-0.1810
S TURB S SEP CD
1.0079 0.0493 0.0176
0.6078 0.0000 0.0015
CL= 1.451 CD=0.01906
CM=-0.1808 S SEP CD CM=-0.1802 S TURB S SEP CD 1.0109 0.0508 0.0179 0.5990 0.0000 0.0015 CL= 1.469 CD=0.01940 CM=-0.1800

7.27

S TURB S SEP CD 1.0049 0.0511 0.0179* 0.9516 0.0000 0.0017 CL= 1.477 CD=0.01964 CM=-0.1800 7.48 S TURB S SEP CD UPPER 0.9795 0.0516 0.0178* LOWER 0.0000 0.0000 0.0006 TOTAL CL= 1.499 CD=0.01840 CM=-0.1802

ALPHA(DEG.) R= 1000000 MII=300 R= 1000000 MU=100 LPHA (DEG.) R= 1000000 MU=300 -2.01 S TORB S SEP CD UPPER 0.4113 0.0000 0.0046* LOWER 1.0018 0.0000 0.0041* TOTAL CL= 0.529 CD=0.00868 CM=-0.1801 R= 1000000 MU=100 S TURB S SEP CD 1.0049 0.0083 0.0085 1.0018 0.0000 0.0041* CL= 0.521 CD=0.01257 CM=-0.1783 CM=-0.1801
2.00 S TURE S SEP CD
UPPER 0.4114 0.0000 0.0046*
LOWER 1.0018 0.0000 0.0041*
TOTAL CL= 0.530 CD=0.00868
CM=-0.1801
1.00 S TURE S SEP CD
UPPER 0.4193 0.0020 0.0048*
LOWER 0.5607 0.0000 0.0021
TOTAL CL= 0.638 CD=0.00690
CM=-0.1813
0.00 S TURE S SEP CD
UPPER 0.4276 0.0047 0.0051*
LOWER 0.3477 0.0000 0.0051*
LOWER 0.3437 0.0000 0.0017
TOTAL CL= 0.745 CD=0.00689
CM=-0.1822
1.00 S TURE S SEP CD CM=-0.1783
S TURB S SEP CD
1.0049 0.0084 0.0085
1.0018 0.0000 0.0041*
CL= 0.522 CD=0.01257
CM=-0.1783
S TURB S SEP CD
1.0049 0.0115 0.0091
0.9516 0.0000 0.0032
CL= 0.629 CD=0.01231
CM=-0.1790
S TURB S SEP CD -2.00 -1.00 CM=-0.1790 S TURE S SEP CD 1.0049 0.0149 0.0098 0.9516 0.0000 0.0029 CL= 0.735 CD=0.01277 CM=-0.1797 1.00 1.00 S TURB S SEP CD UPPER 0.4372 0.0069 0.0054* LOWER 0.3219 0.0000 0.0014 S TURB S SEP CD 1.0049 0.0184 0.0106 0.9516 0.0000 0.0027 UPPER 0.4372 0.0069 0.0054*
LOWER 0.3219 0.0000 0.0014
TOTAL CL= 0.853 CD=0.00686
CM=-0.1833
2.00 S TURB S SEP CD
UPPER 0.4487 0.0088 0.0057*
LOWER 0.2073 0.0000 0.0011
TOTAL CL= 0.960 CD=0.00681
CM=-0.1844
3.00 S TURB S SEP CD
UPPER 0.4625 0.0113 0.0061*
LOWER 0.0000 0.0000 0.0007
TOTAL CL= 1.067 CD=0.00676
CM=-0.1854
4.00 S TURB S SEP CD
UPPER 0.4876 0.0139 0.0066
LOWER 0.0000 0.0000 0.0007
TOTAL CL= 1.173 CD=0.00723
CM=-0.1863
5.00 S TURB S SEP CD
UPPER 0.5421 0.0181 0.0076
LOWER 0.0000 0.0000 0.0007
TOTAL CL= 1.173 CD=0.00723
CM=-0.1863
5.00 S TURB S SEP CD
UPPER 0.5421 0.0181 0.0076
LOWER 0.0000 0.0000 0.0007
CDTAL CL= 1.277 CD=0.00822
CM=-0.1867 CL= 0.840 CD=0.01331 CM=-0.1803 S TURB S SEP CD 1.0049 0.0222 0.0114 0.9516 0.0000 0.0025 CL= 0.945 CD=0.01394 CM=-0.1808 CM=-0.1808 S TURB S SEP CD 1.0049 0.0263 0.0124 0.9516 0.0000 0.0023 CL= 1.049 CD=0.01467 CM=-0.1812 S TURB S SEP CD 1.0049 0.0308 0.0134 0.9516 0.0000 0.0021 CL= 1.152 CD=0.01551 CM=-0.1814 S TURB S SEP CD 1.0049 0.0358 0.0145 0.9516 0.0000 0.020 CL= 1.254 CD=0.01648 CM=-0.1814 S TURB S SEP CD CM=-0.1867
6.00 STURB S SEP CD
UPFER 0.6608 0.0259 0.0098
LOWER 0.0000 0.0000 0.0005
TOTAL CLE 1.375 CD=0.01037
CM=-0.1859
7.00 STURB S SEP CD
UPPER 0.8129 0.0372 0.0130
LOWER 0.0000 0.0000 0.0005
TOTAL CLE 1.468 CD=0.01354
CM=-0.1839
7.24 CM=-0.1814
S TURB S SEP CD
1.0049 0.0417 0.0158
0.9516 0.0000 0.0018
CLE 1.354 CD=0.01765
CM=-0.1811
S TURB S SEP CD
1.0049 0.0479 0.0172
0.9516 0.0000 0.0017
CLE 1.453 CD=0.01887
CM=-0.1807

