

The S825 and S826 Airfoils

Period of Performance: 1994 – 1995

D.M. Somers
Airfoils, Inc.
State College, Pennsylvania



NREL

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Contract No. DE-AC36-99-GO10337

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NREL Technical Monitor: Jim Tangler

Prepared under Subcontract No. AAF-4-14289-01



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Table of Contents

Abstract.....	1
Introduction.....	1
Symbols.....	2
Airfoil Design.....	2
Objectives and Constraints.....	2
Philosophy.....	3
Execution.....	6
Theoretical Procedure.....	6
Discussion of Results.....	6
S825 Airfoil.....	6
S826 Airfoil.....	8
Concluding Remarks.....	9
References.....	10
Appendix.....	38

List of Tables

Table I. Airfoil Design Specifications.....	12
Table II. S825 Airfoil Coordinates.....	13
Table III. S826 Airfoil Coordinates.....	14

List of Figures

Figure 1: Airfoil shapes.....	15
Figure 2: Inviscid pressure distributions for S825 airfoil.....	16 – 21
Figure 3: Section characteristics of S825 airfoil with transition free, transition fixed, and rough.....	22 – 26
Figure 4: Inviscid pressure distributions for S826 airfoil.....	27 – 32
Figure 5: Section characteristics of S826 airfoil and transition free, transition fixed, and rough.....	33 – 37

ABSTRACT

A family of airfoils, the S825 and S826, for 20- to 40-meter, variable-speed and variable-pitch (toward feather), horizontal-axis wind turbines has been designed and analyzed theoretically. The two primary objectives of high maximum lift, insensitive to roughness, and low profile drag have been achieved. The constraints on the pitching moments and the airfoil thicknesses have been satisfied. The airfoils should exhibit docile stalls.

INTRODUCTION

The majority of the airfoils in use on horizontal-axis wind turbines today were originally developed for aircraft. The design requirements for these airfoils, primarily National Advisory Committee for Aeronautics (NACA) and National Aeronautics and Space Administration (NASA) airfoils (refs. 1–6), are significantly different from those for wind-turbine airfoils (ref. 7). Accordingly, several families of airfoils have been designed specifically for horizontal-axis wind-turbine applications, as shown in the following table.

Diameter	Type	Thickness Category	Airfoil			Reference
			Primary	Tip	Root	
2–10 m	Variable speed Variable pitch	Thick		S822	S823	13
10–20 m	Variable speed Variable pitch	Thin	S801	S802 S803	S804	8
	Stall regulated	Thin	S805 S805A	S806 S806A	S807 S808	8
	Stall regulated	Thick	S819	S820	S821	12
20–30 m	Stall regulated	Thick	S809	S810	S811	9
	Stall regulated	Thick	S812	S813	S814 S815	9 and 10
30–50 m	Stall regulated	Thick	S816	S817	S818	11

An overview of all these airfoil families is given in reference 14.

The family of airfoils designed under the present study is intended for 20- to 40-meter, variable-speed and variable-pitch (toward feather), horizontal-axis wind turbines. The specific tasks performed under this study are described in National Renewable Energy Laboratory (NREL) Subcontract Number AAF-4-14289-01. The specifications for the airfoils are outlined in the Statement of Work. These specifications were later refined during discussions with James L. Tangler of NREL.

Because of the limitations of the theoretical methods (refs. 15 and 16) employed in this study, the results presented are in no way guaranteed to be accurate—either in an absolute or in a relative sense. This statement applies to the entire study.

SYMBOLS

C_p	pressure coefficient
c	airfoil chord, m
c_d	section profile-drag coefficient
c_l	section lift coefficient
c_m	section pitching-moment coefficient about quarter-chord point
L.	lower surface
R	Reynolds number based on free-stream conditions and airfoil chord
S.	boundary-layer separation location, $1 - s_{sep}/c$
s_{sep}	arc length along which boundary layer is separated, m
s_{turb}	arc length along which boundary layer is turbulent including s_{sep} , m
T.	boundary-layer transition location, $1 - s_{turb}/c$
U.	upper surface
x	airfoil abscissa, m
y	airfoil ordinate, m
α	angle of attack relative to x-axis, deg

AIRFOIL DESIGN

OBJECTIVES AND CONSTRAINTS

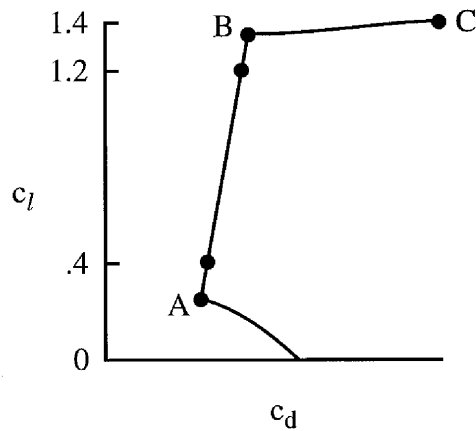
The design specifications for the family of airfoils are contained in table I. The family consists of two airfoils, primary and tip, corresponding to the 0.75 and 0.95 blade radial stations, respectively. (It is recommended that the S814 and S815 airfoils (ref. 10) be used for the root region of a wind-turbine blade incorporating this family.)

Two primary objectives are evident from the specifications. The first objective is to achieve a maximum lift coefficient of at least 1.40 for the primary and tip airfoils for the corresponding Reynolds numbers of 2.0×10^6 and 1.5×10^6 , respectively. A requirement related to this objective is that the maximum lift coefficient not decrease with transition fixed near the leading edge on both surfaces. In addition, the airfoils should exhibit docile stall characteristics. The second objective is to obtain low profile-drag coefficients over the range of lift coefficients from 0.40 to 1.20 for both airfoils.

Two major constraints were placed on the designs of these airfoils. First, the zero-lift pitching-moment coefficient must be no more negative than -0.15 for both airfoils. Second, the airfoil thickness must equal 17-percent chord for the primary airfoil and 14-percent chord for the tip airfoil.

PHILOSOPHY

Given the above objectives and constraints, certain characteristics of the designs are apparent. The following sketch illustrates a drag polar that meets the goals for these designs.



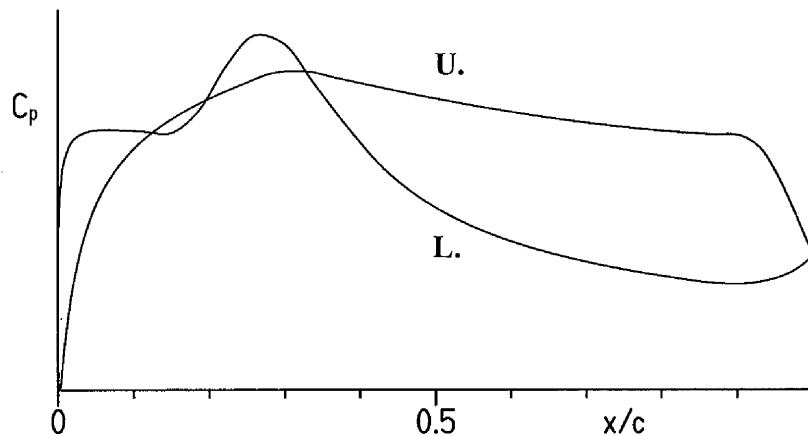
Sketch 1

The desired airfoil shapes can be traced to the pressure distributions that occur at the various points in sketch 1. Point A is the lower limit of the low-drag, lift-coefficient range. The lift coefficient at point A is 0.15 lower than the objective specified in table I. The difference is intended as a margin against such contingencies as manufacturing tolerances, operational deviations, three-dimensional effects, and inaccuracies in the theoretical method. A similar margin is also desirable at the upper limit of the low-drag range, point B, although this margin is constrained by the proximity of the upper limit to the maximum lift coefficient. The drag at point B is not as low as at point A, unlike the polars of many laminar-flow airfoils where the drag within the laminar bucket is nearly constant. This characteristic is related to the elimina-

tion of significant (drag-producing) laminar separation bubbles on the upper surface. (See ref. 17.) It is acceptable because the ratio of the profile drag to the total drag of the wind-turbine blade decreases with increasing lift coefficient. The drag increases very rapidly outside the low-drag range because the boundary-layer transition point moves quickly toward the leading edge with increasing (or decreasing) lift coefficient. This feature results in a leading edge that produces a suction peak at higher lift coefficients, which ensures that transition on the upper surface will occur very near the leading edge. Thus, the maximum lift coefficient, point C, occurs with turbulent flow along the entire upper surface and, therefore, should be relatively insensitive to roughness at the leading edge.

Because the large thickness of the primary airfoil allows a wider low-drag range than specified, the lower limit of the low-drag range should be below point A.

From the preceding discussion, the pressure distributions along the polar can be deduced. The pressure distribution at point A for the primary airfoil should look something like sketch 2. (The pressure distribution for the tip airfoil should be qualitatively similar.)



Sketch 2

To achieve low drag, a favorable pressure gradient is desirable along the upper surface to about 30-percent chord. Aft of this point, a short region having a shallow, adverse pressure gradient (“transition ramp”) promotes the efficient transition from laminar to turbulent flow (ref. 18). The transition ramp is followed by a concave pressure recovery. The specific pressure recovery employed represents a compromise between maximum lift, drag, and stall characteristics. The steep, adverse pressure gradient aft of about 90-percent chord is a “separation ramp,” originally proposed by F. X. Wortmann,¹ which confines turbulent separation to a small region near the trailing edge. By constraining the movement of the separation point at

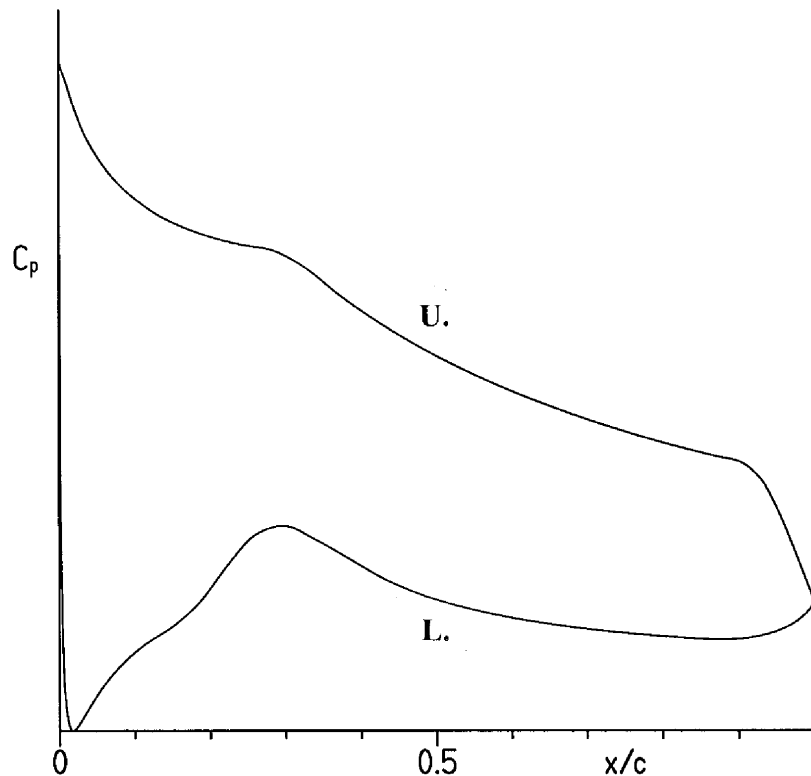
¹Director, Institute for Aerodynamics and Gas Dynamics, University of Stuttgart, Germany.

high angles of attack, high lift coefficients can be achieved with little drag penalty. This feature has the added benefit of promoting docile stall characteristics. (See ref. 19.)

A generally favorable pressure gradient is desirable along the lower surface to about 30-percent chord to achieve low drag. The specific pressure gradients employed along the forward portion of the lower surface increase the amount of camber in the leading-edge region while maintaining low drag at the lower lift coefficients. The forward camber serves to balance, with respect to the pitching-moment constraint, the aft camber, both of which contribute to the achievement of a high maximum lift coefficient. This region is followed by a curved transition ramp (ref. 17) that is longer than the one on the upper surface. The ramp is followed by a concave pressure recovery that produces lower drag and has less tendency to separate than the corresponding linear or convex pressure recovery (ref. 18). The pressure recovery must begin relatively far forward to alleviate separation at lower lift coefficients, especially with transition fixed near the leading edge.

The amounts of pressure recovery on the upper and lower surfaces are determined by the airfoil-thickness and pitching-moment constraints.

At point B, the pressure distribution should look like sketch 3.



Sketch 3

No suction spike exists at the leading edge. Transition is essentially imminent over the entire forward portion of the upper surface. This feature allows a wider low-drag range to be achieved and higher lift coefficients to be reached without significant separation. It also causes the transition point to move very quickly toward the leading edge with increasing lift coefficient, which leads to the roughness insensitivity of the maximum lift coefficient.

EXECUTION

Given the pressure distributions previously discussed, the design of the airfoils is reduced to the inverse problem of transforming the pressure distributions into airfoil shapes. The Eppler Airfoil Design and Analysis Code (refs. 15 and 16) was used because of its unique capability for multipoint design and because of confidence gained during the design, analysis, and experimental verification of several other airfoils. (See refs. 20–23.)

The primary airfoil is designated the S825. The tip airfoil, the S826, was derived from the S825 airfoil to increase the aerodynamic and geometric compatibilities of the two airfoils. The airfoil shapes are shown in figure 1 and the coordinates are contained in tables II and III. The S825 airfoil thickness is 17-percent chord and the S826, 14-percent chord.

THEORETICAL PROCEDURE

The section characteristics are predicted for Reynolds numbers of 1.0×10^6 , 1.5×10^6 , 2.0×10^6 , 2.5×10^6 , and 3.0×10^6 . The computations were performed with transition free using transition mode 3.0, with transition fixed at 2-percent chord on the upper surface and 5-percent chord on the lower surface using transition mode 1.3, and “rough” using transition mode 9.0, which simulates distributed roughness due to, for example, leading-edge contamination by insects or rain. (See ref. 16.) Because the free-stream Mach number for all relevant operating conditions remains below 0.3, all results are incompressible.

DISCUSSION OF RESULTS

S825 AIRFOIL

Pressure Distributions

The inviscid pressure distributions for the S825 airfoil at various angles of attack are shown in figure 2 and tabulated in the appendix.

Transition and Separation Locations

The variation of boundary-layer transition location with lift coefficient for the S825 airfoil is shown in figure 3 and tabulated in the appendix. It should be remembered that the

method of references 15 and 16 “defines” the transition location as the end of the laminar boundary layer whether due to natural transition or laminar separation. Thus, for conditions that result in relatively long laminar separation bubbles (low lift coefficients for the upper surface, high lift coefficients for the lower surface, and low Reynolds numbers), poor agreement between the predicted “transition” locations and the locations measured experimentally can be expected. This poor agreement is worsened by the fact that transition is normally confirmed in the wind tunnel only by the detection of attached turbulent flow. For conditions that result in shorter laminar separation bubbles (high lift coefficients for the upper surface, low lift coefficients for the lower surface, and high Reynolds numbers), the agreement between theory and experiment should be quite good. (See refs. 20 and 24.)

The variation of turbulent boundary-layer separation location with lift coefficient for the S825 airfoil is shown in figure 3 and tabulated in the appendix. A small, trailing-edge separation is predicted on the upper surface at most lift coefficients. This separation, which is caused by the separation ramp (fig. 2), increases in length with transition fixed and rough. Separation is predicted on the lower surface at lower lift coefficients. Such separation usually has little effect on the section characteristics. (See ref. 20.)

Section Characteristics

Reynolds number effects.— The section characteristics of the S825 airfoil are shown in figure 3 and tabulated in the appendix. It should be noted that the maximum lift coefficient computed by the method of references 15 and 16 is not always realistic. Accordingly, an empirical criterion should be applied to the computed results. This criterion assumes that the maximum lift coefficient has been reached if the drag coefficient of the upper surface is greater than 0.0150 or if the length of turbulent separation on the upper surface is greater than 0.10. Thus, the maximum lift coefficient for the design Reynolds number of 2.0×10^6 is estimated to be 1.44, which exceeds the design objective by 3 percent. Based on the variation of the upper-surface separation location with lift coefficient, the stall characteristics are expected to be docile, which meets the design goal. Low profile-drag coefficients are predicted over the range of lift coefficients from about 0 to more than 1.3, which exceeds the range specified (0.40 to 1.20). The drag coefficient at the specified lower limit of the low-drag range ($c_l = 0.40$) is predicted to be 0.0076, which is 5 percent below the design objective. The zero-lift pitching-moment coefficient is predicted to be -0.18 , which exceeds the design constraint. However, the method of references 15 and 16 generally overpredicts the pitching-moment coefficient by about 20 percent. Thus, the actual zero-lift pitching-moment coefficient should be about -0.15 , which satisfies the constraint.

An additional analysis (not shown) indicates that significant (drag-producing) laminar separation bubbles should not occur on either surface for any relevant operating condition.

Effect of roughness.— The effect of roughness on the section characteristics of the S825 airfoil is shown in figure 3. The maximum lift coefficient for the design Reynolds number of 2.0×10^6 with transition fixed is estimated to be 1.37, a reduction of less than 5 percent from that for the transition-free condition. For the rough condition, the maximum lift coeffi-

cient for the design Reynolds number is estimated to be 1.31, a reduction of 9 percent from that for the transition-free condition. Thus, the design requirement has essentially been satisfied. The effect of roughness on the maximum lift coefficient increases with decreasing Reynolds number. The drag coefficients are, of course, adversely affected by the roughness.

S826 AIRFOIL

Pressure Distributions

The inviscid pressure distributions for the S826 airfoil at various angles of attack are shown in figure 4 and tabulated in the appendix.

Transition and Separation Locations

The variations of transition and turbulent-separation locations with lift coefficient for the S826 airfoil are shown in figure 5 and tabulated in the appendix. A small, trailing-edge separation is predicted on the upper surface at most lift coefficients. This separation, which is caused by the separation ramp (fig. 4), increases in length with transition fixed and rough. Separation is predicted on the lower surface at lower lift coefficients. This separation is not considered important because it occurs at lift coefficients that are not typical of normal wind-turbine operations. Also, such separation usually has little effect on the section characteristics.