> S TURB S SEP CD 1.0049 0.0504 0.0177* 0.9516 0.0000 0.0017 CL= 1.487 CD=0.01940 CM=-0.1804

CLE - 0.524 CDE. 0.1162
CM=-0.1787
S TURB S SEP CD
0.8189 0.0097 0.0082
0.9475 0.0000 0.0032
CL= 0.631 CD=0.01140
CM=-0.1795
S TURB S SEP CD
0.8487 0.0130 0.0089
0.9066 0.0000 0.0029
CLE - 0.737 CD=0.01177
CM=-0.1802
S TURB S SEP CD
0.8770 0.0167 0.0097
0.8679 0.0000 0.0022
CLE - 0.842 CD=0.01232
CM=-0.1808
S TURB S SEP CD
0.9028 0.0206 0.0106
0.8289 0.0000 0.0022
CLE - 0.842 CD=0.01237
CM=-0.1812
S TURB S SEP CD
0.9028 0.0206 0.0106
0.8289 0.0000 0.0022
CLE - 0.947 CD=0.01297
CM=-0.1812
S TURB S SEP CD
0.9926 0.02047 0.0116
0.7900 0.0000 0.0021
CLE 1.051 CD=0.01373
CM=-0.1816
S TURB S SEP CD
0.9947 0.0294 0.0127
0.7495 0.0000 0.0019
CLE 1.154 CD=0.01466
CM=-0.1818
S TURB S SEP CD
0.9919 0.0412 0.0157
CM=-0.1817
S TURB S SEP CD
0.9919 0.0412 0.01576
CM=-0.1813
S TURB S SEP CD
0.9919 0.0412 0.01576
CM=-0.1813
S TURB S SEP CD
0.9919 0.0412 0.01576
CM=-0.1813
S TURB S SEP CD
0.9919 0.0412 0.0156
0.6661 0.0000 0.0016
CLE 1.355 CD=0.01778
CM=-0.1805
S TURB S SEP CD
1.0131 0.0500 0.0177
0.6117 0.0000 0.0014
CLE 1.4476 CD=0.01918
CM=-0.1803

R= 1000000 MU=900 S TURB S SEP CD 0.7845 0.0064 0.0075 1.0018 0.0000 0.0041* CL= 0.523 CD=0.01162 CM=-0.1787

S TURB S SEP CD 0.7850 0.0064 0.0075 1.0018 0.0000 0.0041 CL= 0.524 CD=0.01162

7.35

7.51 S TURB S SEP CD
UPPER 0.9875 0.0509 0.0177*
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.503 CD=0.01824
CM=-0.1804

ALPHA(DEG.) R= 1100000 MU=300
-2.06 S TURB S SEP CD
UPPER 0.4109 0.0000 0.0044*
LOWER 1.0018 0.0000 0.0041*
TOTAL CL= 0.523 CD=0.00848
CM=-0.1800
-2.00 S TURB S SEP CD
UPPER 0.4114 0.0000 0.0044*
LOWER 1.0018 0.0000 0.0044*
LOWER 1.0018 0.0000 0.0044*
CM=-0.1801
-1.00 S TURB S SEP CD
UPPER 0.4193 0.0007 0.0047*
LOWER 0.4193 0.0007 0.0047*
LOWER 0.4193 0.0007 0.0021
TOTAL CL= 0.639 CD=0.00683
CM=-0.1816
0.00 S TURB S SEP CD
UPPER 0.4276 0.0035 0.056*
LOWER 0.4504 0.0000 0.0017
TOTAL CL= 0.746 CD=0.00672
CM=-0.1825
1.00 S TURB S SEP CD
UPPER 0.4372 0.0058 0.0053*
LOWER 0.3397 0.0000 0.0014
TOTAL CL= 0.854 CD=0.006672
CM=-0.1836
2.00 S TURB S SEP CD
UPPER 0.4372 0.0058 0.0053*
LOWER 0.2370 0.0000 0.0014
TOTAL CL= 0.854 CD=0.00667
CM=-0.1847
3.00 S TURB S SEP CD
UPPER 0.4487 0.0078 0.0055*
LOWER 0.1037 0.0000 0.0011
TOTAL CL= 0.961 CD=0.00664
CM=-0.1847
3.00 S TURB S SEP CD
UPPER 0.4626 0.0102 0.0059*
LOWER 0.1037 0.0000 0.0009
TOTAL CL= 1.068 CD=0.00673
CM=-0.1857
4.00 S TURB S SEP CD
UPPER 0.4523 0.0131 0.0055
LOWER 0.0000 0.0000
TOTAL CL= 1.068 CD=0.00673
CM=-0.1855
5.00 S TURB S SEP CD
UPPER 0.4555 1 0.0176 0.0076
LOWER 0.0000 0.0000
TOTAL CL= 1.168 CD=0.00613
CM=-0.1868
6.00 S TURB S SEP CD
UPPER 0.4586 0.0260 0.0099
LOWER 0.0000 0.0000 0.0006
TOTAL CL= 1.168 SEP CD
UPPER 0.4585 0.01317 0.0058
CM=-0.1868
6.00 S TURB S SEP CD
UPPER 0.4585 0.01375 CD=0.00818
CM=-0.1868
6.00 S TURB S SEP CD
UPPER 0.5551 0.0176 0.0076
LOWER 0.0000 0.0000 0.0006
TOTAL CL= 1.764 CD=0.006134
CM=-0.1859
7.00 S TURB S SEP CD
UPPER 0.5552 0.0176 0.0099
LOWER 0.0000 0.0000 0.0006
TOTAL CL= 1.764 CD=0.00614
CM=-0.1859
7.00 S TURB S SEP CD
UPPER 0.5859 0.01375 CD=0.00445
CM=-0.1869
6.00 S TURB S SEP CD
UPPER 0.6826 0.0260 0.0099
LOWER 0.0000 0.0000 0.0000