Section Characteristics

Reynolds number effects.— The section characteristics of the S826 airfoil are shown in figure 5 and tabulated in the appendix. Using the previously-described criterion, the maximum lift coefficient for the design Reynolds number of 1.5×10^6 is estimated to be 1.42, which exceeds the design objective by 1 percent. The stall characteristics are expected to be docile, which meets the design goal. Low profile-drag coefficients are predicted over the range of lift coefficients from less than 0.3 to more than 1.3, which exceeds the range specified (0.40 to 1.20). The drag coefficient at the specified lower limit of the low-drag range ($c_l = 0.40$) is predicted to be 0.0073, which exceeds the design objective by 22 percent. The achievement of this objective was sacrificed to meet the other, more important objectives and constraints. The zero-lift pitching-moment coefficient is predicted to be -0.18 , which exceeds the design constraint. Again, because the method of references 15 and 16 generally overpredicts the pitching-moment coefficient, the actual zero-lift pitching-moment coefficient should be about -0.15 , which satisfies the constraint. Significant (drag-producing) laminar separation bubbles should not occur on either surface for any relevant operating condition.

Effect of roughness.— The effect of roughness on the section characteristics of the S826 airfoil is shown in figure 5. The maximum lift coefficient for the design Reynolds number of 1.5×10^6 with transition fixed is estimated to be 1.35, a reduction of less than 5 percent

from that for the transition-free condition. For the rough condition, the maximum lift coefficient for the design Reynolds number is estimated to be 1.31, a reduction of less than 8 percent from that for the transition-free condition. Thus, the design requirement has essentially been satisfied. The effect of roughness on the maximum lift coefficient increases with decreasing Reynolds number. The drag coefficients are, of course, adversely affected by the roughness.

CONCLUDING REMARKS

A family of airfoils, the S825 and S826, for 20- to 40-meter, variable-speed and variable-pitch (toward feather), horizontal-axis wind turbines has been designed and analyzed theoretically. The two primary objectives of a high maximum lift coefficient, insensitive to leading-edge roughness, and low profile-drag coefficients have been achieved. The constraints on the zero-lift pitching-moment coefficients and the airfoil thicknesses have been satisfied. The airfoils should exhibit docile stall characteristics.

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TABLE I.– AIRFOIL DESIGN SPECIFICATIONS

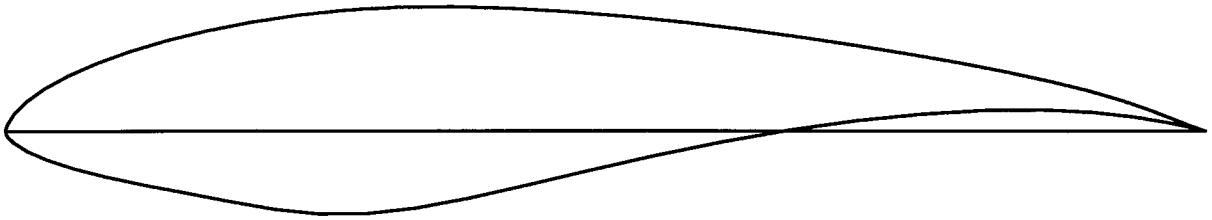
<u>Parameter</u>	<u>Objective/Constraint</u>	
	Primary	Tip
Airfoil		
Blade radial station	0.75	0.95
Reynolds number	2.0×10^6	1.5×10^6
Maximum lift coefficient	≥ 1.40	≥ 1.40
Low-drag, lift-coefficient range		
Lower limit	0.40	0.40
Upper limit	1.20	1.20
Minimum profile-drag coefficient	≤ 0.0080	≤ 0.0060
Zero-lift pitching-moment coefficient	≥ -0.15	≥ -0.15
Thickness	0.17c	0.14c

TABLE II.- S825 AIRFOIL COORDINATES

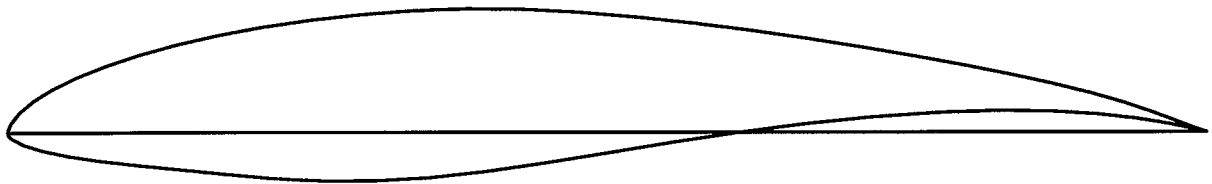
Upper Surface		Lower Surface	
x/c	y/c	x/c	y/c
0.00001	0.00030	0.00014	-0.00143
.00028	.00224	.00081	-.00307
.00129	.00543	.00197	-.00477
.00721	.01481	.00650	-.00920
.01766	.02500	.01819	-.01650
.03250	.03549	.03502	-.02381
.05161	.04596	.05670	-.03093
.07479	.05616	.08297	-.03780
.10185	.06588	.11351	-.04443
.13251	.07494	.14790	-.05114
.16643	.08315	.18480	-.05834
.20324	.09032	.22231	-.06499
.24253	.09625	.25997	-.06891
.28387	.10060	.29879	-.06869
.32709	.10296	.34011	-.06415
.37230	.10329	.38475	-.05600
.41930	.10195	.43307	-.04520
.46763	.09920	.48499	-.03306
.51676	.09525	.53974	-.02082
.56616	.09029	.59631	-.00935
.61526	.08450	.65355	.00060
.66350	.07806	.71026	.00854
.71028	.07112	.76514	.01410
.75503	.06385	.81692	.01713
.79720	.05636	.86437	.01757
.83624	.04878	.90608	.01553
.87165	.04117	.94062	.01168
.90294	.03351	.96717	.00727
.92994	.02560	.98566	.00342
.95294	.01758	.99646	.00088
.97208	.01022	1.00000	.00000
.98695	.00450		
.99661	.00108		
1.00000	.00000		

TABLE III.— S826 AIRFOIL COORDINATES

Upper Surface		Lower Surface	
x/c	y/c	x/c	y/c
0.00018	0.00159	0.00000	-0.00005
.00255	.00748	.00021	-.00146
.00954	.01638	.00093	-.00274
.02088	.02596	.00216	-.00403
.03651	.03580	.00367	-.00525
.05636	.04562	.01367	-.01035
.08026	.05519	.02920	-.01518
.10801	.06434	.04998	-.01960
.13934	.07288	.07580	-.02362
.17395	.08068	.10637	-.02729
.21146	.08758	.14133	-.03091
.25149	.09343	.17965	-.03486
.29361	.09807	.21987	-.03855
.33736	.10133	.26153	-.04064
.38228	.10294	.30497	-.04051
.42820	.10249	.35027	-.03794
.47526	.10005	.39779	-.03280
.52324	.09607	.44785	-.02563
.57161	.09094	.50032	-.01720
.61980	.08489	.55484	-.00841
.66724	.07816	.61055	-.00015
.71333	.07095	.66644	.00699
.75749	.06341	.72142	.01254
.79915	.05572	.77434	.01621
.83778	.04798	.82409	.01784
.87287	.04029	.86953	.01741
.90391	.03262	.90945	.01498
.93072	.02479	.94257	.01113
.95355	.01695	.96813	.00689
.97251	.00982	.98604	.00324
.98719	.00431	.99655	.00084
.99668	.00103	1.00000	.00000
1.00000	.00000		

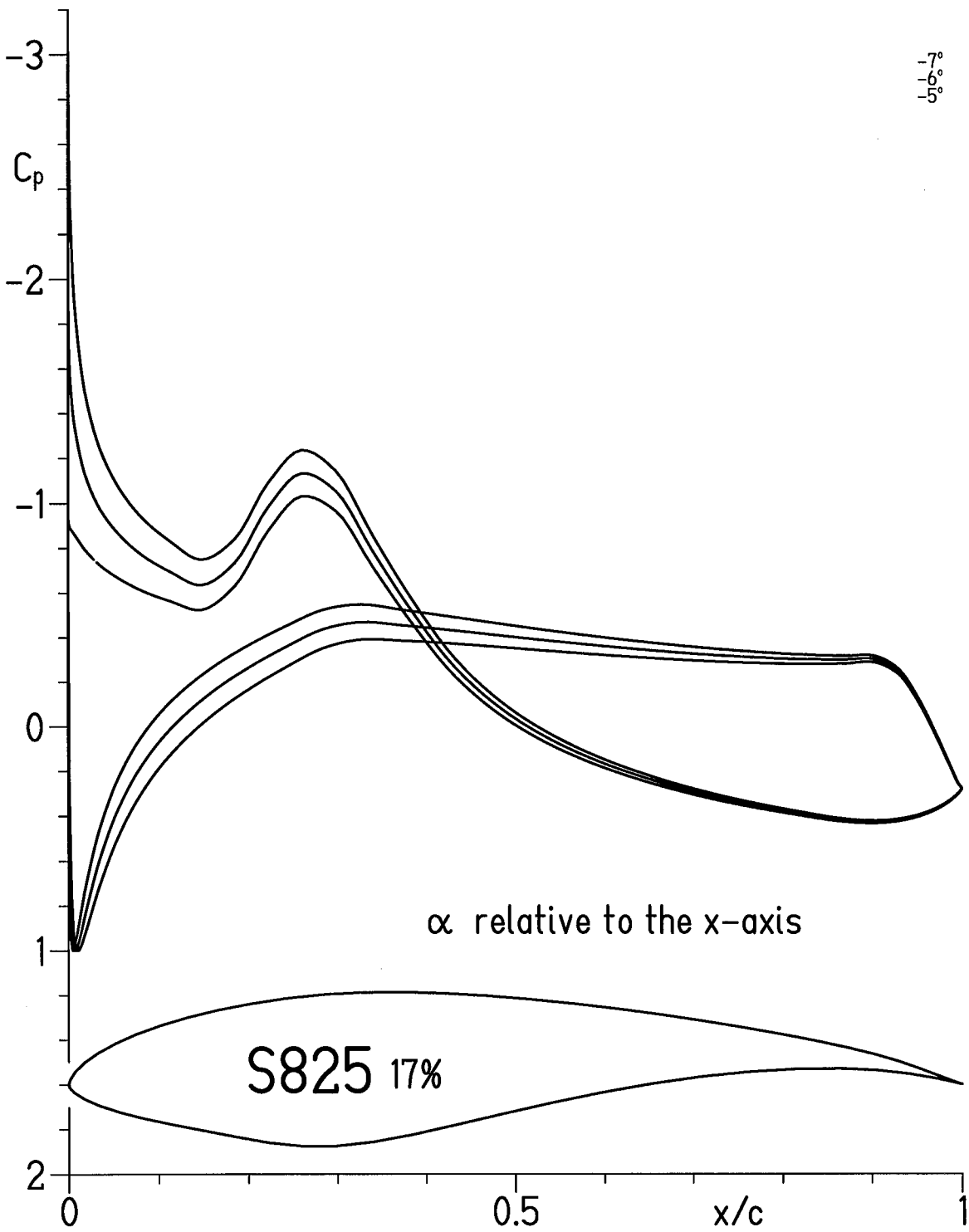


(a) S825.



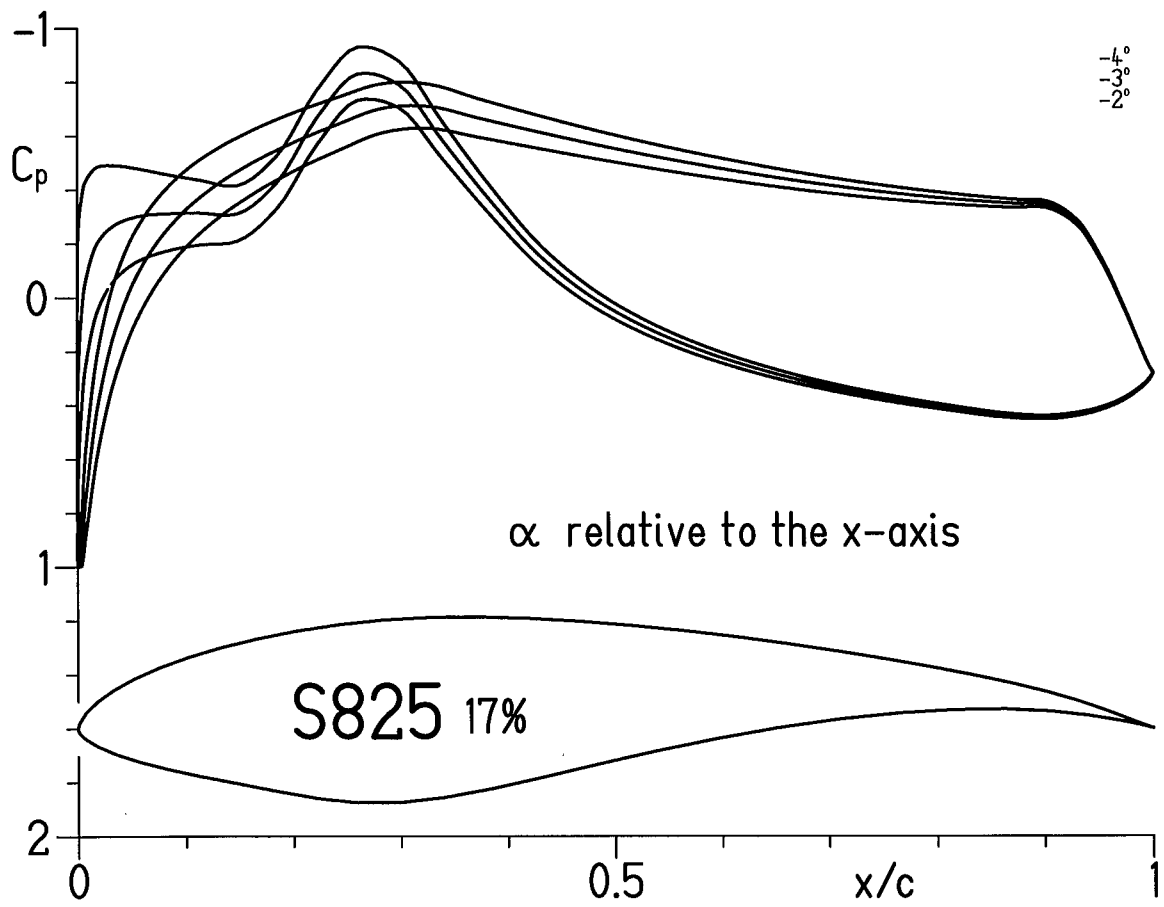
(b) S826.

Figure 1.- Airfoil shapes.



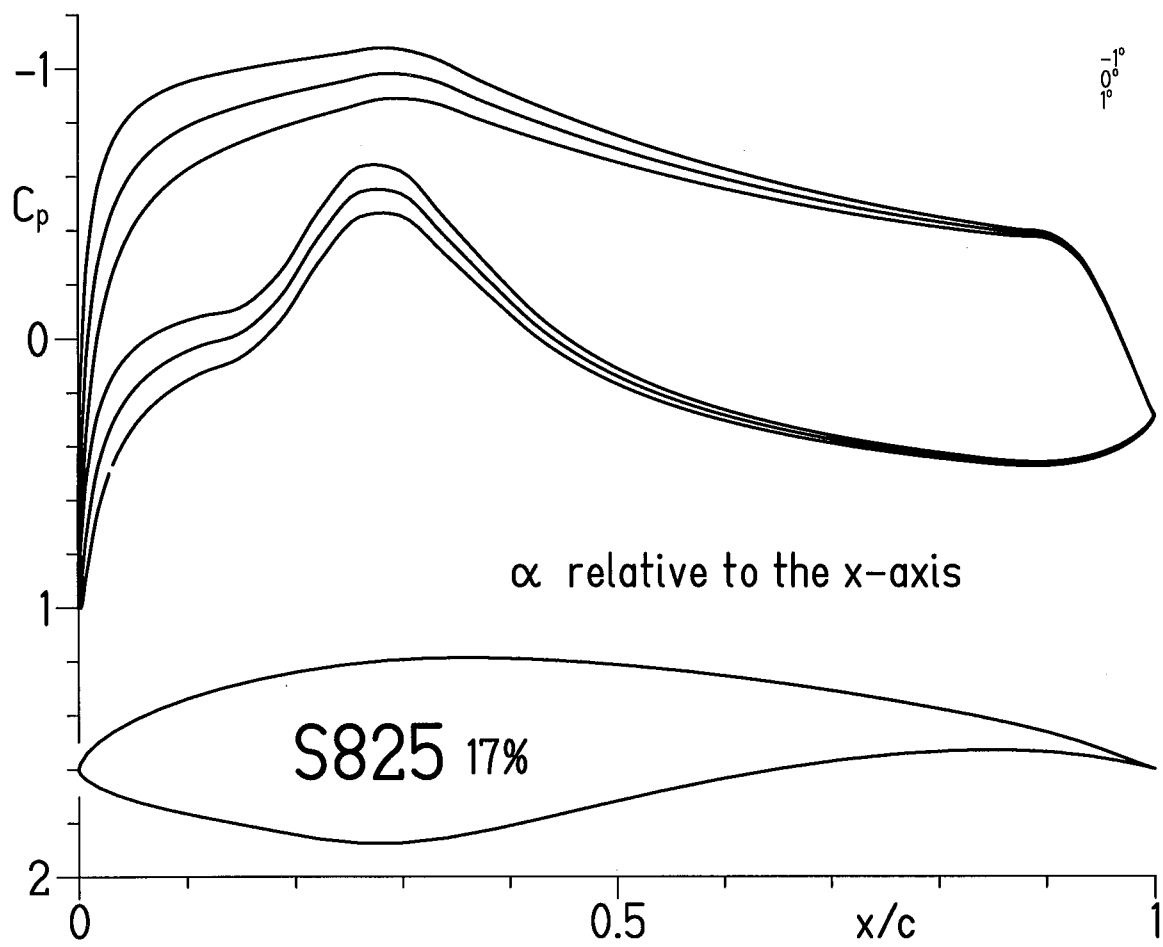
(a) $\alpha = -7^\circ, -6^\circ, \text{ and } -5^\circ$.

Figure 2.- Inviscid pressure distributions for S825 airfoil.



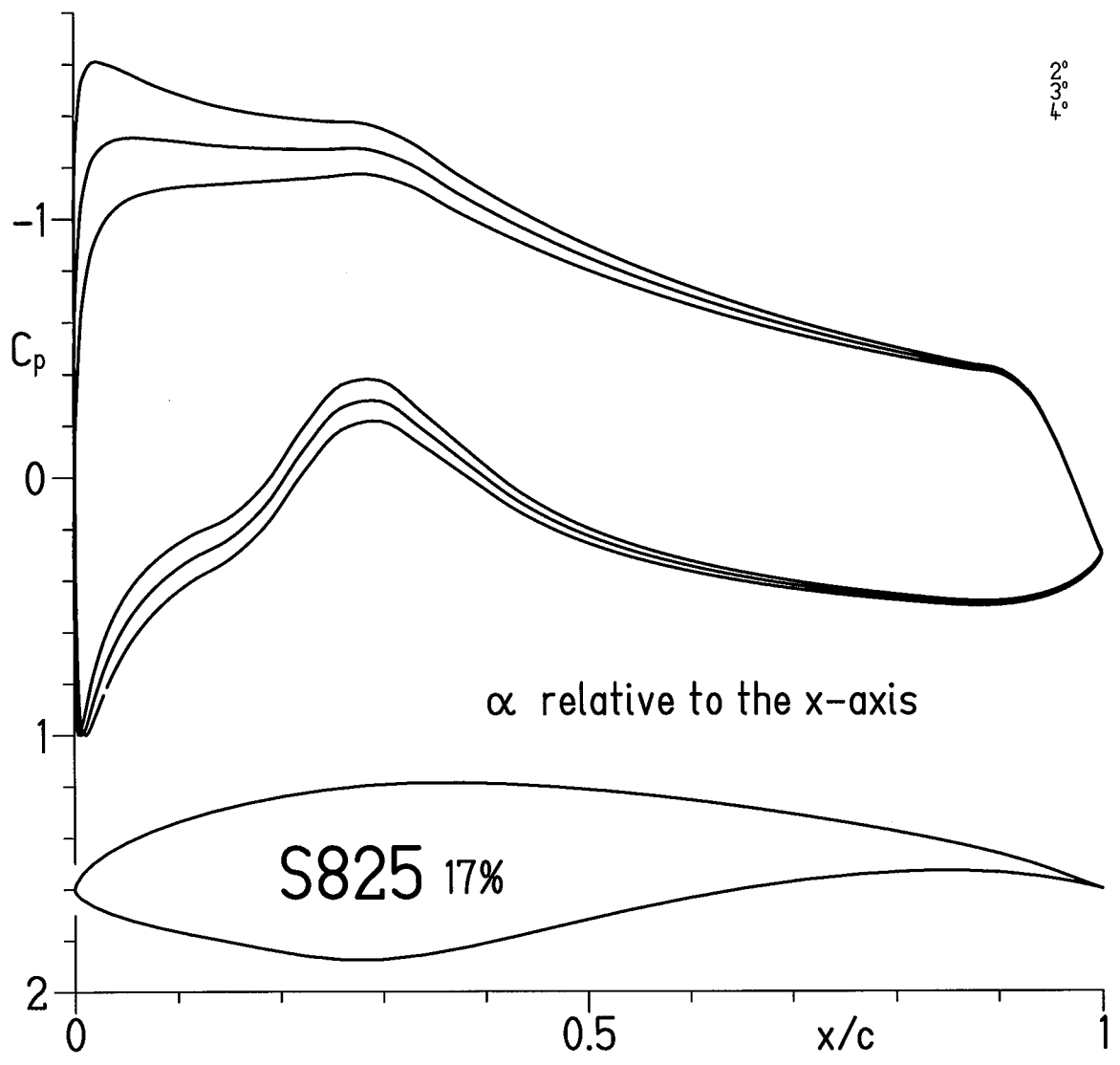
(b) $\alpha = -4^\circ, -3^\circ, \text{ and } -2^\circ$.

Figure 2.- Continued.



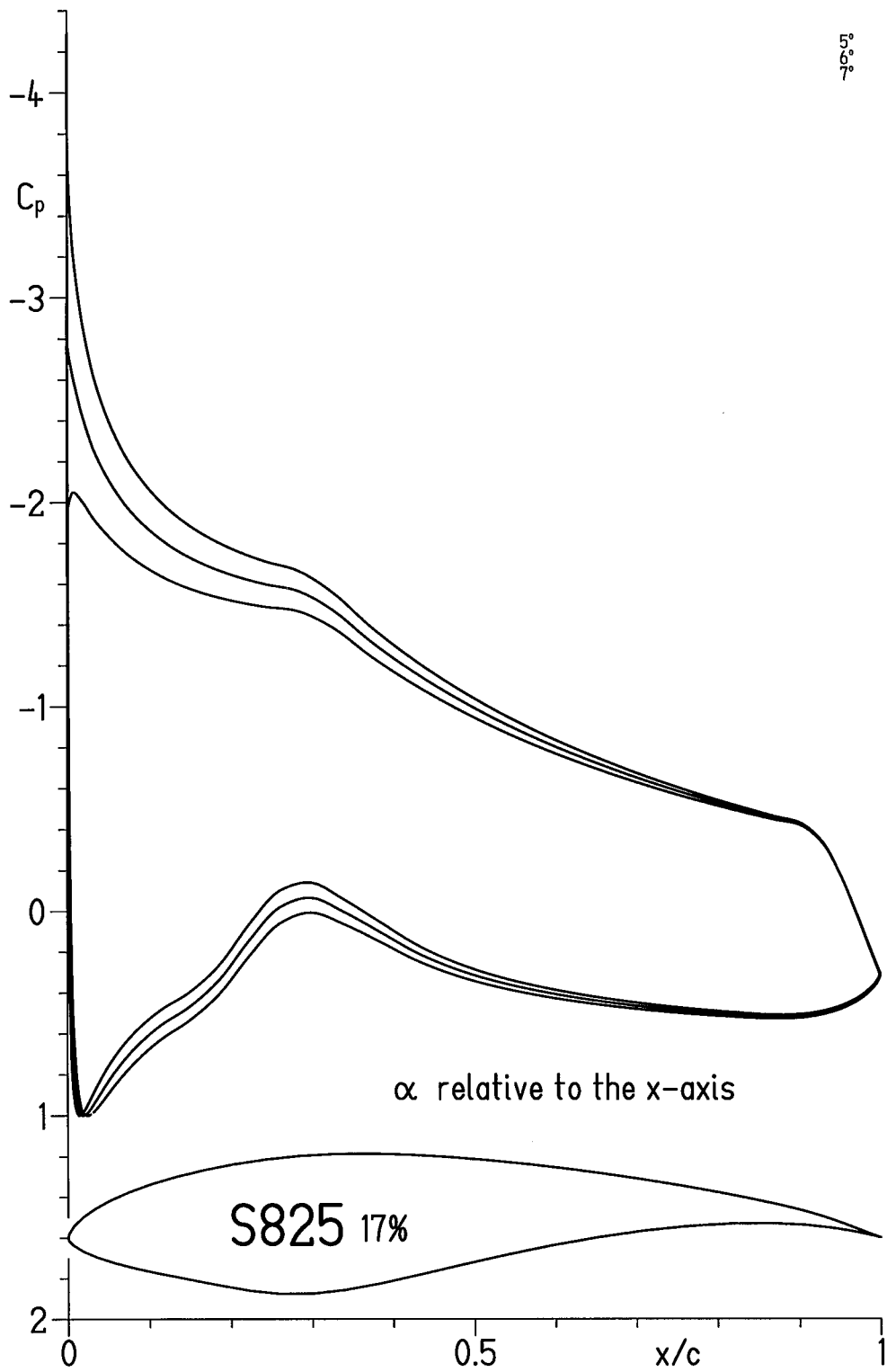
(c) $\alpha = -1^\circ, 0^\circ, \text{ and } 1^\circ$.

Figure 2.- Continued.



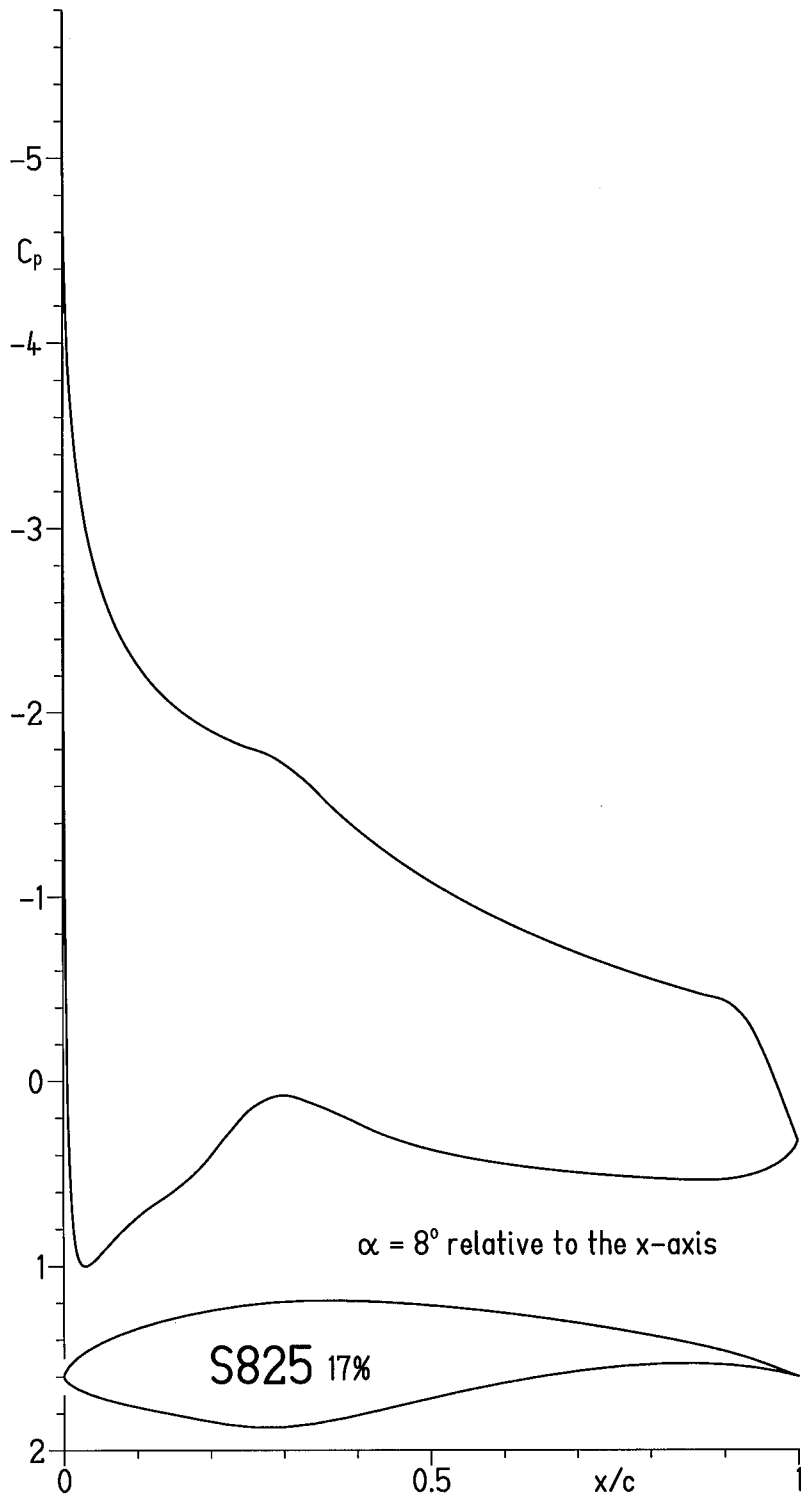
(d) $\alpha = 2^\circ, 3^\circ, \text{ and } 4^\circ$.

Figure 2.- Continued.



(e) $\alpha = 5^\circ, 6^\circ, \text{ and } 7^\circ$.

Figure 2.- Continued.



(f) $\alpha = 8^\circ$.

Figure 2.- Concluded.

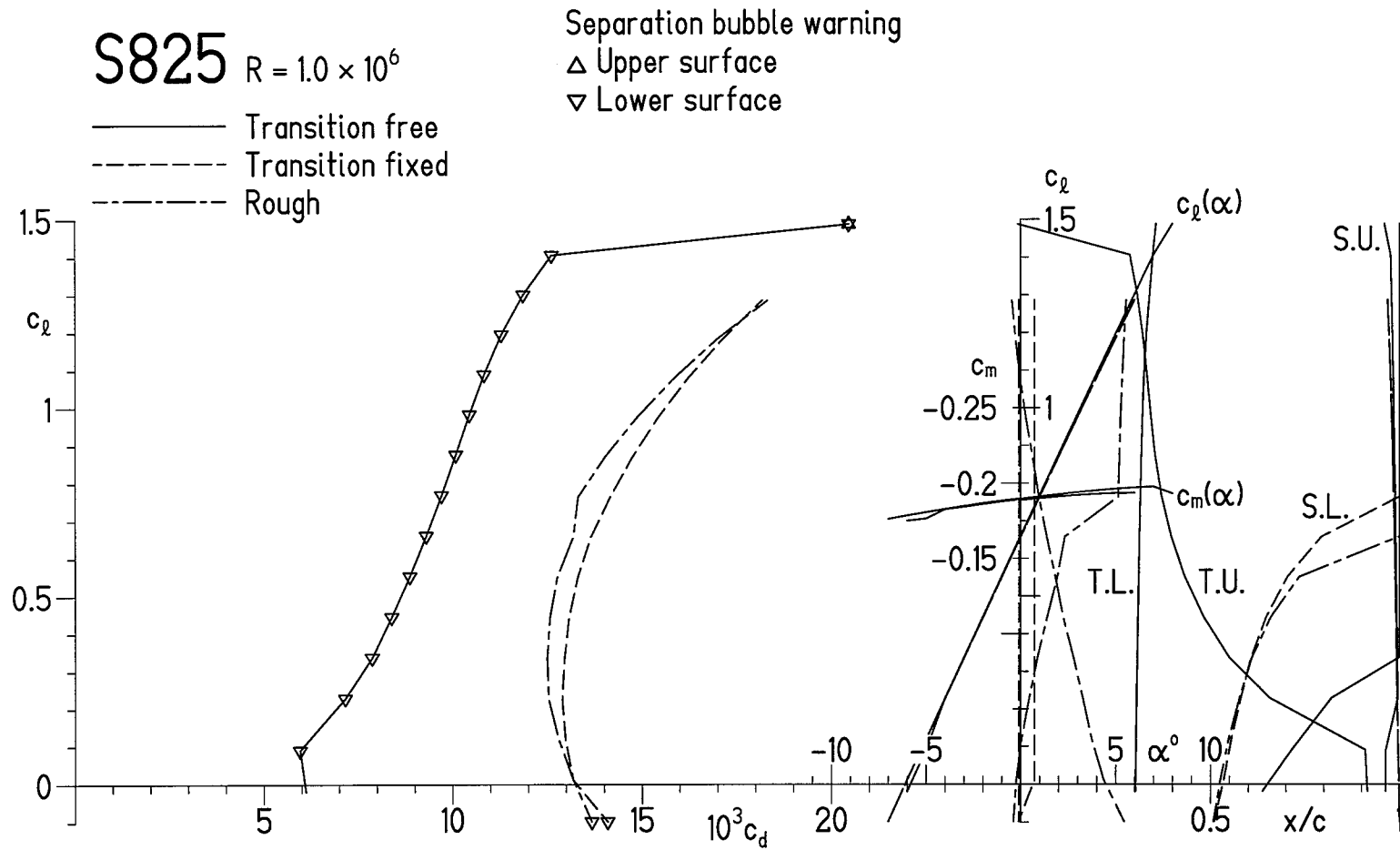
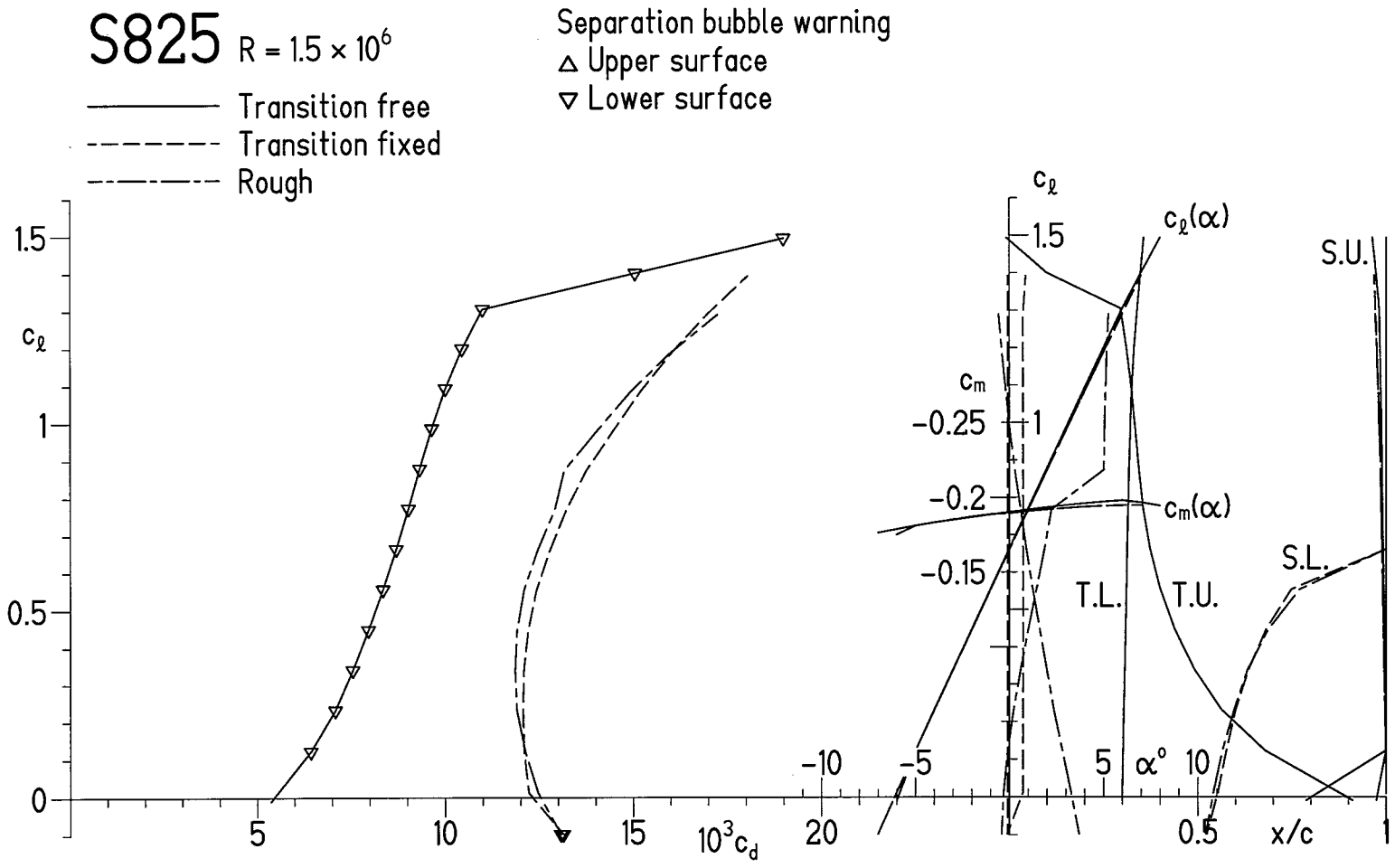
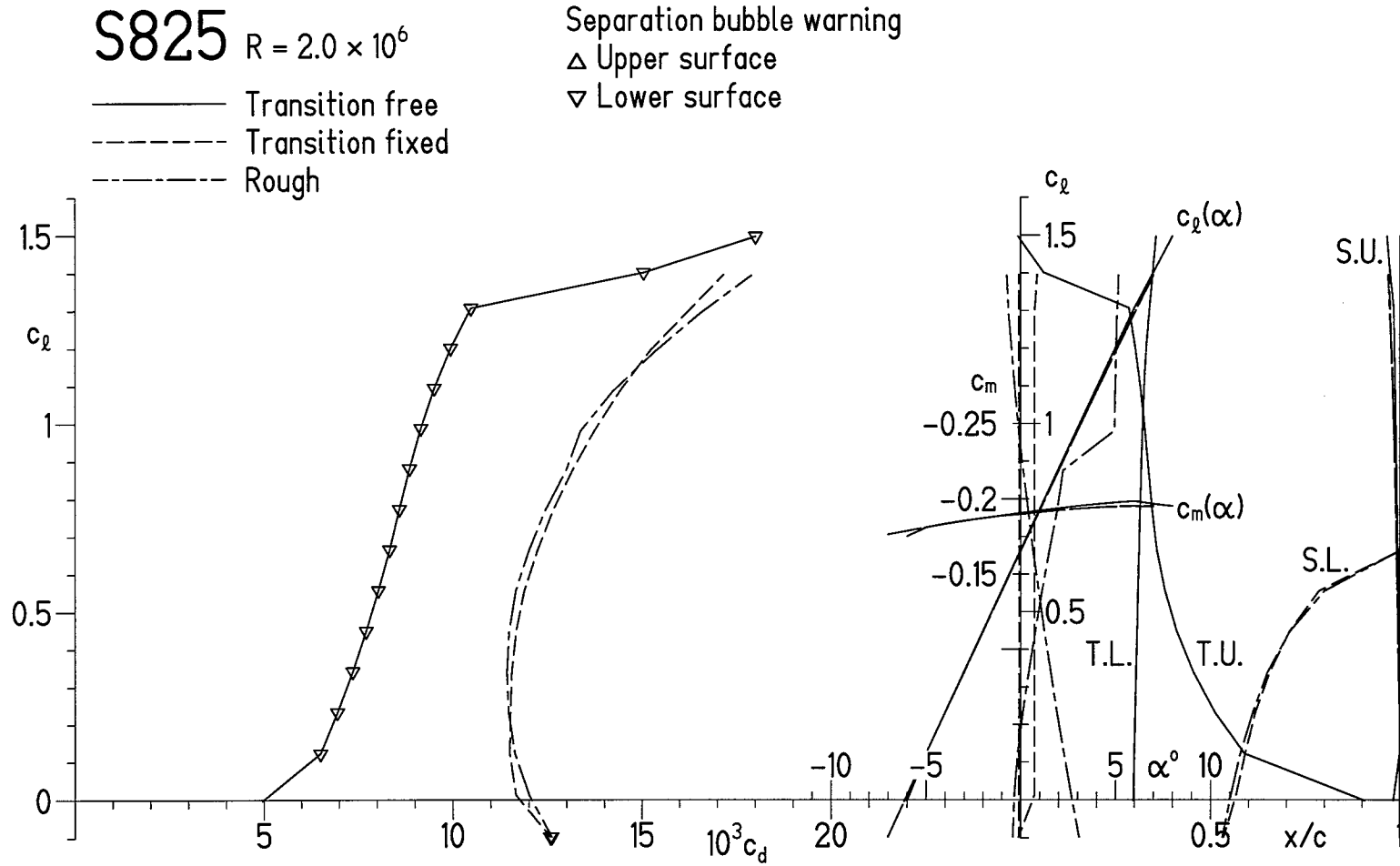
(a) $R = 1.0 \times 10^6$.