R= 1100000 MU=100
S TURB S SEP CD
1.0049 0.0076 0.0083
1.0018 0.0076 0.0083
1.0018 0.0000 0.0041*
CL= 0.517 CD=0.01238
CM=-0.1784
S TURB S SEP CD
1.0049 0.0078 0.0083
1.0018 0.0000 0.0041*
CL= 0.523 CD=0.01239
CM=-0.1784
S TURB S SEP CD
1.0049 0.0108 0.0090
0.9516 0.0000 0.0032
CL= 0.630 CD=0.01213
CM=-0.1792
S TURB S SEP CD
1.0049 0.0142 0.0097
0.9516 0.0000 0.0029
CL= 0.7786 CD=0.01258
CM=-0.1799
S TURB S SEP CD
1.0049 0.0142 0.0017
CM=0.1810
S TURB S SEP CD
1.0049 0.025 0.0113
CM=-0.1810
S TURB S SEP CD
1.0049 0.025 0.0125
S TURB S SEP CD
1.0049 0.025 0.0125
S TURB S SEP CD
1.0049 0.025 0.0125
CM=-0.1810
S TURB S SEP CD
1.0049 0.025 0.0122
0.9516 0.0000 0.0025
CL= 0.946 CD=0.01445
CM=-0.1814
S TURB S SEP CD
1.0049 0.0300 0.0122
0.9516 0.0000 0.0022
CL= 1.255 CD=0.01621
CM=-0.1816
S TURB S SEP CD
1.0049 0.0300 0.0122
0.9516 0.0000 0.0022
CL= 1.255 CD=0.01621
CM=-0.1817
S TURB S SEP CD
1.0049 0.0349 0.0142
0.9516 0.0000 0.0022
CL= 1.255 CD=0.01621
CM=-0.1817
S TURB S SEP CD
1.0049 0.0349 0.0142
0.9516 0.0000 0.0022
CL= 1.255 CD=0.01621
CM=-0.1817
S TURB S SEP CD
1.0049 0.0407 0.0156
0.9516 0.0000 0.0020
CL= 1.255 CD=0.01737
CM=-0.1818
S TURB S SEP CD
1.0049 0.0407 0.0156
0.9516 0.0000 0.0018
CL= 1.355 CD=0.01737
CM=-0.1818

R= 1100000 MU=900
S TURB S SEP CD
0.7948 0.0058 0.0074
1.0018 0.0050 0.0041*
CL= 0.518 CD=0.01150
CM=-0.1788
S TURB S SEP CD
0.7953 0.0059 0.0074
1.0018 0.0000 0.0041*
CL= 0.525 CD=0.01150
CM=-0.1788
S TURB S SEP CD
0.8277 0.0091 0.0081
0.9503 0.0000 0.0032
CL= 0.631 CD=0.01128
CM=-0.1796
S TURB S SEP CD
0.8560 0.0125 0.0088
0.9108 0.0000 0.0022
CL= 0.1737 CD=0.01166
CM=-0.1803
S TURB S SEP CD
0.8832 0.0161 0.0096
0.8734 0.0000 0.0025
CL= 0.843 CD=0.01218
CM=-0.1803
S TURB S SEP CD
0.8948 CD=0.01218
CM=-0.1804
S TURB S SEP CD
0.9948 CD=0.01281
CM=-0.1818
S TURB S SEP CD
0.9930 0.0000 0.0023
CL= 0.948 CD=0.01281
CM=-0.1818
S TURB S SEP CD
0.9930 0.0000 0.0023
CL= 0.948 CD=0.01281
CM=-0.1818
S TURB S SEP CD
0.9304 0.0240 0.0115
0.7980 0.0000 0.0021
CL= 1.052 CD=0.01356
CM=-0.1818
S TURB S SEP CD
0.9533 0.0287 0.0125
0.7586 0.0000 0.0012
CL= 1.155 CD=0.01447
CM=-0.1820
S TURB S SEP CD
0.9533 0.0287 0.0125
0.7586 0.0000 0.0018
CL= 1.155 CD=0.01555
CM=-0.1815
S TURB S SEP CD
0.9740 0.0339 0.0138
0.7183 0.0000 0.0018
CL= 1.155 CD=0.01555
CM=-0.1815
S TURB S SEP CD
0.9939 0.0403 0.0153
0.6780 0.0000 0.0016
CL= 1.155 CD=0.01695
CM=-0.1815
S TURB S SEP CD
1.0141 0.0488 0.0174
0.6263 0.0000 0.0018
CL= 1.457 CD=0.1850
CM=-0.1817
S TURB S SEP CD
1.0141 0.0488 0.0174
0.6263 0.0000 0.0018
CL= 1.457 CD=0.1857
CM=-0.1807

7.36

7.51 S TURB S SEP CD UPPER 0.9875 0.0497 0.0174* LOWER 0.0000 0.0000 0.0005 TOTAL CL= 1.505 CD=0.01788 CM=-0.1808 S TURB S SEP CD 1.0049 0.0493 0.0174* 0.9516 0.0000 0.0016 CL= 1.490 CD=0.01909 CM=-0.1807