Figure 3.— Section characteristics of S825 airfoil with transition free, transition fixed, and rough.



(b) $R = 1.5 \times 10^6$.

Figure 3.- Continued.



(c) $R = 2.0 \times 10^6$.

Figure 3.- Continued.

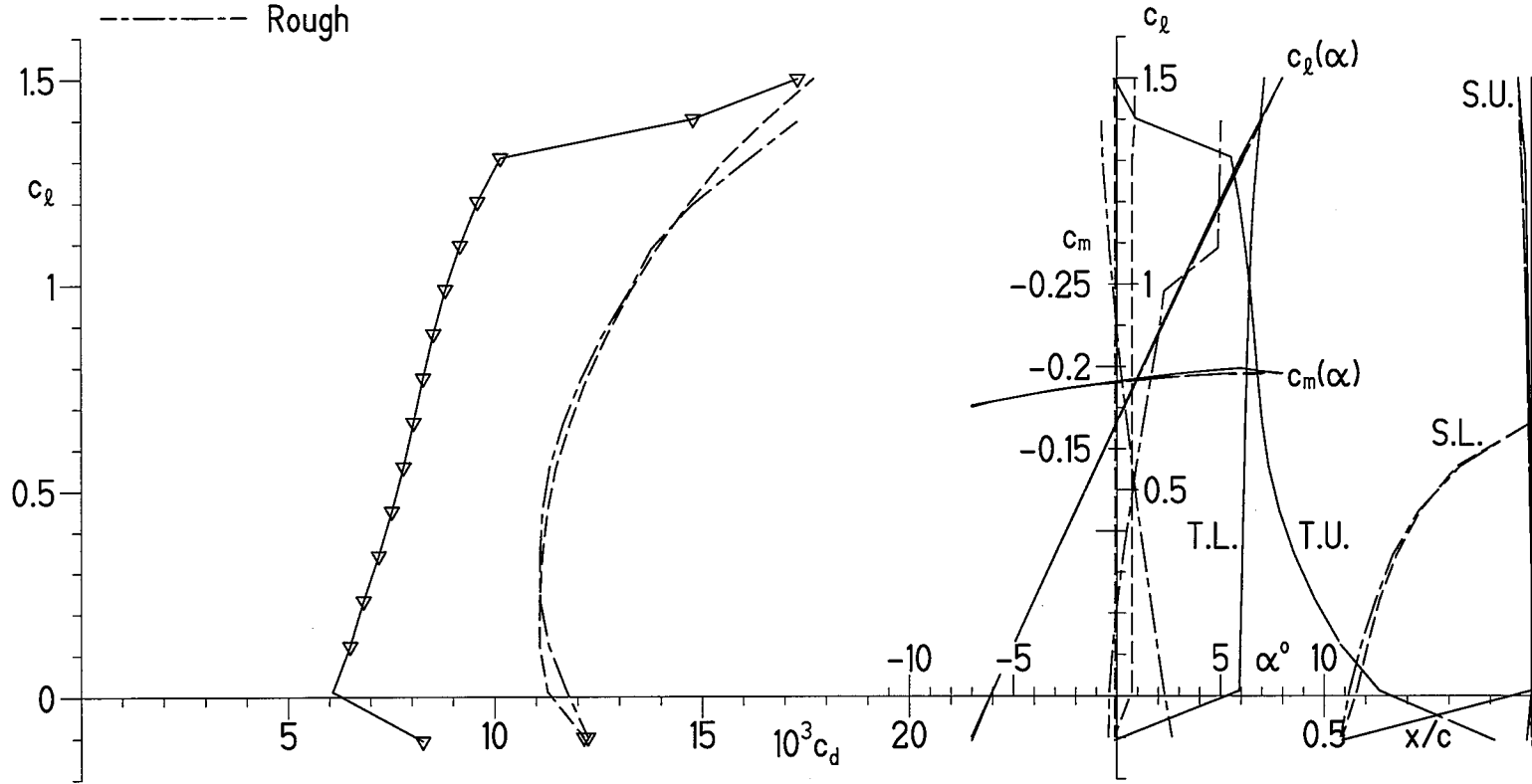
S825 $R = 2.5 \times 10^6$

— Transition free
 - - - Transition fixed
 - · - · - Rough

Separation bubble warning

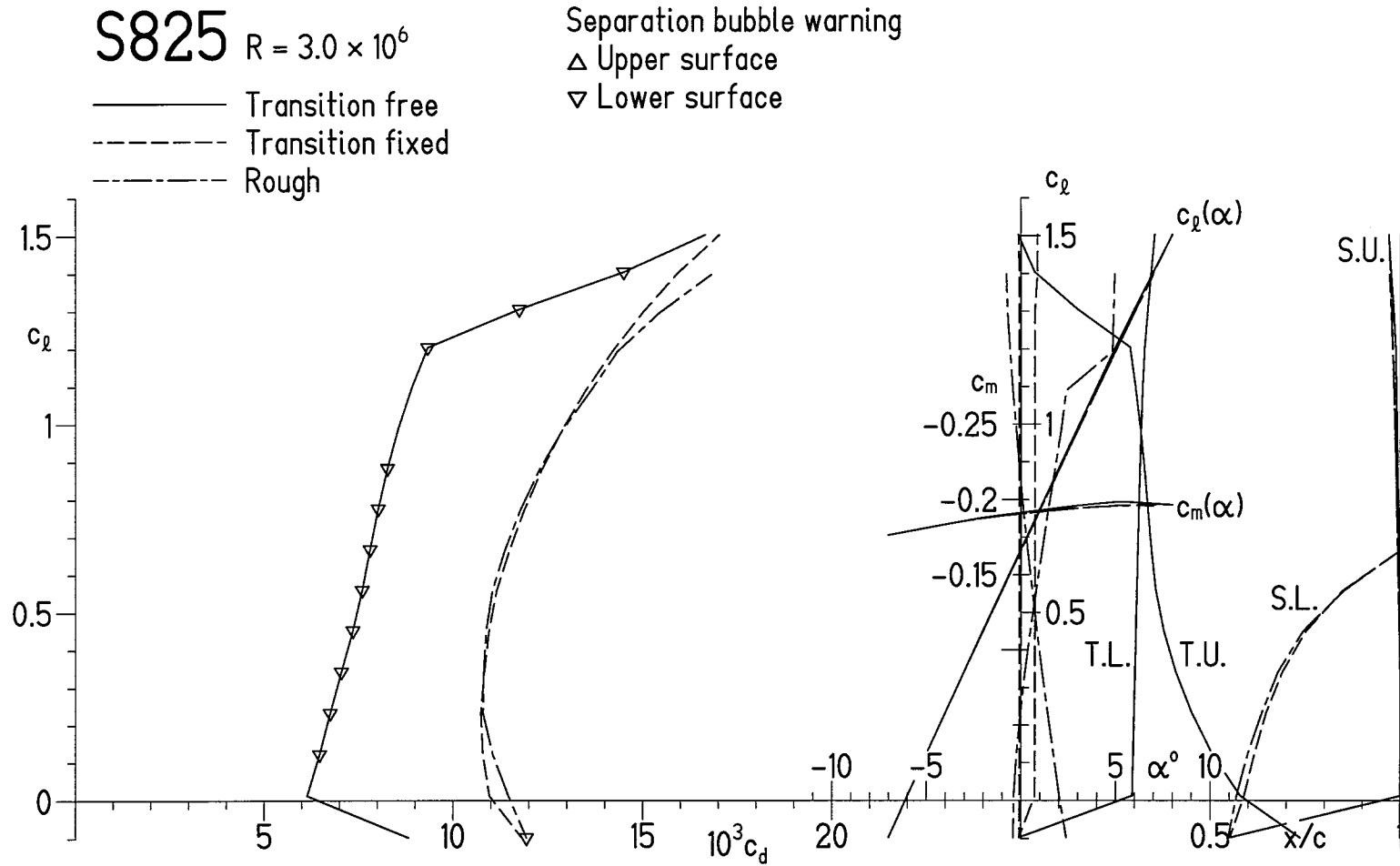
△ Upper surface

▽ Lower surface



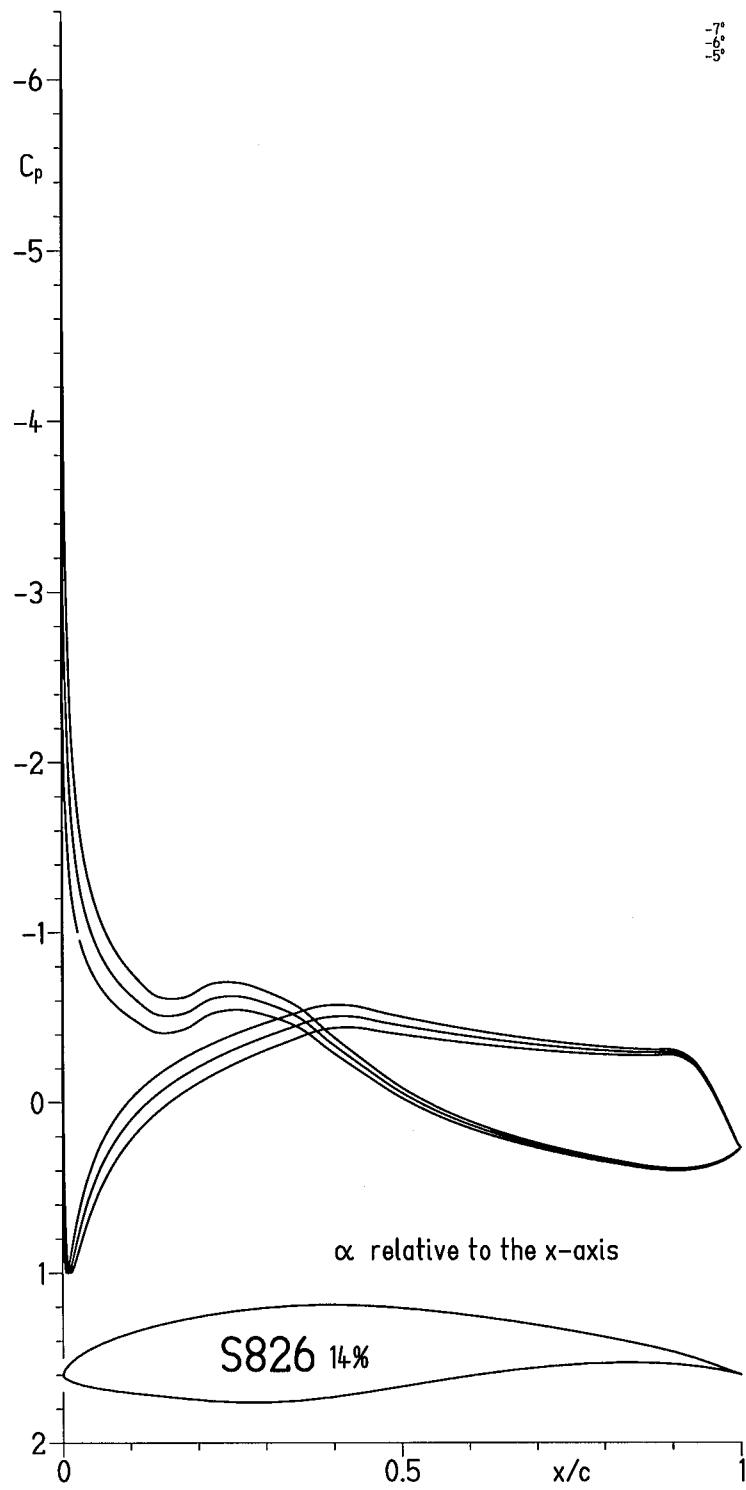
(d) $R = 2.5 \times 10^6$.

Figure 3.- Continued.



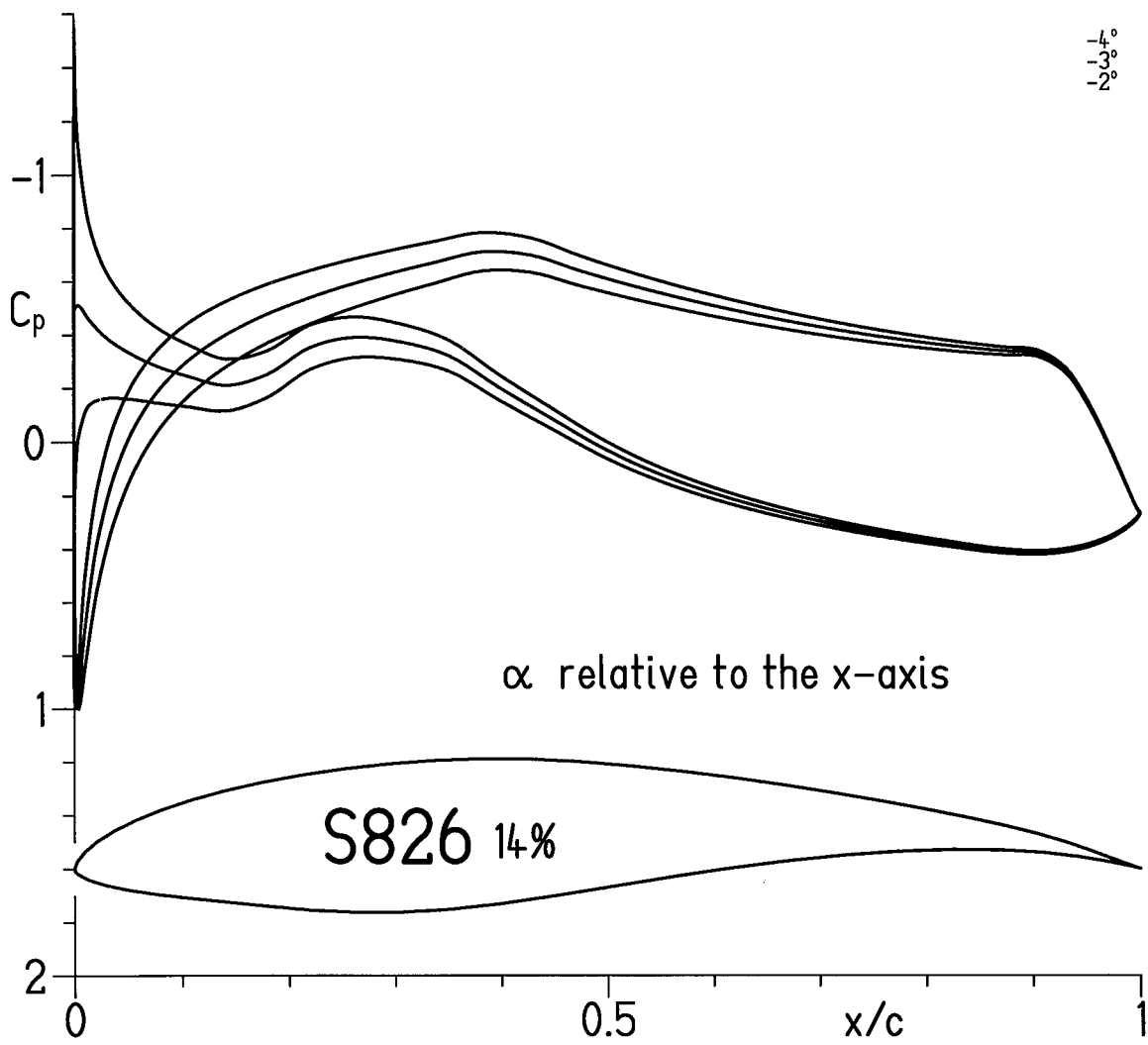
(e) $R = 3.0 \times 10^6$.

Figure 3.- Concluded.



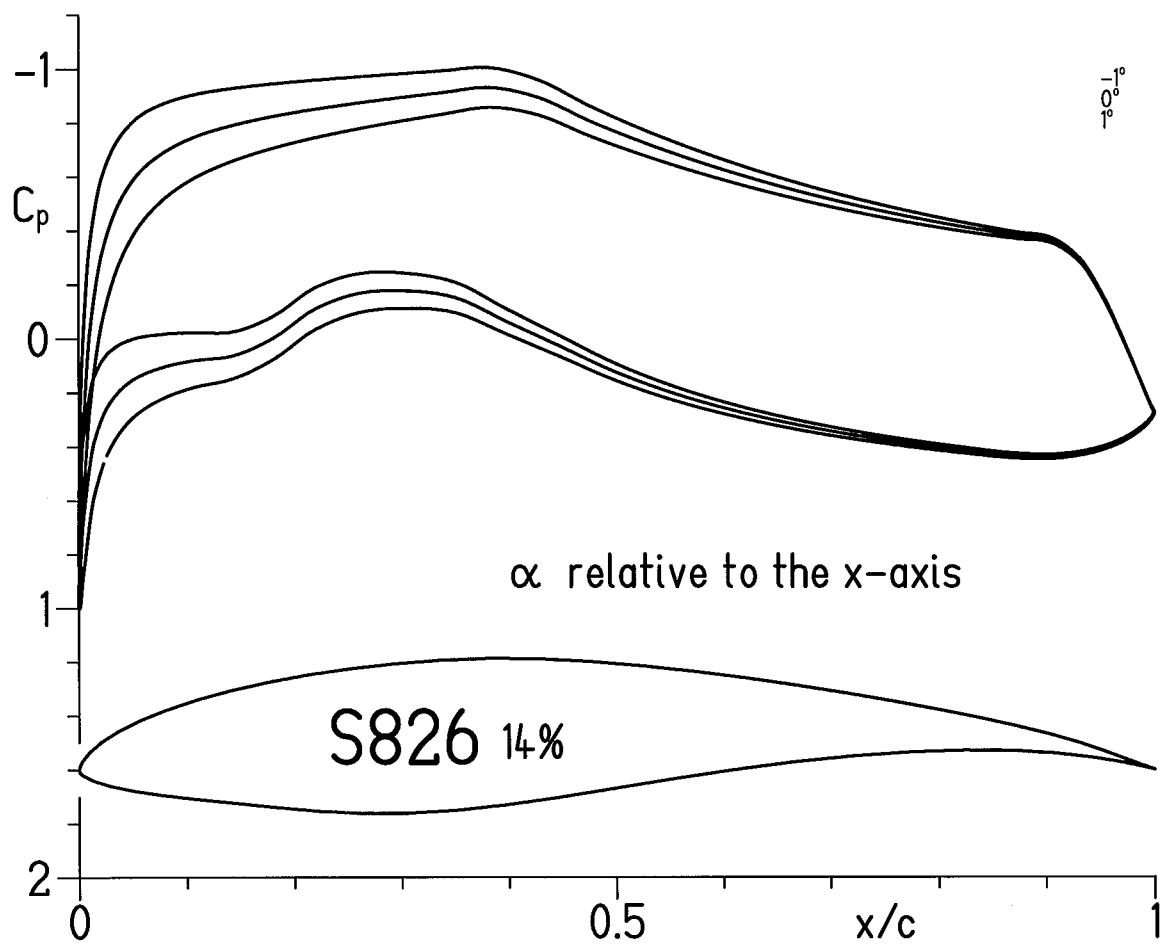
(a) $\alpha = -7^\circ, -6^\circ, \text{ and } -5^\circ$.

Figure 4.- Inviscid pressure distributions for S826 airfoil.



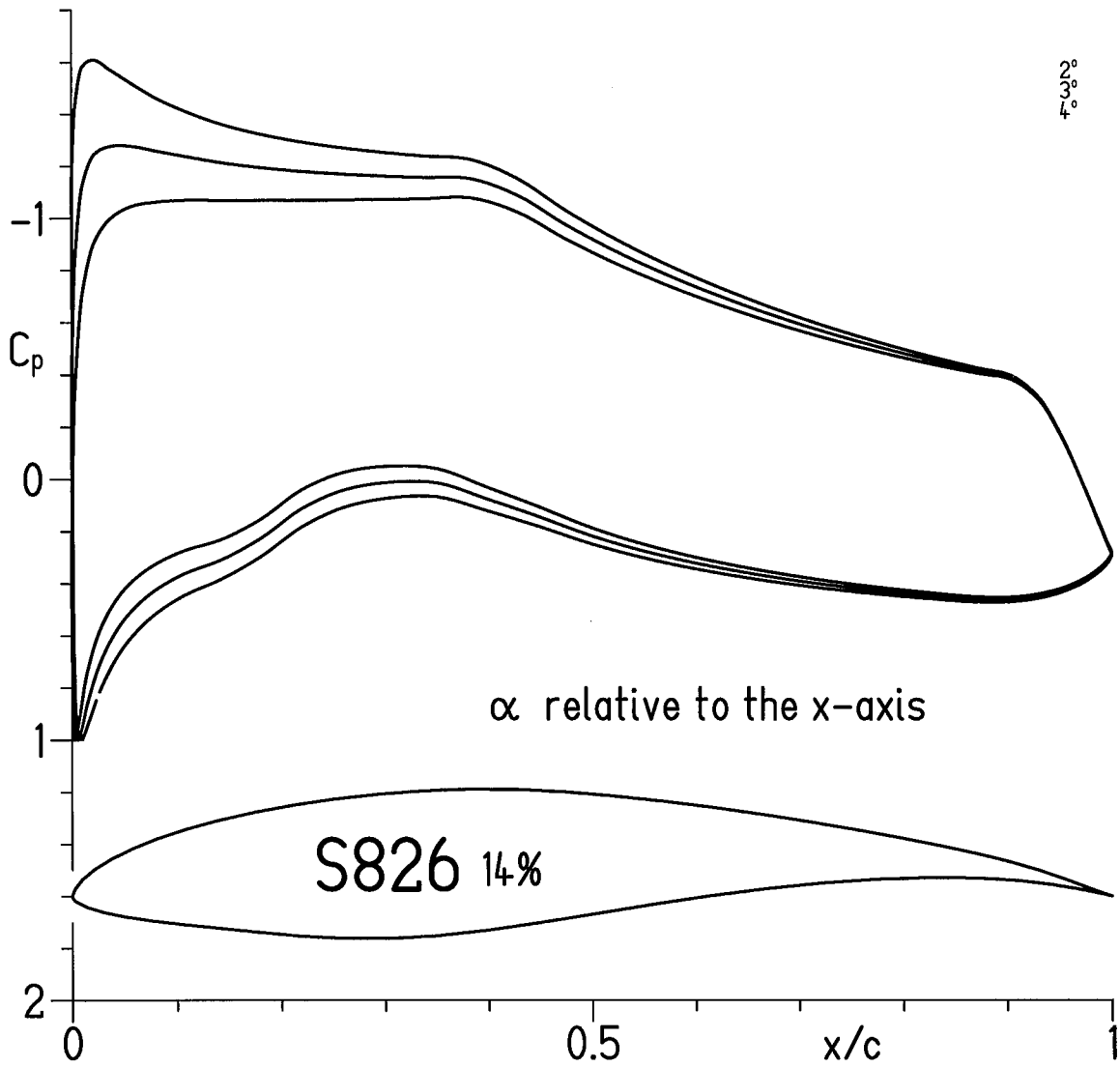
(b) $\alpha = -4^\circ, -3^\circ, \text{ and } -2^\circ$.

Figure 4.— Continued.



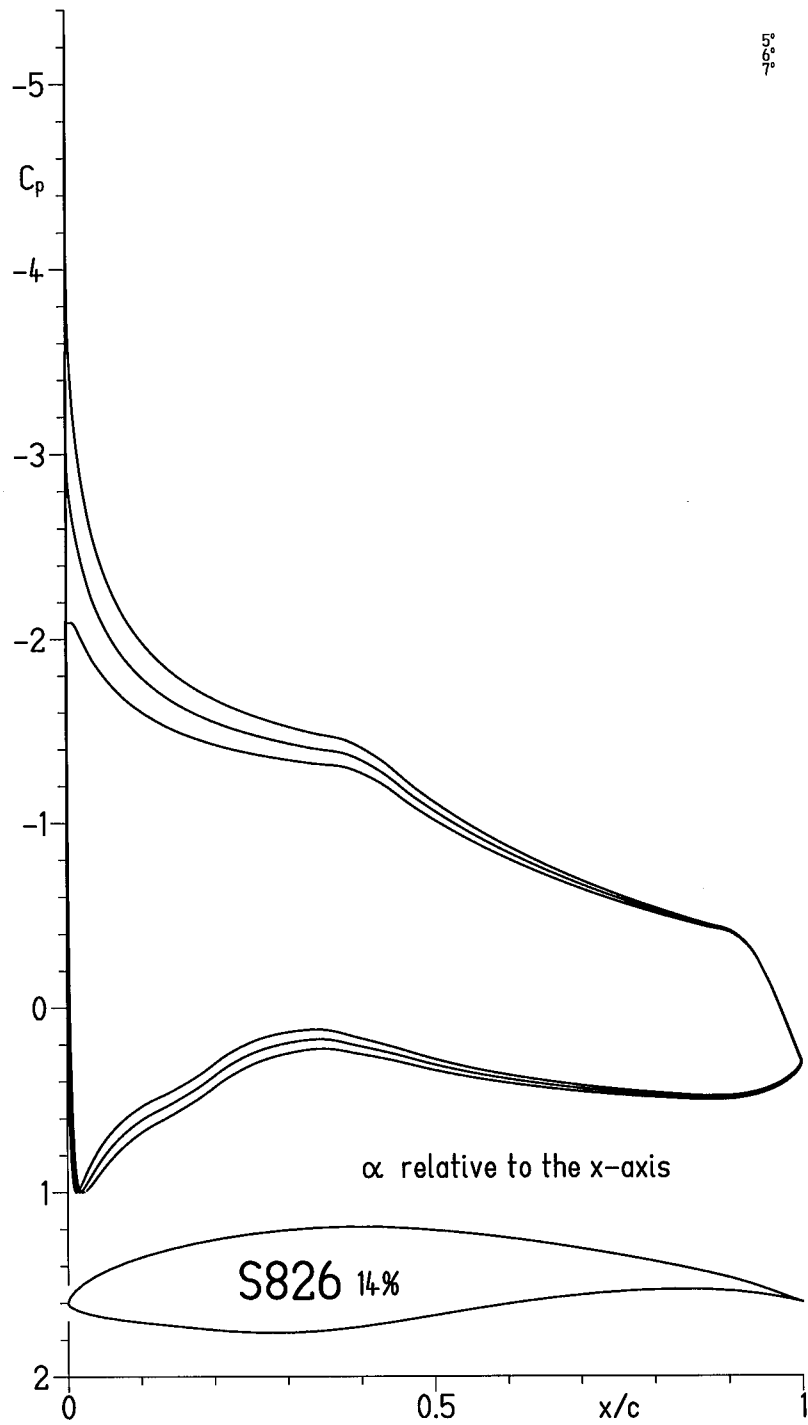
(c) $\alpha = -1^\circ, 0^\circ, \text{ and } 1^\circ$.

Figure 4.- Continued.



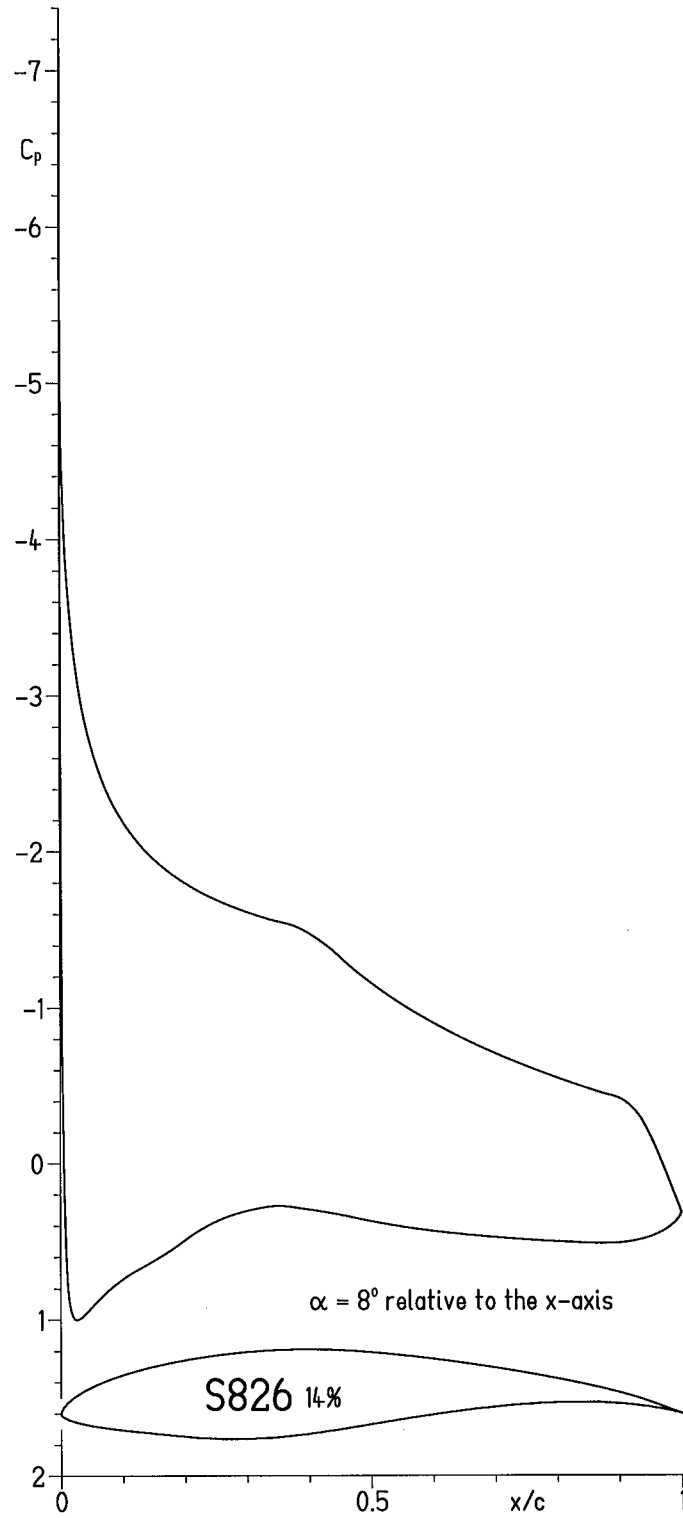
(d) $\alpha = 2^\circ, 3^\circ, \text{ and } 4^\circ$.

Figure 4.- Continued.