"-WARNING 1990 ALPHA REL. CHO	KD LINE	
ALPHA (DEG.) R= 1200000 MU=300 -2.11 S TURB S SEP CD UPPER 0.4105 0.0000 0.0043* LOMER 1.0018 0.0000 0.0040* TOTAL CL= 0.518 CD=0.00830 CM=-0.1800 -2.00 S TURB S SEP CD UPPER 0.4114 0.0000 0.0043* LOMER 1.0018 0.0000 0.0044* TOTAL CL= 0.530 CD=0.00827 CM=-0.1801 -1.00 S TURB S SEP CD UPPER 0.4139 0.0000 0.0046* LOMER 1.0518 0.0000 0.0046* LOMER 0.5591 0.0000 0.0021	R= 1200000 MU=100 S TURB S SEP CD 1.0049 0.0068 0.0082 1.0018 0.0080 0.0082 1.0018 0.0080 0.0040* CL= 0.512 CD=0.01220 CM=-0.1784 S TURB S SEP CD 1.0049 0.0072 0.0082 1.0018 0.0000 0.0040* CL= 0.523 CD=0.01221 CM=-0.1785 S TURB S SEP CD 1.0049 0.0103 0.0089 0.9516 0.0000 0.0089	R= 1200000 MU=900 S TURB S SEP CD 0.8021 0.0051 0.0073 1.0018 0.0000 0.0040* CL= 0.513 CD=0.01137 CM=-0.1788 S TURB S SEP CD 0.8043 0.0054 0.0074 LD= 0.525 CD=0.01137 CM=-0.1789 S TURB S SEP CD 0.8353 0.0087 0.0080 0.8353 0.0087 0.0080
TOTAL CL= 0.640 CD=0.00669 CM=-0.1817 0.00 S TURB S SEP CD UPPER 0.4276 0.0025 0.0048* LOWER 0.4648 0.0000 0.0017	CL= 0.630 CD=0.01197 CM=-0.1793 S TURB S SEP CD 1.0049 0.0136 0.0095 0.9516 0.0000 0.0029	CL= 0.632 CD=0.01116 CM=-0.1797 S TURB S SEP CD 0.8624 0.0119 0.0088 0.9144 0.0000 0.0028
TOTAL CL= 0.747 CD=0.00657 CM=-0.1828 1.00 S TURB S SEP CD UPPER 0.4372 0.0047 0.0051* LOWER 0.3560 0.0000 0.0014	CL= 0.736 CD=0.01241 CM=-0.1800 S TURB S SEP CD 1.0049 0.0171 0.0103 0.9516 0.0000 0.0026	CL= 0.738 CD=0.01154 CM=-0.1804 S TURB S SEP CD 0.8887 0.0155 0.0095 0.8782 0.0000 0.0025
TOTAL CL= 0.855 CD=0.00650 CM=-0.1839 2.00 S TURB S SEP CD UPPER 0.4487 0.0068 0.0054* LOWER 0.2446 0.0000 0.0011 TOTAL CL= 0.962 CD=0.00648	CL= 0.842 CD=0.01294 CM=-0.1807 S TURB S SEP CD 1.0049 0.0208 0.0111 0.9516 0.0000 0.0024 CL= 0.947 CD=0.01355	CL= 0.843 CD=0.01205 CM=-0.1810 S TURB S SEP CD 0.9121 0.0193 0.0104 0.8414 0.0000 0.0023 CL= 0.948 CD=0.01267
CM=-0.1850 3.00 S TURE S SEP CD UPPER 0.4679 0.0092 0.0058 LOWER 0.1261 0.0000 0.0009 TOTAL CL= 1.069 CD=0.00662	CM=-0.1812 S TURB S SEP CD 1.0049 0.0248 0.0120 0.9516 0.0000 0.0023 CL= 1.051 CD=0.01425	CM=-0.1816 S TURB S SEP CD 0.9341 0.0234 0.0113 0.8049 0.0000 0.0021 CL= 1.052 CD=0.01341
CM=-0.1860 4.00 S TURB S SEP CD UPPER 0.5031 0.0124 0.0064 LOWER 0.0000 0.0000 0.0006 TOTAL CL= 1.175 CD=0.00703 CM=-0.1867	CM=-0.1816 S TURB S SEP CD 1.0049 0.0292 0.0130 0.9516 0.0000 0.0021 CL= 1.154 CD=0.01506 CM=-0.1819	CM=-0.1820 S TURB S SEP CD 0.9564 0.0280 0.0124 0.7665 0.0000 0.0019 CL= 1.155 CD=0.01430 CM=-0.1822
5.00 S TURB S SEP CD UPPER 0.5681 0.0172 0.0076 LOWER 0.0000 0.0000 0.0006 TOTAL CL= 1.278 CD=0.00817 CM=-0.1869	S TURB S SEP CD 1.0049 0.0341 0.0140 0.9516 0.0000 0.0019 CL= 1.256 CD=0.01598 CM=-0.1819	S TURB S SEP CD 0.9765 0.0332 0.0136 0.7276 0.0000 0.0017 CL= 1.257 CD=0.01536 CM=-0.1822
6.00 S TURB S SEP CD UPPER 0.7020 0.0260 0.0100 LOWER 0.0000 0.0000 0.0005 TOTAL CL= 1.375 CD=0.01052 CM=-0.1859	S TURB S SEP CD 1.0049 0.0399 0.0153 0.9516 0.0000 0.0018 CL= 1.356 CD=0.01711 CM=-0.1817	S TURB S SEP CD 0.9958 0.0395 0.0151 0.6886 0.0000 0.0016 CL= 1.357 CD=0.01674 CM=-0.1818
7.00 S TURB S SEP CD UPPER 0.8329 0.0361 0.0128 LOWER 0.0000 0.0000 0.0005 TOTAL CL= 1.469 CD=0.01334 CM=-0.1842	S TURB S SEP CD 1.0049 0.0457 0.0166 0.9516 0.0000 0.0017 CL= 1.456 CD=0.01828 CM=-0.1813	S TURB S SEP CD 1.0121 0.0462 0.0168 0.6477 0.0000 0.0015 CL= 1.455 CD=0.01826 CM=-0.1812
7.24		S TURE S SEP CD 1.0154 0.0480 0.0172 0.6372 0.0000 0.0014 CL= 1.479 CD=0.01867 CM=-0.1809
7.40	S TURB S SEP CD 1.0049 0.0485 0.0172* 0.9516 0.0000 0.0016 CL= 1.495 CD=0.01885 CM=-0.1810	
7.52 S TURB S SEP CD		