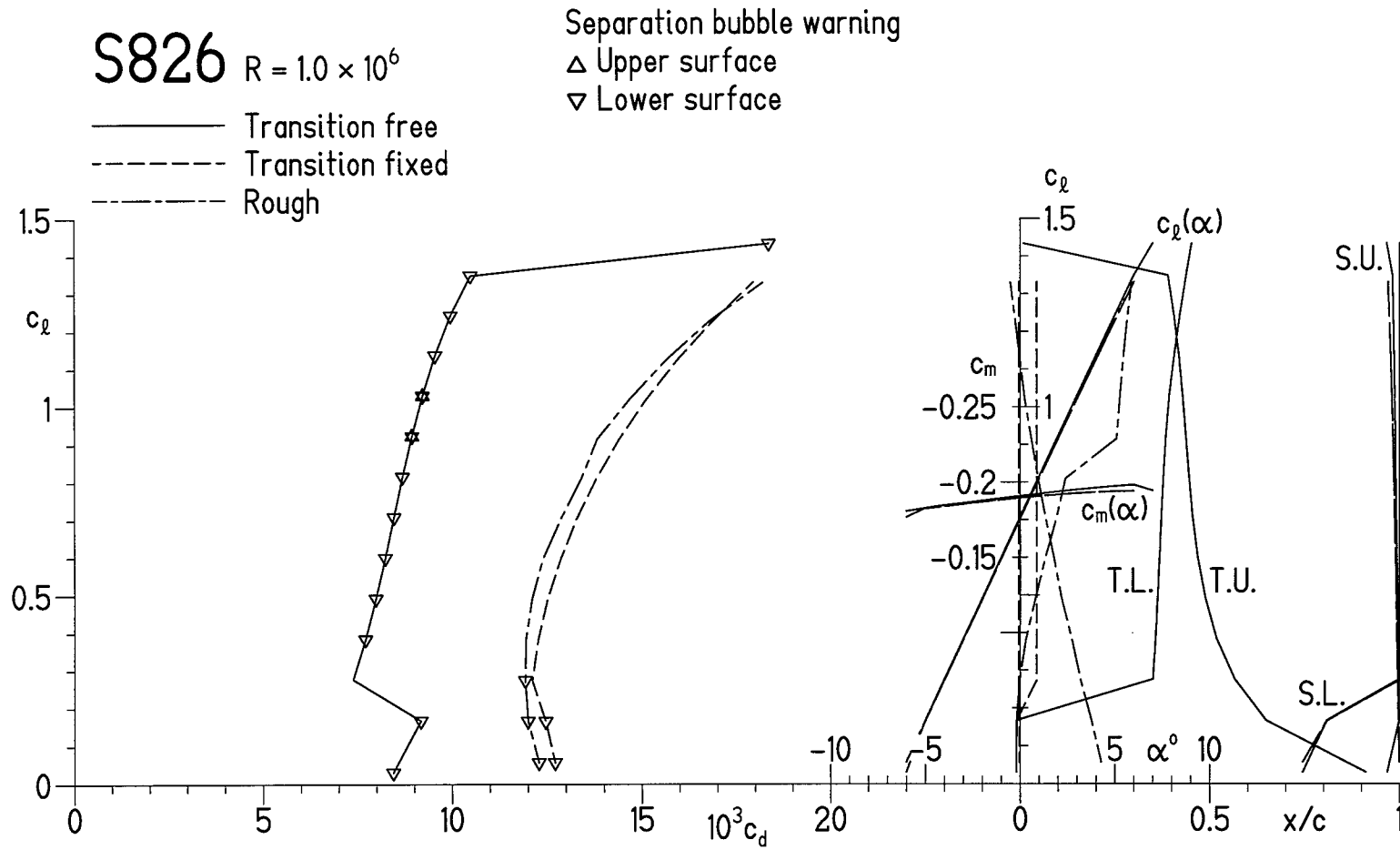
(e) $\alpha = 5^\circ, 6^\circ, \text{ and } 7^\circ$.

Figure 4.- Continued.



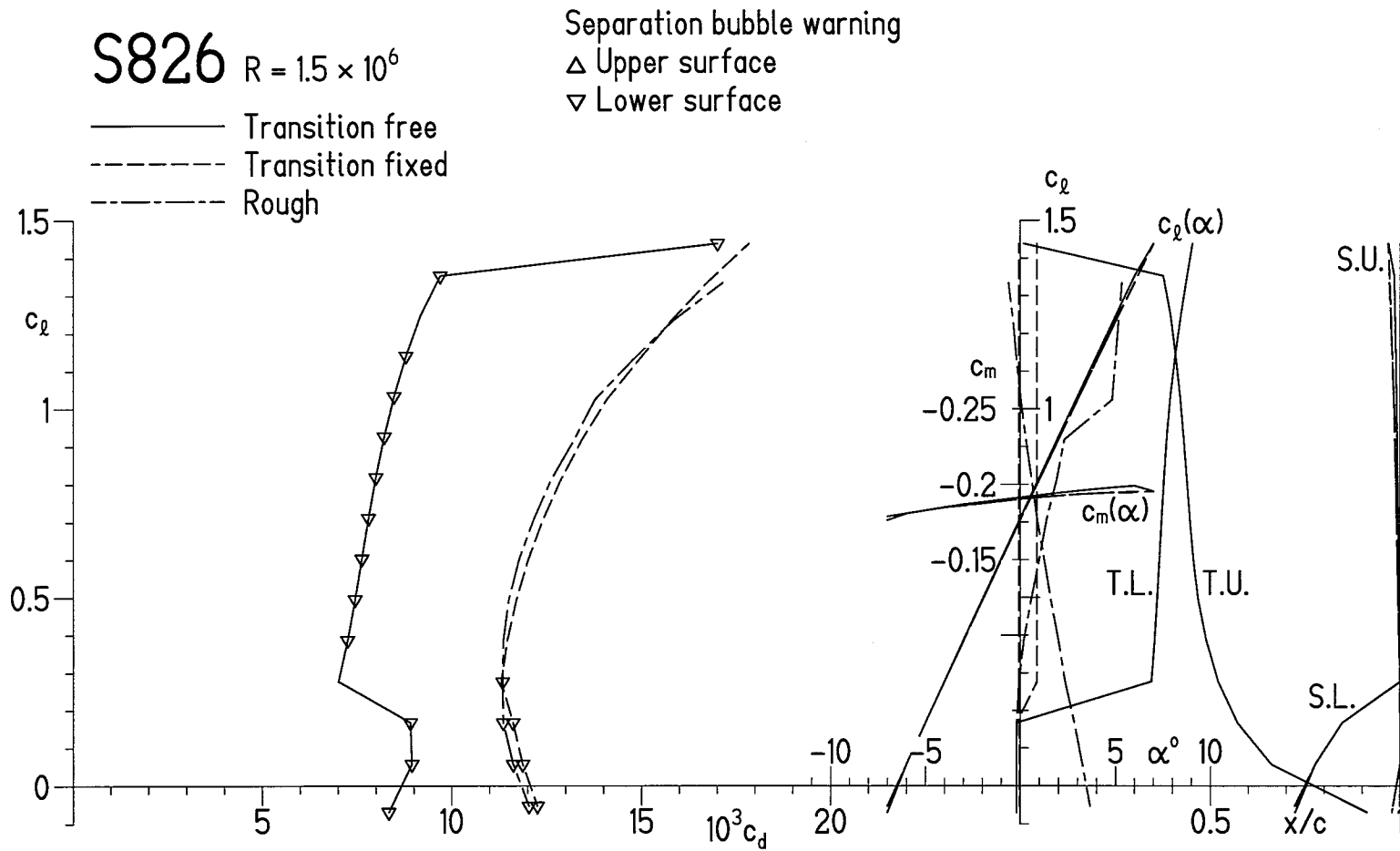
(f) $\alpha = 8^\circ$.

Figure 4.— Concluded.



(a) $R = 1.0 \times 10^6$.

Figure 5.— Section characteristics of S826 airfoil with transition free, transition fixed, and rough.



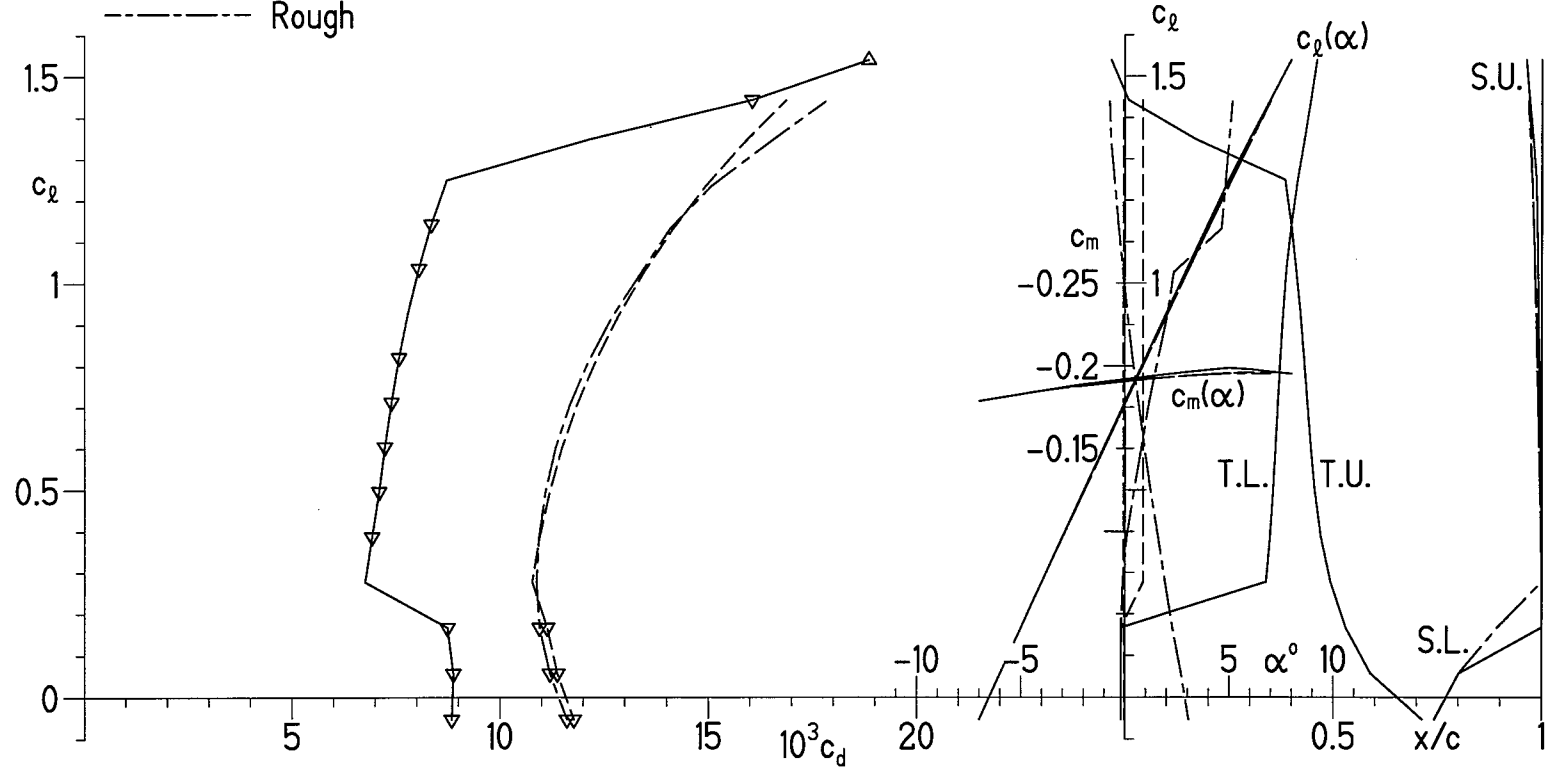
(b) $R = 1.5 \times 10^6$.

Figure 5.- Continued.

S826 $R = 2.0 \times 10^6$

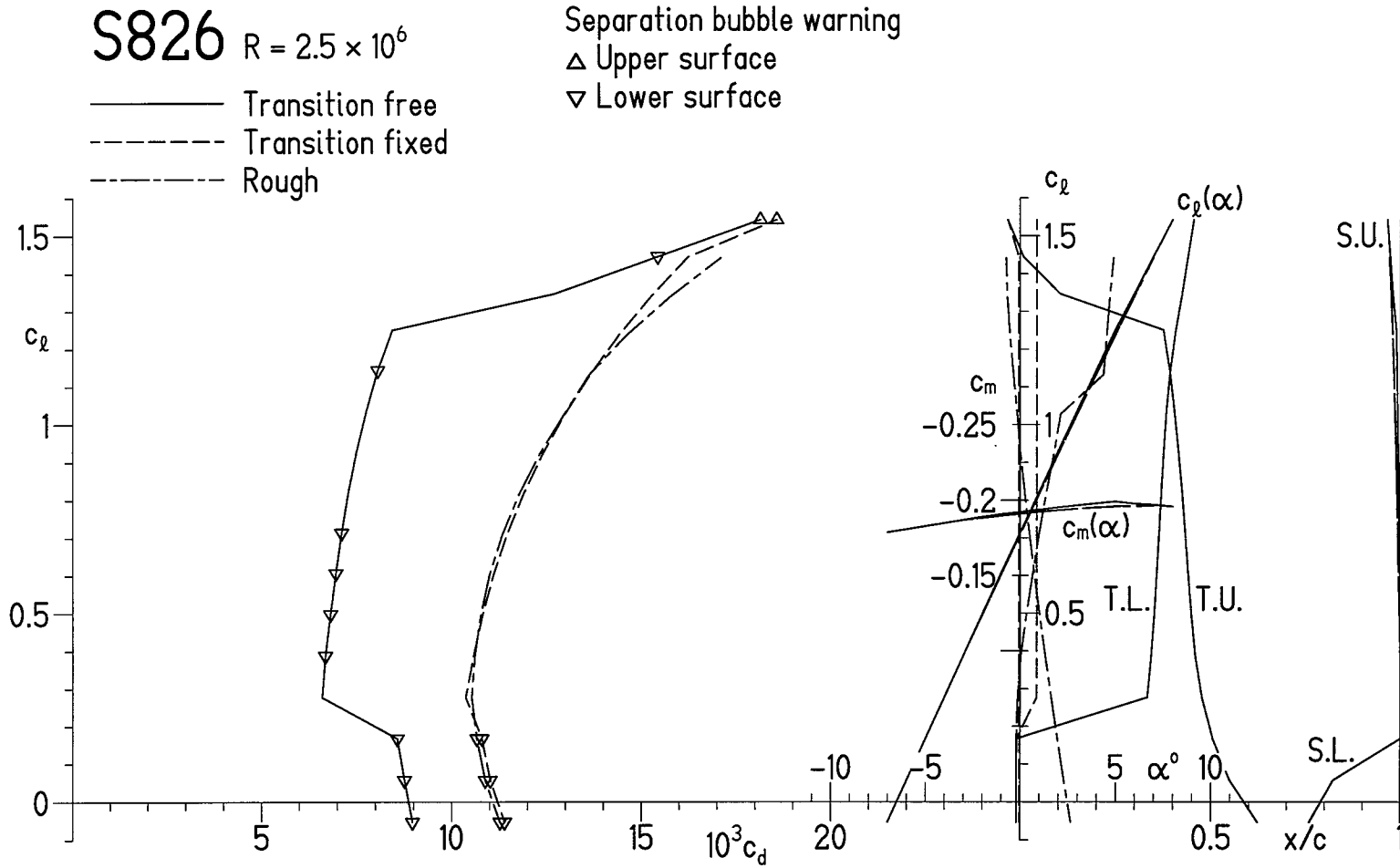
— Transition free
 - - - Transition fixed
 - · - · - Rough

Separation bubble warning
 \triangle Upper surface
 ∇ Lower surface



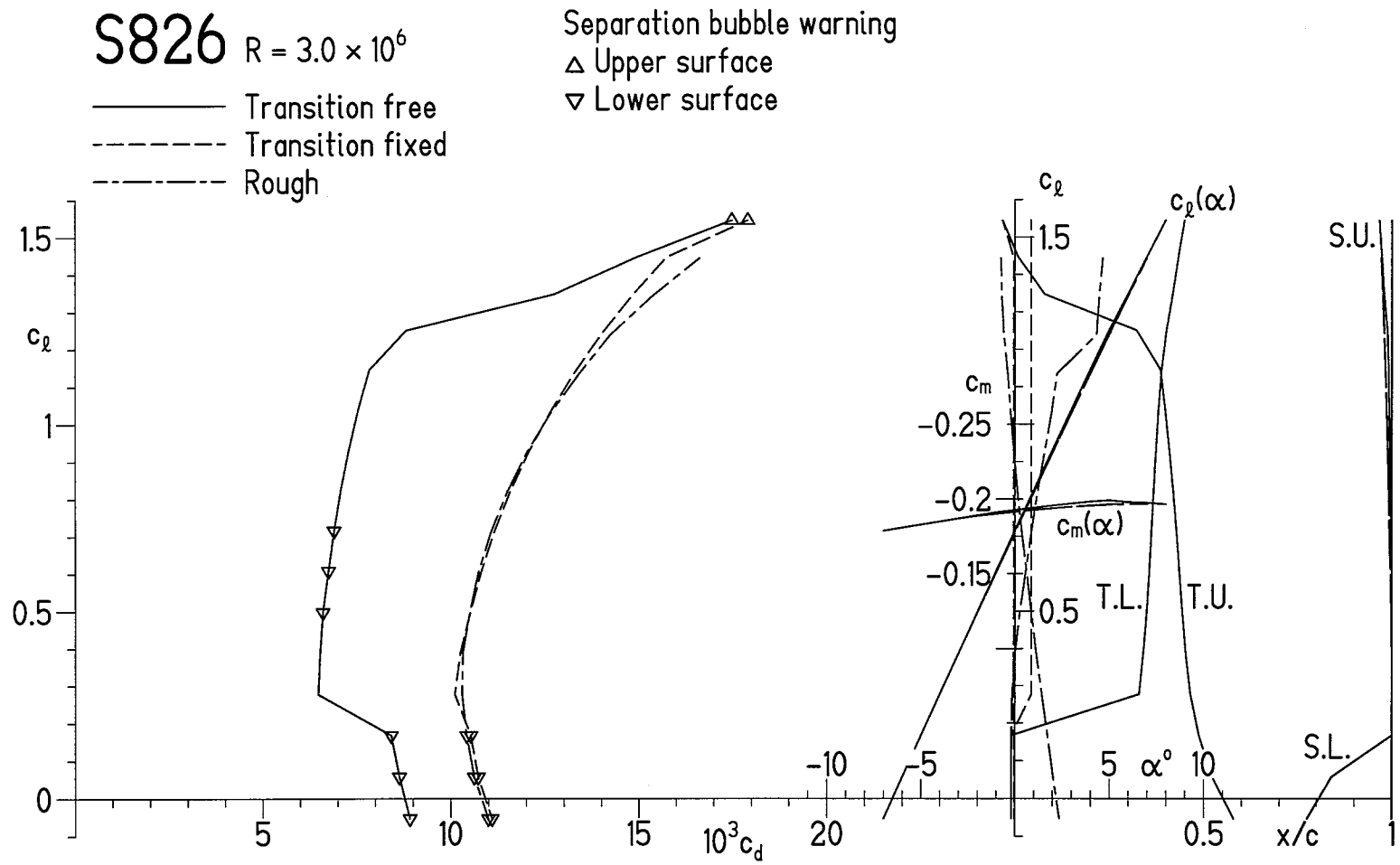
(c) $R = 2.0 \times 10^6$.

Figure 5.- Continued.



(d) $R = 2.5 \times 10^6$.

Figure 5.- Continued.



(e) $R = 3.0 \times 10^6$.

Figure 5.- Concluded.

APPENDIX

PRESSURE DISTRIBUTIONS, TRANSITION AND SEPARATION LOCATIONS, AND
SECTION CHARACTERISTICS

AIRFOIL S825 17%			-7.00	-6.00	-5.00	-4.00	-3.00	-2.00	-1.00	0.00	1.00	
N	X	Y	NUE	CP-DISTR.	FOR THE	ABOVE	ALPHA REL.	CHORD	LINE			
1	1.00000	0.00000	0.00	0.279	0.278	0.279	0.279	0.281	0.282	0.284	0.287	0.289
2	0.99661	0.00108	1.00	0.262	0.260	0.259	0.258	0.258	0.258	0.259	0.260	0.262
3	0.98695	0.00450	2.00	0.180	0.177	0.174	0.172	0.170	0.169	0.168	0.168	0.168
4	0.97208	0.01022	3.00	0.049	0.043	0.038	0.034	0.030	0.027	0.024	0.022	0.021
5	0.95294	0.01758	4.00	-0.105	-0.113	-0.121	-0.128	-0.135	-0.140	-0.146	-0.150	-0.154
6	0.92994	0.02560	5.00	-0.236	-0.248	-0.259	-0.270	-0.279	-0.288	-0.297	-0.304	-0.311
7	0.90294	0.03351	6.00	-0.289	-0.304	-0.318	-0.332	-0.345	-0.357	-0.368	-0.379	-0.388
8	0.87165	0.04117	7.00	-0.283	-0.301	-0.318	-0.334	-0.350	-0.364	-0.379	-0.392	-0.404
9	0.83624	0.04878	8.00	-0.281	-0.302	-0.321	-0.341	-0.359	-0.377	-0.394	-0.410	-0.425
10	0.79720	0.05636	9.00	-0.283	-0.306	-0.329	-0.351	-0.372	-0.393	-0.414	-0.433	-0.452
11	0.75503	0.06385	10.00	-0.287	-0.314	-0.340	-0.365	-0.390	-0.414	-0.438	-0.461	-0.483
12	0.71028	0.07112	11.00	-0.294	-0.325	-0.354	-0.383	-0.412	-0.440	-0.467	-0.494	-0.520
13	0.66350	0.07806	12.00	-0.305	-0.339	-0.372	-0.405	-0.438	-0.470	-0.502	-0.533	-0.563
14	0.61526	0.08450	13.00	-0.317	-0.355	-0.393	-0.431	-0.468	-0.505	-0.541	-0.577	-0.612
15	0.56616	0.09029	14.00	-0.331	-0.374	-0.417	-0.459	-0.502	-0.544	-0.586	-0.627	-0.668
16	0.51676	0.09525	15.00	-0.346	-0.394	-0.443	-0.491	-0.539	-0.587	-0.635	-0.683	-0.730
17	0.46763	0.09920	16.00	-0.361	-0.415	-0.470	-0.525	-0.580	-0.635	-0.690	-0.744	-0.799
18	0.41930	0.10195	17.00	-0.375	-0.436	-0.498	-0.560	-0.623	-0.685	-0.748	-0.811	-0.874
19	0.37230	0.10329	18.00	-0.385	-0.455	-0.525	-0.595	-0.666	-0.738	-0.810	-0.883	-0.956
20	0.32709	0.10296	19.00	-0.391	-0.468	-0.548	-0.628	-0.709	-0.791	-0.874	-0.958	-1.043
21	0.28387	0.10060	20.00	-0.351	-0.436	-0.523	-0.612	-0.703	-0.794	-0.888	-0.982	-1.077
22	0.24253	0.09625	21.00	-0.265	-0.357	-0.450	-0.546	-0.644	-0.744	-0.846	-0.949	-1.054
23	0.20324	0.09032	22.00	-0.172	-0.270	-0.370	-0.474	-0.580	-0.689	-0.801	-0.915	-1.031
24	0.16643	0.08315	23.00	-0.069	-0.173	-0.281	-0.393	-0.509	-0.629	-0.752	-0.878	-1.008
25	0.13251	0.07494	24.00	0.047	-0.064	-0.180	-0.301	-0.428	-0.559	-0.695	-0.836	-0.982
26	0.10185	0.06588	25.00	0.181	0.063	-0.061	-0.193	-0.332	-0.477	-0.629	-0.788	-0.952
27	0.07479	0.05616	26.00	0.339	0.216	0.074	-0.058	-0.210	-0.371	-0.541	-0.721	-0.908
28	0.05161	0.04596	27.00	0.523	0.399	0.262	0.110	-0.054	-0.232	-0.423	-0.627	-0.844
29	0.03250	0.03549	28.00	0.732	0.617	0.483	0.328	0.154	-0.040	-0.253	-0.485	-0.736
30	0.01766	0.02500	29.00	0.931	0.851	0.739	0.598	0.426	0.223	-0.009	-0.271	-0.562
31	0.00721	0.01481	30.00	0.980	1.000	0.969	0.888	0.758	0.578	0.348	0.069	-0.259
32	0.00129	0.00543	31.00	0.314	0.622	0.838	0.964	0.999	0.944	0.797	0.559	0.231
33	0.00028	0.00224	31.38	-0.514	0.029	0.452	0.755	0.938	1.000	0.941	0.762	0.462
34	0.00001	0.00030	31.63	-1.474	-0.692	-0.057	0.430	0.768	0.956	0.996	0.886	0.627
35	0.00014	-0.00143	31.88	-3.011	-1.878	-0.931	-0.171	0.400	0.782	0.975	0.978	0.790
36	0.00081	-0.00307	32.13	-2.625	-1.699	-0.908	-0.253	0.265	0.646	0.890	0.995	0.963
37	0.00197	-0.00477	32.38	-2.350	-1.570	-0.892	-0.317	0.155	0.523	0.787	0.946	1.000
38	0.00650	-0.00920	33.00	-1.921	-1.364	-0.865	-0.424	-0.042	0.281	0.545	0.749	0.893
39	0.01819	-0.01650	34.00	-1.505	-1.137	-0.796	-0.485	-0.202	0.052	0.276	0.470	0.635
40	0.03502	-0.02381	35.00	-1.245	-0.977	-0.725	-0.490	-0.271	-0.068	0.117	0.285	0.436
41	0.05670	-0.03093	36.00	-1.066	-0.860	-0.664	-0.478	-0.302	-0.136	0.019	0.163	0.297
42	0.08297	-0.03780	37.00	-0.932	-0.767	-0.608	-0.456	-0.311	-0.173	-0.042	0.083	0.199
43	0.11351	-0.04443	38.00	-0.830	-0.694	-0.563	-0.436	-0.313	-0.195	-0.082	0.025	0.128
44	0.14790	-0.05114	39.00	-0.748	-0.634	-0.523	-0.415	-0.310	-0.209	-0.110	-0.016	0.075
45	0.18480	-0.05834	40.00	-0.837	-0.731	-0.627	-0.525	-0.426	-0.329	-0.235	-0.143	-0.055
46	0.22231	-0.06499	41.00	-1.087	-0.980	-0.874	-0.769	-0.667	-0.567	-0.469	-0.373	-0.280
47	0.25997	-0.06891	42.00	-1.235	-1.132	-1.030	-0.929	-0.829	-0.731	-0.635	-0.540	-0.448
48	0.29879	-0.06869	43.00	-1.143	-1.053	-0.965	-0.877	-0.790	-0.704	-0.620	-0.536	-0.454
49	0.34011	-0.06415	44.00	-0.857	-0.787	-0.718	-0.649	-0.580	-0.512	-0.444	-0.377	-0.311
50	0.38475	-0.05600	45.00	-0.568	-0.515	-0.462	-0.409	-0.356	-0.303	-0.251	-0.199	-0.147
51	0.43307	-0.04520	46.00	-0.303	-0.263	-0.223	-0.183	-0.143	-0.103	-0.063	-0.023	0.016
52	0.48499	-0.03306	47.00	-0.108	-0.078	-0.047	-0.016	0.015	0.046	0.077	0.108	0.140
53	0.53974	-0.02082	48.00	0.034	0.058	0.082	0.107	0.131	0.156	0.181	0.206	0.231
54	0.59631	-0.00935	49.00	0.142	0.161	0.180	0.200	0.219	0.239	0.260	0.280	0.300
55	0.65355	0.00060	50.00	0.225	0.240	0.255	0.271	0.287	0.304	0.320	0.337	0.354
56	0.71026	0.00854	51.00	0.289	0.301	0.314	0.327	0.340	0.354	0.367	0.381	0.396
57	0.76514	0.01410	52.00	0.340	0.350	0.360	0.371	0.381	0.393	0.404	0.416	0.428
58	0.81692	0.01713	53.00	0.379	0.388	0.396	0.405	0.414	0.423	0.433	0.442	0.452
59	0.86437	0.01757	54.00	0.411	0.417	0.424	0.431	0.438	0.446	0.454	0.462	0.471
60	0.90608	0.01553	55.00	0.421	0.427	0.432	0.438	0.444	0.451	0.458	0.465	0.472
61	0.94062	0.01168	56.00	0.406	0.411	0.415	0.420	0.425	0.431	0.437	0.443	0.450
62	0.96717	0.00727	57.00	0.374	0.377	0.381	0.385	0.389	0.394	0.399	0.404	0.410
63	0.98566	0.00342	58.00	0.333	0.335	0.338	0.341	0.344	0.348	0.352	0.357	0.362
64	0.99646	0.00088	59.00	0.296	0.297	0.299	0.301	0.303	0.306	0.309	0.313	0.317
65	1.00000	0.00000	60.00	0.279	0.278	0.279	0.279	0.281	0.282	0.284	0.287	0.289

ALPHA0= 6.11 DEGREES CMO=-0.1803 ETA= 1.117

AIRFOIL S825 17%			2.00	3.00	4.00	5.00	6.00	7.00	8.00	9.00	10.00	
N	X	Y	NUE	CP-DISTR.	FOR THE	ABOVE	ALPHA	REL.	CHORD	LINE		
1	1.00000	0.00000	0.00	0.293	0.297	0.301	0.305	0.310	0.316	0.321	0.327	0.334
2	0.99661	0.00108	1.00	0.264	0.267	0.270	0.273	0.277	0.281	0.286	0.291	0.296
3	0.98695	0.00450	2.00	0.169	0.170	0.172	0.174	0.177	0.181	0.184	0.189	0.193
4	0.97208	0.01022	3.00	0.020	0.020	0.020	0.021	0.023	0.025	0.027	0.031	0.035
5	0.95294	0.01758	4.00	-0.157	-0.159	-0.161	-0.162	-0.162	-0.162	-0.161	-0.159	-0.156
6	0.92994	0.02560	5.00	-0.317	-0.322	-0.326	-0.330	-0.333	-0.335	-0.336	-0.336	-0.336
7	0.90294	0.03351	6.00	-0.397	-0.405	-0.413	-0.419	-0.424	-0.429	-0.433	-0.436	-0.438
8	0.87165	0.04117	7.00	-0.416	-0.427	-0.437	-0.446	-0.455	-0.462	-0.469	-0.475	-0.479
9	0.83624	0.04878	8.00	-0.440	-0.454	-0.467	-0.479	-0.491	-0.501	-0.511	-0.520	-0.528
10	0.79720	0.05636	9.00	-0.470	-0.487	-0.503	-0.519	-0.533	-0.547	-0.560	-0.572	-0.583
11	0.75503	0.06385	10.00	-0.505	-0.525	-0.545	-0.564	-0.583	-0.600	-0.617	-0.632	-0.647
12	0.71028	0.07112	11.00	-0.546	-0.570	-0.594	-0.617	-0.640	-0.661	-0.682	-0.701	-0.720
13	0.66350	0.07806	12.00	-0.593	-0.622	-0.651	-0.678	-0.705	-0.731	-0.756	-0.780	-0.803
14	0.61526	0.08450	13.00	-0.647	-0.681	-0.715	-0.747	-0.779	-0.810	-0.840	-0.870	-0.898
15	0.56616	0.09029	14.00	-0.708	-0.748	-0.787	-0.826	-0.863	-0.900	-0.937	-0.972	-1.006
16	0.51676	0.09525	15.00	-0.777	-0.823	-0.869	-0.914	-0.959	-1.002	-1.046	-1.088	-1.129
17	0.46763	0.09920	16.00	-0.853	-0.907	-0.960	-1.013	-1.066	-1.118	-1.169	-1.219	-1.269
18	0.41930	0.10195	17.00	-0.937	-1.000	-1.062	-1.125	-1.186	-1.248	-1.308	-1.368	-1.428
19	0.37230	0.10329	18.00	-1.029	-1.102	-1.175	-1.248	-1.321	-1.393	-1.465	-1.537	-1.608
20	0.32709	0.10296	19.00	-1.127	-1.213	-1.298	-1.384	-1.470	-1.556	-1.642	-1.727	-1.812
21	0.28387	0.10060	20.00	-1.173	-1.270	-1.368	-1.467	-1.566	-1.665	-1.764	-1.864	-1.963
22	0.24253	0.09625	21.00	-1.161	-1.269	-1.378	-1.488	-1.599	-1.711	-1.824	-1.937	-2.051
23	0.20324	0.09032	22.00	-1.150	-1.271	-1.393	-1.517	-1.643	-1.770	-1.898	-2.028	-2.158
24	0.16643	0.08315	23.00	-1.141	-1.276	-1.414	-1.555	-1.699	-1.844	-1.992	-2.141	-2.292
25	0.13251	0.07494	24.00	-1.132	-1.285	-1.443	-1.605	-1.769	-1.938	-2.109	-2.284	-2.461
26	0.10185	0.06588	25.00	-1.123	-1.299	-1.482	-1.669	-1.862	-2.059	-2.261	-2.468	-2.679
27	0.07479	0.05616	26.00	-1.105	-1.310	-1.522	-1.743	-1.971	-2.206	-2.448	-2.697	-2.952
28	0.05161	0.04596	27.00	-1.073	-1.314	-1.567	-1.831	-2.106	-2.392	-2.689	-2.996	-3.312
29	0.03250	0.03549	28.00	-1.006	-1.293	-1.598	-1.921	-2.260	-2.616	-2.989	-3.377	-3.780
30	0.01766	0.02500	29.00	-0.882	-1.230	-1.607	-2.011	-2.443	-2.901	-3.385	-3.895	-4.430
31	0.00721	0.01481	30.00	-0.635	-1.059	-1.531	-2.050	-2.615	-3.225	-3.881	-4.580	-5.323
32	0.00129	0.00543	31.00	-0.187	-0.694	-1.290	-1.975	-2.747	-3.605	-4.548	-5.576	-6.687
33	0.00028	0.00224	31.38	0.042	-0.497	-1.155	-1.931	-2.825	-3.834	-4.959	-6.196	-7.546
34	0.00001	0.00030	31.63	0.218	-0.339	-1.043	-1.895	-2.892	-4.034	-5.320	-6.747	-8.314
35	0.00014	-0.00143	31.88	0.414	-0.152	-0.907	-1.849	-2.977	-4.291	-5.788	-7.466	-9.324
36	0.00081	-0.00307	32.13	0.792	0.483	0.037	-0.546	-1.265	-2.120	-3.109	-4.231	-5.485
37	0.00197	-0.00477	32.38	0.949	0.793	0.532	0.167	-0.302	-0.875	-1.550	-2.327	-3.205
38	0.00650	-0.00920	33.00	0.976	1.000	0.963	0.865	0.708	0.490	0.213	-0.124	-0.520
39	0.01819	-0.01650	34.00	0.769	0.872	0.945	0.988	1.000	0.981	0.931	0.851	0.741
40	0.03502	-0.02381	35.00	0.569	0.685	0.783	0.862	0.924	0.968	0.993	1.000	0.989
41	0.05670	-0.03093	36.00	0.419	0.529	0.629	0.717	0.793	0.857	0.909	0.950	0.979
42	0.08297	-0.03780	37.00	0.309	0.410	0.504	0.590	0.668	0.738	0.800	0.854	0.899
43	0.11351	-0.04443	38.00	0.226	0.318	0.405	0.486	0.562	0.632	0.695	0.753	0.806
44	0.14790	-0.05114	39.00	0.163	0.246	0.326	0.401	0.473	0.540	0.603	0.661	0.715
45	0.18480	-0.05834	40.00	0.031	0.114	0.193	0.269	0.342	0.412	0.478	0.540	0.598
46	0.22231	-0.06499	41.00	-0.189	-0.101	-0.016	0.067	0.147	0.223	0.296	0.367	0.433
47	0.25997	-0.06891	42.00	-0.357	-0.269	-0.183	-0.099	-0.017	0.062	0.138	0.211	0.282
48	0.29879	-0.06869	43.00	-0.373	-0.294	-0.216	-0.140	-0.066	0.007	0.077	0.146	0.212
49	0.34011	-0.06415	44.00	-0.246	-0.182	-0.119	-0.056	0.005	0.064	0.123	0.180	0.236
50	0.38475	-0.05600	45.00	-0.096	-0.045	0.005	0.054	0.103	0.151	0.198	0.245	0.290
51	0.43307	-0.04520	46.00	0.056	0.095	0.134	0.173	0.211	0.249	0.286	0.323	0.359
52	0.48499	-0.03306	47.00	0.171	0.202	0.233	0.264	0.294	0.325	0.355	0.385	0.414
53	0.53974	-0.02082	48.00	0.256	0.281	0.307	0.332	0.357	0.382	0.407	0.431	0.456
54	0.59631	-0.00935	49.00	0.321	0.342	0.363	0.383	0.404	0.425	0.446	0.467	0.488
55	0.65355	0.00060	50.00	0.371	0.388	0.406	0.423	0.441	0.459	0.476	0.494	0.512
56	0.71026	0.00854	51.00	0.410	0.424	0.439	0.454	0.469	0.484	0.499	0.515	0.530
57	0.76514	0.01410	52.00	0.440	0.452	0.465	0.478	0.490	0.504	0.517	0.530	0.543
58	0.81692	0.01713	53.00	0.463	0.473	0.484	0.495	0.506	0.518	0.529	0.541	0.552
59	0.86437	0.01757	54.00	0.480	0.489	0.498	0.507	0.517	0.527	0.537	0.547	0.558
60	0.90608	0.01553	55.00	0.480	0.487	0.496	0.504	0.513	0.521	0.530	0.540	0.549
61	0.94062	0.01168	56.00	0.456	0.463	0.471	0.478	0.486	0.494	0.503	0.511	0.520
62	0.96717	0.00727	57.00	0.416	0.423	0.430	0.437	0.444	0.452	0.460	0.468	0.476
63	0.98566	0.00342	58.00	0.367	0.373	0.379	0.386	0.392	0.400	0.407	0.415	0.423
64	0.99646	0.00088	59.00	0.322	0.326	0.332	0.337	0.343	0.350	0.356	0.364	0.371
65	1.00000	0.00000	60.00	0.293	0.297	0.301	0.305	0.310	0.316	0.321	0.327	0.334