7.52 S TURB S SEP CD UPPER 0.9897 0.0488 0.0172* LOWER 0.0000 0.0000 0.0005 TOTAL CL= 1.508 CD=0.01767 CM=-0.1811

ALPHA(DEG.) R= 1300000 MU=300
-2.16 S TURB S SEP CD
UPPER 0.4010 0.0000 0.0041*
LOWER 1.0018 0.0000 0.0040*
TOTAL CL= 0.512 CD=0.00815
CM=-0.1799
-2.00 S TURB S SEP CD
UPPER 0.4114 0.0000 0.0042*
LOWER 1.0018 0.0000 0.0039*
TOTAL CL= 0.530 CD=0.00809
CM=-0.1801
-1.00 S TURB S SEP CD
UPPER 0.413 0.0000 0.0021*
TOTAL CL= 0.640 CD=0.00809
CM=-0.1801
-1.00 S TURB S SEP CD
UPPER 0.413 0.0000 0.0021*
TOTAL CL= 0.640 CD=0.00655
CM=-0.1817
0.00 S TURB S SEP CD
UPPER 0.4276 0.0015 0.0047*
LOWER 0.4276 0.0015 0.0047*
LOWER 0.4276 0.0015 0.0047*
LOWER 0.4276 0.0015 0.0017
TOTAL CL= 0.748 CD=0.00644
CM=-0.1830
1.00 S TURB S SEP CD
UPPER 0.4372 0.0038 0.0049*
LOWER 0.3706 0.0000 0.0011
TOTAL CL= 0.856 CD=0.00635
CM=-0.1841
2.00 S TURB S SEP CD
UPPER 0.4487 0.0060 0.0052*
LOWER 0.2667 0.0000 0.0011
TOTAL CL= 0.963 CD=0.00635
CM=-0.1852
3.00 S TURB S SEP CD
UPPER 0.4530 0.0086 0.0057
LOWER 0.4540 0.0000 0.0007
TOTAL CL= 1.070 CD=0.00656
CM=-0.1869
4.00 S TURB S SEP CD
UPPER 0.5107 0.0118 0.0064
LOWER 0.0000 0.0000 0.0006
TOTAL CL= 1.175 CD=0.00696
CM=-0.1869
5.00 S TURB S SEP CD
UPPER 0.5812 0.1770 0.0076
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.175 CD=0.00696
CM=-0.1870
CM=-0.1857
5.00 S TURB S SEP CD
UPPER 0.5812 0.1770 0.0076
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.175 CD=0.00817
CM=-0.1857
5.00 S TURB S SEP CD
UPPER 0.5812 0.1770 0.0076
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.175 CD=0.00817
CM=-0.1857
5.00 S TURB S SEP CD
UPPER 0.5812 0.1770 0.0076
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.175 CD=0.00817
CM=-0.1859
7.00 S TURB S SEP CD
UPPER 0.5812 0.0170 0.0076
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.175 CD=0.00857
CM=-0.1859
7.00 S TURB S SEP CD
UPPER 0.5812 0.0170 0.0076
LOWER 0.8080 0.00357 0.0128
LOWER 0.8080 0.00357 0.012

RE 1300000 MU=100
S TURB S SEP CD
1.0048 0.0061 0.0080
L018 0.0061 0.0080
CL= 0.507 CD=0.01203
CM=-0.1785
S TURB S SEP CD
1.0049 0.0066 0.0081
L018 0.0000 0.0039*
CL= 0.524 CD=0.01204
CM=-0.1786
S TURB S SEP CD
1.0049 0.0097 0.0087
0.9516 0.0000 0.0031
CL= 0.631 CD=0.01182
CM=-0.1794
S TURB S SEP CD
1.0049 0.0130 0.0094
0.9516 0.0000 0.0028
CL= 0.737 CD=0.01226
CM=-0.1802
S TURB S SEP CD
1.0049 0.0130 0.0094
0.9516 0.0000 0.0028
CL= 0.737 CD=0.01226
CM=-0.1808
S TURB S SEP CD
1.0049 0.0155 0.1002
0.9516 0.0000 0.0028
CL= 0.947 CD=0.01277
CM=-0.1808
S TURB S SEP CD
1.0049 0.0222 0.0110
0.9516 0.0000 0.0026
CL= 0.947 CD=0.01233
CM=-0.1813
S TURB S SEP CD
1.0049 0.0222 0.0118
0.9516 0.0000 0.0024
CL= 0.947 CD=0.01333
CM=-0.1813
S TURB S SEP CD
1.0049 0.0242 0.0118
0.9516 0.0000 0.0022
CL= 1.052 CD=0.01486
CM=-0.1821
S TURB S SEP CD
1.0049 0.0233 0.0138
0.9516 0.0000 0.0021
CL= 1.155 CD=0.01486
CM=-0.1821
S TURB S SEP CD
1.0049 0.0333 0.0138
0.9516 0.0000 0.0016
CL= 1.358 CD=0.01688
CM=-0.1819
S TURB S SEP CD
1.0049 0.0331 0.0151
CL= 1.155 CD=0.01688
CM=-0.1819
S TURB S SEP CD
1.0049 0.0448 0.0164
0.9516 0.0000 0.0016
CL= 1.457 CD=0.01803
CM=-0.1816

R= 1300000 MU=900
S TORB S SEP CD
0.8083 0.0044 0.0072
1.0018 0.0000 0.0040*
CL= 0.508 CD=0.01124
CM=-0.1789
S TURE S SEP CD
0.8123 0.0050 0.0073
1.0018 0.0000 0.0039*
CL= 0.525 CD=0.01124
CM=-0.1790
S TURE S SEP CD
0.8418 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.9548 0.0082 0.0080
0.0080 0.0085
S TURB S SEP CD
0.8935 0.0150 0.0094
0.8824 0.0000 0.0025
CL= 0.844 CD=0.01254
CM=-0.1817
S TURE S SEP CD
0.9159 0.0188 0.0103
0.8466 0.0000 0.0023
CL= 0.949 CD=0.01254
CM=-0.1824
S TURE S SEP CD
0.9374 0.0228 0.0112
0.8100 0.0000 0.0021
CL= 1.053 CD=0.01326
CM=-0.1824
S TURE S SEP CD
0.9978 0.0000 0.0019
CL= 1.258 CD=0.01519
CM=-0.1824
S TURE S SEP CD
0.9978 0.0000 0.0017
CL= 1.258 CD=0.01519
CM=-0.1824
S TURE S SEP CD
0.9979 0.0000 0.0016
CL= 1.358 CD=0.0150
CM=-0.1820
S TURE S SEP CD
0.9979 0.0000 0.0016
CL= 1.358 CD=0.01500
CM=0.1820
S TURE S SEP CD
0.0974 0.0387 0.0150
0.6979 0.0000 0.0016
CL= 1.481 CD=0.01846
CM=-0.1814
S TURE S SEP CD

S TURB S SEP CD 1.0049 0.0478 0.0170* 0.9516 0.0000 0.0016 CL= 1.499 CD=0.01864 CM=-0.1813

7.54 S TURB S SEP CD UPPER 0.9938 0.0481 0.0170* LOWER 0.0000 0.0000 0.0005 TOTAL CL= 1.511 CD=0.01749 CM=-0.1813

7.43

R= 1400000 MU=900
S TURB S SEP CD
0.8136 0.0038 0.0072
1.0019 0.0000 0.0040*
CL= 0.503 CD=0.01112
CM=-0.1790
S TURB S SEP CD
0.8193 0.0045 0.0073
1.0018 0.0000 0.0038*
CL= 0.526 CD=0.01111
CM=-0.1791
S TURB S SEP CD
0.8476 0.0078 0.0079
0.9567 0.0000 0.0031
CL= 0.633 CD=0.01097
CM=-0.1799
S TURB S SEP CD
0.8476 0.0078 0.0079
0.9567 0.0000 0.0031
CL= 0.633 CD=0.01097
CM=-0.1799
S TURB S SEP CD
0.8730 0.0110 0.0086
0.9206 0.0000 0.0027
CL= 0.739 CD=0.0133
CM=-0.1807
S TURB S SEP CD
0.8977 0.0146 0.0094
0.8862 0.0000 0.0025
CL= 0.9444 CD=0.0182
CM=-0.1813
S TURB S SEP CD
0.9194 0.0183 0.0102
0.8512 0.0000 0.0025
CL= 0.949 CD=0.01242
CM=-0.1819
S TURB S SEP CD
0.9494 0.0183 0.0102
0.8512 0.0000 0.0022
CL= 0.949 CD=0.01242
CM=-0.1819
S TURB S SEP CD
0.9404 0.0223 0.0111
0.8166 0.0000 0.0022
CL= 1.054 CD=0.01314
CM=-0.1825
S TURB S SEP CD
0.9615 0.0268 0.0121
0.7804 0.0000 0.0012
CL= 1.157 CD=0.01401
CM=-0.1825
S TURB S SEP CD
0.9866 0.0319 0.013
0.7434 0.0000 0.0019
CL= 1.259 CD=0.01504
CM=-0.1826
S TURB S SEP CD
0.9988 0.0380 0.0148
0.7061 0.0000 0.0016
CL= 1.359 CD=0.01636
CM=-0.1825
S TURB S SEP CD
0.9988 0.0380 0.0148
0.7061 0.0000 0.0012
CL= 1.359 CD=0.01636
CM=-0.1822
S TURB S SEP CD ALPHA(DEG.) R= 1400000 MII=300 R= 1400000 MU=100 LPHA (DEG.) R= 1400000 MU=300 -2.21 S TURB S SEP CD UPPER 0.4096 0.0000 0.0040* LOWER 1.0019 0.0000 0.0040* TOTAL CLE 0.507 CD=0.00801 CM=-0.1798 -2.00 S TURB S SEP CD UPPER 0.4114 0.0000 0.0041* LOWER 1.0018 0.0000 0.0038* TOTAL CLE 0.530 CD=0.00790 CM=-0.1801 -1.00 S TURB S SEP CD S TURB S SEP CD 1.0049 0.0055 0.0079 1.0019 0.0000 0.0040* 1.0019 0.0000 0.0040*
CL= 0.502 CD=0.01187
CM=-0.1786
S TURB S SEP CD
1.0049 0.0061 0.0080
1.0018 0.0000 0.0038*
CL= 0.524 CD=0.01186
CM=-0.1788
S TURB S SEP CD
1.0049 0.0092 0.0086
0.9516 0.0000 0.0030
CL= 0.631 CD=0.01168
CM=-0.1796
S TURB S SEP CD
1.0049 0.0125 0.0093
0.9516 0.0000 0.0030
CL= 0.637 CD=0.01168
CM=-0.1796
S TURB S SEP CD
1.0049 0.0125 0.0093
0.9516 0.0000 0.0028
CL= 0.737 CD=0.01211
CM=-0.1803 CL= 0.737 CD=0.01211
CM=-0.1803
S TURE S SEP CD
1.0049 0.0160 0.0100
0.9516 0.0000 0.0026
CL= 0.843 CD=0.01263
CM=-0.1809
S TURE S SEP CD
1.0049 0.0196 0.0108
0.9516 0.0000 0.0024
CL= 0.948 CD=0.01322
CM=-0.1815
S TURE S SEP CD
1.0049 0.0226 0.017
0.9516 0.0000 0.0022
CL= 1.052 CD=0.01391
CM=-0.1819
S TURE S SEP CD
1.0049 0.0227 0.0126
0.9516 0.0000 0.0022
CL= 1.052 CD=0.01391
CM=-0.1819
S TURE S SEP CD
1.0049 0.0279 0.0126
0.9516 0.0000 0.0022
CL= 1.156 CD=0.01469 TOTAL CLE - 0.964 CD-0.00627 CM=-0.1854 3.00 S TURB S SEP CD UPPER 0.4782 0.0080 0.0056 LOWER 0.1630 0.0000 0.0009 TOTAL CLE - 1.071 CD-0.00652 CM=-0.1863 4 00 0.9516 0.0000 0.0020 CL= 1.156 CD=0.01469 CM=-0.1822 S TURB S SEP CD 1.0049 0.0327 0.0137 0.9516 0.0000 0.0019 CL= 1.258 CD=0.01557 CM=-0.1823 CM=-0.1871 6.00 S TURB S SEP CD UPPER 0.7329 0.0258 0.0101 LOWER 0.0000 0.0000 0.0005 TOTAL CL= 1.375 CD=0.01061 CM=-0.1859 LM=-0.1823 S TURB S SEP CD 1.0049 0.0382 0.0149 0.9516 0.0000 0.0018 CL= 1.359 CD=0.01666 CM=-0.1821 6.00 CM=-0.1859
7.00 S TURB S SEP CD
UPPER 0.8479 0.0352 0.0127
LOWER 0.0000 0.0000 0.0005
TOTAL CL= 1.471 CD=0.01318
CM=-0.1845 CM=-0.1821 S TURB S SEP CD 1.0049 0.0440 0.0162 0.9516 0.0000 0.0016 CL= 1.458 CD=0.01780 CM=-0.1818 CL= 1.458 CD=0.01785 CM=-0.1817 S TURB S SEP CD 1.0173 0.0463 0.0168 0.6572 0.0000 0.0014 CL= 1.481 CD=0.01824 CM=-0.1815 S TURB S SEP CD 1.0049 0.0469 0.0168* 0.9516 0.0000 0.0016 7.44 CL= 1.502 CD=0.01841 CM=-0.1815

7.54 S TURB S SEP CD UPPER 0.9938 0.0471 0.0168* LOWER 0.0000 0.0000 0.0004 TOTAL CL= 1.512 CD=0.01723 CM=-0.1816

71

ALPHA (DEG.) R= 1500000 MU=300
-1.96 S TURE S SEP CD
UPPER 0.4117 0.0000 0.0036*
TOTAL CL= 0.534 CD=0.00759
CM=-0.1802
-1.00 S TURE S SEP CD
UPPER 0.4193 0.0000 0.0021
TOTAL CL= 0.640 CD=0.00633
CM=-0.1817
0.00 S TURE S SEP CD
UPPER 0.4276 0.0000 0.0021
TOTAL CL= 0.640 CD=0.00633
CM=-0.1817
TOTAL CL= 0.75 CD=0.00621
CM=-0.1834
1.00 S TURE S SEP CD
UPPER 0.4372 0.0022 0.0047*
LOWER 0.3959 0.0000 0.0014
TOTAL CL= 0.858 CD=0.00612
CM=-0.1845
2.00 S TURE S SEP CD
UPPER 0.4372 0.0022 0.0047*
LOWER 0.3959 0.0000 0.0014
TOTAL CL= 0.985 CD=0.00621
CM=-0.1845
2.00 S TURE S SEP CD
UPPER 0.4559 0.0047 0.0051
LOWER 0.1791 0.0000 0.0011
TOTAL CL= 0.985 CD=0.00622
CM=-0.1865
4.00 S TURE S SEP CD
UPPER 0.4832 0.0075 0.0056
LOWER 0.1791 0.0000 0.0009
TOTAL CL= 1.176 CD=0.00648
CM=-0.1865
4.00 S TURE S SEP CD
UPPER 0.6073 0.0167 0.0077
TOTAL CL= 1.176 CD=0.00648
CM=-0.1817
5.00 S TURE S SEP CD
UPPER 0.6073 0.0167 0.0077
TOTAL CL= 1.278 CD=0.00622
CM=-0.1866
4.00 S TURE S SEP CD
UPPER 0.5025 0.0110 0.0063
TOTAL CL= 1.278 CD=0.00622
CM=-0.1866
4.00 S TURE S SEP CD
UPPER 0.5025 0.0110 0.0063
TOTAL CL= 1.278 CD=0.00648
CM=-0.1866
4.00 S TURE S SEP CD
UPPER 0.5025 0.0110 0.0063
TOTAL CL= 1.278 CD=0.00647
CM=-0.1821
5.00 S TURE S SEP CD
UPPER 0.6073 0.0167 0.0077
CDAL CL= 1.375 CD=0.10632
CM=-0.1824
5.008 5.0080 0.0080
0.0000 0.0000 0.0005
TOTAL CL= 1.375 CD=0.1063
CM=-0.1824
5.008 5.0080 0.0000
0.0000 0.0000
0.0020
CM=-0.1847
5.00 S TURE S SEP CD
UPPER 0.5025 0.0110 0.0063
TOTAL CL= 1.375 CD=0.10632
CM=-0.1824
5.008 5.0080 0.0080
0.0000 0.0000 0.0005
TOTAL CL= 1.471 CD=0.01308
CM=-0.1824
5.008 5.0080 0.0083
0.0086
0.0086 0.0086
0.0086 0.0086
0.0086 0.00867
0.0092 0.0017
0.9516 0.0000 0.0002
CM=-0.1855
0.0000 0.00010
0.0016
0.9516 0.0000 0.0002
0.0016
0.9516 0.0000 0.0016
0.9516 0.0000 0.0016
0.9516 0.0000 0.0016
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000 0.0002
0.9516 0.0000

S TURB S SEP CD 1.0049 0.0466 0.0167* 0.9516 0.0000 0.0016 CL= 1.510 CD=0.01830 CM=-0.1817 R= 1500000 MU=900
S TURB S SEP CD
0.8273 0.0042 0.0073
1.0018 0.0000 0.0036
CL= 0.531 CD=0.01083
CM=-0.1792
S TURB S SEP CD
0.8528 0.0074 0.0079
0.9584 0.0000 0.0030
CL= 0.633 CD=0.01088
CM=-0.1800
S TURB S SEP CD
0.8775 0.0106 0.0085
0.9231 0.0000 0.0027
CL= 0.739 CD=0.01124
CM=-0.1808
S TURB S SEP CD
0.9015 0.0141 0.0093
0.8896 0.0000 0.0025
CL= 0.845 CD=0.01172
CM=-0.1814
S TURB S SEP CD
0.9227 0.0178 0.0101
0.8553 0.0000 0.0022
CL= 0.950 CD=0.01231
CM=-0.1820
S TURB S SEP CD
0.9431 0.0218 0.0110
0.8218 0.0000 0.0022
CL= 1.054 CD=0.01231
CM=-0.1824
S TURB S SEP CD
0.9638 0.0262 0.0120
0.7863 0.0000 0.0012
CL= 1.054 CD=0.01338
CM=-0.1827
S TURB S SEP CD
0.9824 0.0313 0.013
CM=-0.1827
S TURB S SEP CD
0.9824 0.0313 0.013
CM=-0.1827
S TURB S SEP CD
0.9824 0.0313 0.013
CM=-0.1827
S TURB S SEP CD
0.9824 0.0313 0.013
CM=-0.1827
S TURB S SEP CD
0.9824 0.0313 0.013
CM=-0.1827
S TURB S SEP CD
0.9824 0.0313 0.013
CM=-0.1824
S TURB S SEP CD
1.0150 0.0000 0.0017
CL= 1.260 CD=0.01620
CM=-0.1824
S TURB S SEP CD
1.0150 0.0000 0.0016
CL= 1.360 CD=0.01620
CM=-0.1824
S TURB S SEP CD
1.0150 0.0438 0.0162
CM=-0.1824
S TURB S SEP CD
1.0150 0.0438 0.0162
CM=-0.1829
S TURB S SEP CD
1.0150 0.0438 0.0162
CM=-0.1824
S TURB S SEP CD
1.0150 0.0438 0.0162
CM=-0.1824
S TURB S SEP CD
1.0150 0.0438 0.0162
CM=-0.1824

7.51

REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, to Department of Defense, Executive Services and Communications Directorate (0704-0188). Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number

	ently valid OMB control number. EASE DO NOT RETURN YOUR FORM	и то тн	IE ABOVE ORGANI	IZATION.	-					
	REPORT DATE (DD-MM-YYYY) 2. REPORT TYPE					3. DATES COVERED (From - To)				
	January 2005	Sı	ubcontract repor	t	_	May 1998 – January 1999				
4.	TITLE AND SUBTITLE The S904 and S905 Airfoils					NTRACT NUMBER -AC36-99-GO10337				
					5b. GRA	NT NUMBER				
					5c. PROGRAM ELEMENT NUMBER					
6.	AUTHOR(S) D.M. Somers				5d. PROJECT NUMBER NREL/SR-500-36338					
						K NUMBER R4.3110				
		5f. WOF	WORK UNIT NUMBER							
7.	PERFORMING ORGANIZATION NA Airfoils, Inc. 601 Cricklewood Drive State College, PA 16083	ME(S) A	ND ADDRESS(ES)			8. PERFORMING ORGANIZATION REPORT NUMBER AAM-8-18218-01				
9.	SPONSORING/MONITORING AGEN National Renewable Energy L 1617 Cole Blvd.			SS(ES)		10. SPONSOR/MONITOR'S ACRONYM(S) NREL				
	Golden, CO 80401-3393			11. SPONSORING/MONITORING AGENCY REPORT NUMBER NREL/SR-500-36338						
12.	12. DISTRIBUTION AVAILABILITY STATEMENT National Technical Information Service U.S. Department of Commerce 5285 Port Royal Road Springfield, VA 22161									
13.	SUPPLEMENTARY NOTES NREL Technical Monitor: J. Ta	angler								
14.	4. ABSTRACT (Maximum 200 Words) A family of natural-laminar-flow airfoils, the S904 and S905, for cooling-tower fans has been designed and analyzed theoretically. The two primary objectives of high maximum lift, relatively insensitive to roughness, and low profile drag have been achieved. The constraint on the lift a zero angle of attack has not been satisfied. The constraints on the pitching moment and the airfoil thicknesses have essentially been satisfied. The airfoils should exhibit docile stalls.									
15.	SUBJECT TERMS									
	airfoils; wind turbine; airfoil de	sign; P	ennsylvania Sta	te University; wi	ind energ	у				
	SECURITY CLASSIFICATION OF:		17. LIMITATION OF ABSTRACT	18. NUMBER 1 OF PAGES	19a. NAME C	OF RESPONSIBLE PERSON				
	BEPORT b. ABSTRACT c. THIS F Inclassified Unclassified Unclass		UL	L	19b. TELEPC	ONE NUMBER (Include area code)				

Standard Form 298 (Rev. 8/98) Prescribed by ANSI Std. Z39.18