ALPHA0= 6.11 DEGREES CM0=-0.1803 ETA= 1.117

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA (DEG.)	R= 1000000 MU=3.0	R= 1000000 MU=1.3	R= 1000000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.0801 0.0369 0.0021 LOWER 1.0055 0.4907 0.0080* TOTAL CL=-0.127 CD=0.01012 CM=-0.1740	S TURB S SEP CD 1.0043 0.0000 0.0061 1.0055 0.4907 0.0080* CL=-0.097 CD=0.01409 CM=-0.1764	S TURB S SEP CD 0.7282 0.0000 0.0055 1.0191 0.4924 0.0082* CL=-0.097 CD=0.01367 CM=-0.1764
-6.00	S TURB S SEP CD UPPER 0.0845 0.0366 0.0022 LOWER 0.6984 0.3624 0.0039 TOTAL CL=-0.018 CD=0.00611 CM=-0.1752	S TURB S SEP CD 1.0043 0.0012 0.0065 0.9635 0.4650 0.0066 CL= 0.012 CD=0.01318 CM=-0.1787	S TURB S SEP CD 0.7815 0.0011 0.0061 1.0117 0.4739 0.0071 CL= 0.012 CD=0.01319 CM=-0.1787
-5.00	S TURB S SEP CD UPPER 0.0902 0.0357 0.0024 LOWER 0.6968 0.2847 0.0036* TOTAL CL= 0.090 CD=0.00595 CM=-0.1766	S TURB S SEP CD 1.0043 0.0039 0.0070 0.9635 0.4451 0.0060 CL= 0.119 CD=0.01298 CM=-0.1808	S TURB S SEP CD 0.8128 0.0038 0.0066 0.9976 0.4520 0.0062 CL= 0.119 CD=0.01280 CM=-0.1808
-4.00	S TURB S SEP CD UPPER 0.3426 0.0041 0.0038 LOWER 0.6951 0.1793 0.0033* TOTAL CL= 0.229 CD=0.00716 CM=-0.1827	S TURB S SEP CD 1.0043 0.0057 0.0075 0.9635 0.4204 0.0054 CL= 0.227 CD=0.01289 CM=-0.1829	S TURB S SEP CD 0.8358 0.0055 0.0071 0.9776 0.4237 0.0055 CL= 0.227 CD=0.01254 CM=-0.1829
-3.00	S TURB S SEP CD UPPER 0.4506 0.0054 0.0047 LOWER 0.6932 0.0000 0.0032* TOTAL CL= 0.337 CD=0.00787 CM=-0.1844	S TURB S SEP CD 1.0043 0.0074 0.0081 0.9635 0.3932 0.0049 CL= 0.335 CD=0.01295 CM=-0.1849	S TURB S SEP CD 0.8603 0.0072 0.0077 0.9561 0.3910 0.0048 CL= 0.335 CD=0.01250 CM=-0.1849
-2.00	S TURB S SEP CD UPPER 0.5185 0.0069 0.0054 LOWER 0.6913 0.0000 0.0030* TOTAL CL= 0.445 CD=0.00839 CM=-0.1862	S TURB S SEP CD 1.0043 0.0092 0.0087 0.9635 0.3529 0.0044 CL= 0.443 CD=0.01307 CM=-0.1868	S TURB S SEP CD 0.8876 0.0089 0.0083 0.9303 0.3406 0.0043 CL= 0.443 CD=0.01257 CM=-0.1868
-1.00	S TURB S SEP CD UPPER 0.5684 0.0083 0.0061 LOWER 0.6893 0.0000 0.0028* TOTAL CL= 0.553 CD=0.00887 CM=-0.1879	S TURB S SEP CD 1.0043 0.0110 0.0093 0.9635 0.2963 0.0040 CL= 0.550 CD=0.01330 CM=-0.1885	S TURB S SEP CD 0.9085 0.0107 0.0090 0.9033 0.2647 0.0038 CL= 0.551 CD=0.01276 CM=-0.1884
0.00	S TURB S SEP CD UPPER 0.6042 0.0098 0.0067 LOWER 0.6871 0.0000 0.0026* TOTAL CL= 0.661 CD=0.00930 CM=-0.1896	S TURB S SEP CD 1.0043 0.0131 0.0101 0.9635 0.2059 0.0036 CL= 0.657 CD=0.01365 CM=-0.1898	S TURB S SEP CD 0.9312 0.0128 0.0097 0.8835 0.0000 0.0035 CL= 0.658 CD=0.01319 CM=-0.1887
1.00	S TURB S SEP CD UPPER 0.6293 0.0114 0.0072 LOWER 0.6848 0.0000 0.0025* TOTAL CL= 0.769 CD=0.00970 CM=-0.1911	S TURB S SEP CD 1.0043 0.0154 0.0108 0.9635 0.0000 0.0033 CL= 0.764 CD=0.01416 CM=-0.1900	S TURB S SEP CD 0.9521 0.0150 0.0105 0.7428 0.0000 0.0028 CL= 0.764 CD=0.01331 CM=-0.1901
2.00	S TURB S SEP CD UPPER 0.6461 0.0131 0.0078 LOWER 0.6821 0.0000 0.0023* TOTAL CL= 0.876 CD=0.01008 CM=-0.1926	S TURB S SEP CD 1.0043 0.0178 0.0117 0.9635 0.0000 0.0031 CL= 0.870 CD=0.01474 CM=-0.1911	S TURB S SEP CD 0.9689 0.0175 0.0114 0.7402 0.0000 0.0026 CL= 0.870 CD=0.01402 CM=-0.1912
3.00	S TURB S SEP CD UPPER 0.6574 0.0148 0.0083 LOWER 0.6790 0.0000 0.0022* TOTAL CL= 0.983 CD=0.01044 CM=-0.1939	S TURB S SEP CD 1.0043 0.0205 0.0126 0.9635 0.0000 0.0028 CL= 0.975 CD=0.01543 CM=-0.1921	S TURB S SEP CD 0.9865 0.0203 0.0125 0.7368 0.0000 0.0024 CL= 0.975 CD=0.01487 CM=-0.1922
4.00	S TURB S SEP CD UPPER 0.6674 0.0166 0.0088 LOWER 0.6749 0.0000 0.0020* TOTAL CL= 1.089 CD=0.01083 CM=-0.1951	S TURB S SEP CD 1.0043 0.0235 0.0136 0.9635 0.0000 0.0026 CL= 1.080 CD=0.01622 CM=-0.1929	S TURB S SEP CD 1.0015 0.0235 0.0136 0.7325 0.0000 0.0022 CL= 1.080 CD=0.01585 CM=-0.1929
5.00	S TURB S SEP CD UPPER 0.6783 0.0186 0.0094 LOWER 0.6688 0.0000 0.0019* TOTAL CL= 1.196 CD=0.01129 CM=-0.1962	S TURB S SEP CD 1.0043 0.0269 0.0148 0.9635 0.0000 0.0024 CL= 1.184 CD=0.01714 CM=-0.1934	S TURB S SEP CD 1.0136 0.0271 0.0149 0.7274 0.0000 0.0021 CL= 1.183 CD=0.01699 CM=-0.1933
6.00	S TURB S SEP CD UPPER 0.6929 0.0208 0.0101 LOWER 0.6603 0.0000 0.0017* TOTAL CL= 1.301 CD=0.01186 CM=-0.1971	S TURB S SEP CD 1.0043 0.0307 0.0160 0.9635 0.0000 0.0022 CL= 1.286 CD=0.01818 CM=-0.1936	S TURB S SEP CD 1.0228 0.0314 0.0164 0.7220 0.0000 0.0019 CL= 1.285 CD=0.01831 CM=-0.1934
7.00	S TURB S SEP CD UPPER 0.7121 0.0235 0.0110 LOWER 0.6517 0.0000 0.0016* TOTAL CL= 1.406 CD=0.01261 CM=-0.1977	S TURB S SEP CD 1.0043 0.0350 0.0174 0.9564 0.0000 0.0020 CL= 1.388 CD=0.01938 CM=-0.1936	S TURB S SEP CD 1.0316 0.0364 0.0181 0.7171 0.0000 0.0018 CL= 1.386 CD=0.01992 CM=-0.1931

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEC.)	R= 1000000 MU=3.0	R= 1000000 MU=1.3	R= 1000000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0070 0.0400 0.0190*	1.0070 0.0400 0.0190*	1.0363 0.0422 0.0200
	LOWER 0.6431 0.0000 0.0015*	0.9564 0.0000 0.0018	0.7128 0.0000 0.0017
	TOTAL CL= 1.488 CD=0.02046	CL= 1.488 CD=0.02081	CL= 1.484 CD=0.02171
	CM=-0.1931	CM=-0.1931	CM=-0.1923
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0277 0.0480 0.0217*	1.0277 0.0480 0.0217*	1.0385 0.0494 0.0222*
	LOWER 0.6337 0.0000 0.0014*	0.9564 0.0000 0.0017	0.7090 0.0000 0.0015
	TOTAL CL= 1.582 CD=0.02303	CL= 1.582 CD=0.02335	CL= 1.580 CD=0.02374
	CM=-0.1914	CM=-0.1914	CM=-0.1910
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0363 0.0580 0.0244*	1.0363 0.0580 0.0244*	1.0388 0.0586 0.0246*
	LOWER 0.6225 0.0000 0.0013*	0.9293 0.0000 0.0016	0.7055 0.0000 0.0014
	TOTAL CL= 1.672 CD=0.02572	CL= 1.672 CD=0.02600	CL= 1.671 CD=0.02605
	CM=-0.1889	CM=-0.1889	CM=-0.1887

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA (DEG.)	R= 1500000 MU=3.0	R= 1500000 MU=1.3	R= 1500000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.0840 0.0263 0.0017 LOWER 1.0055 0.4765 0.0075* TOTAL CL=-0.118 CD=0.00924 CM=-0.1746	S TURB S SEP CD 1.0043 0.0000 0.0057 1.0055 0.4765 0.0075* CL=-0.097 CD=0.01314 CM=-0.1764	S TURB S SEP CD 0.8151 0.0000 0.0054 1.0203 0.4790 0.0077* CL=-0.097 CD=0.01307 CM=-0.1764
-6.00	S TURB S SEP CD UPPER 0.0890 0.0256 0.0019 LOWER 0.7007 0.2120 0.0035 TOTAL CL=-0.009 CD=0.00537 CM=-0.1752	S TURB S SEP CD 1.0043 0.0000 0.0060 0.9635 0.4469 0.0062 CL= 0.013 CD=0.01222 CM=-0.1788	S TURB S SEP CD 0.8361 0.0000 0.0058 1.0151 0.4587 0.0067 CL= 0.013 CD=0.01247 CM=-0.1788
-5.00	S TURB S SEP CD UPPER 0.3221 0.0000 0.0031 LOWER 0.6984 0.0000 0.0033* TOTAL CL= 0.123 CD=0.00643 CM=-0.1811	S TURB S SEP CD 1.0043 0.0001 0.0065 0.9635 0.4245 0.0056 CL= 0.122 CD=0.01209 CM=-0.1811	S TURB S SEP CD 0.8590 0.0000 0.0063 1.0045 0.4348 0.0059 CL= 0.123 CD=0.01213 CM=-0.1811
-4.00	S TURB S SEP CD UPPER 0.4379 0.0007 0.0040 LOWER 0.6961 0.0000 0.0031* TOTAL CL= 0.232 CD=0.00709 CM=-0.1833	S TURB S SEP CD 1.0043 0.0027 0.0070 0.9635 0.4002 0.0051 CL= 0.230 CD=0.01206 CM=-0.1831	S TURB S SEP CD 0.8816 0.0026 0.0067 0.9887 0.4042 0.0052 CL= 0.230 CD=0.01191 CM=-0.1832
-3.00	S TURB S SEP CD UPPER 0.5094 0.0031 0.0047 LOWER 0.6937 0.0000 0.0029* TOTAL CL= 0.339 CD=0.00755 CM=-0.1850	S TURB S SEP CD 1.0043 0.0049 0.0075 0.9635 0.3659 0.0046 CL= 0.338 CD=0.01209 CM=-0.1851	S TURB S SEP CD 0.9002 0.0047 0.0073 0.9701 0.3681 0.0046 CL= 0.338 CD=0.01186 CM=-0.1852
-2.00	S TURB S SEP CD UPPER 0.5615 0.0048 0.0053 LOWER 0.6913 0.0000 0.0027* TOTAL CL= 0.447 CD=0.00797 CM=-0.1867	S TURB S SEP CD 1.0043 0.0067 0.0081 0.9635 0.3194 0.0041 CL= 0.445 CD=0.01221 CM=-0.1870	S TURB S SEP CD 0.9190 0.0065 0.0078 0.9503 0.3135 0.0041 CL= 0.446 CD=0.01191 CM=-0.1870
-1.00	S TURB S SEP CD UPPER 0.6000 0.0063 0.0058 LOWER 0.6893 0.0000 0.0026* TOTAL CL= 0.555 CD=0.00835 CM=-0.1885	S TURB S SEP CD 1.0043 0.0086 0.0087 0.9635 0.2519 0.0037 CL= 0.553 CD=0.01242 CM=-0.1887	S TURB S SEP CD 0.9377 0.0084 0.0085 0.9284 0.2297 0.0036 CL= 0.553 CD=0.01210 CM=-0.1887
0.00	S TURB S SEP CD UPPER 0.6269 0.0078 0.0063 LOWER 0.6871 0.0000 0.0024* TOTAL CL= 0.663 CD=0.00871 CM=-0.1901	S TURB S SEP CD 1.0043 0.0106 0.0094 0.9635 0.0000 0.0034 CL= 0.660 CD=0.01278 CM=-0.1894	S TURB S SEP CD 0.9548 0.0104 0.0091 0.9071 0.0000 0.0033 CL= 0.660 CD=0.01246 CM=-0.1894
1.00	S TURB S SEP CD UPPER 0.6451 0.0094 0.0068 LOWER 0.6848 0.0000 0.0023* TOTAL CL= 0.771 CD=0.00903 CM=-0.1917	S TURB S SEP CD 1.0043 0.0128 0.0101 0.9635 0.0000 0.0031 CL= 0.767 CD=0.01322 CM=-0.1907	S TURB S SEP CD 0.9698 0.0126 0.0099 0.8884 0.0000 0.0030 CL= 0.767 CD=0.01291 CM=-0.1908
2.00	S TURB S SEP CD UPPER 0.6563 0.0109 0.0072 LOWER 0.6821 0.0000 0.0021* TOTAL CL= 0.879 CD=0.00933 CM=-0.1932	S TURB S SEP CD 1.0043 0.0152 0.0109 0.9635 0.0000 0.0029 CL= 0.873 CD=0.01375 CM=-0.1919	S TURB S SEP CD 0.9851 0.0151 0.0107 0.7490 0.0000 0.0024 CL= 0.873 CD=0.01316 CM=-0.1920
3.00	S TURB S SEP CD UPPER 0.6662 0.0125 0.0077 LOWER 0.6790 0.0000 0.0020* TOTAL CL= 0.986 CD=0.00965 CM=-0.1946	S TURB S SEP CD 1.0043 0.0182 0.0118 0.9635 0.0000 0.0027 CL= 0.978 CD=0.01446 CM=-0.1928	S TURB S SEP CD 0.9987 0.0182 0.0118 0.7471 0.0000 0.0023 CL= 0.978 CD=0.01403 CM=-0.1928
4.00	S TURB S SEP CD UPPER 0.6762 0.0143 0.0082 LOWER 0.6749 0.0000 0.0019* TOTAL CL= 1.093 CD=0.01001 CM=-0.1959	S TURB S SEP CD 1.0043 0.0211 0.0127 0.9635 0.0000 0.0024 CL= 1.083 CD=0.01519 CM=-0.1936	S TURB S SEP CD 1.0094 0.0212 0.0128 0.7445 0.0000 0.0021 CL= 1.083 CD=0.01493 CM=-0.1936
5.00	S TURB S SEP CD UPPER 0.6889 0.0163 0.0087 LOWER 0.6688 0.0000 0.0017* TOTAL CL= 1.199 CD=0.01045 CM=-0.1970	S TURB S SEP CD 1.0043 0.0243 0.0138 0.9635 0.0000 0.0022 CL= 1.187 CD=0.01603 CM=-0.1942	S TURB S SEP CD 1.0195 0.0247 0.0140 0.7410 0.0000 0.0020 CL= 1.187 CD=0.01599 CM=-0.1941
6.00	S TURB S SEP CD UPPER 0.7045 0.0184 0.0094 LOWER 0.6603 0.0000 0.0016* TOTAL CL= 1.305 CD=0.01100 CM=-0.1979	S TURB S SEP CD 1.0043 0.0279 0.0149 0.9635 0.0000 0.0021 CL= 1.291 CD=0.01697 CM=-0.1946	S TURB S SEP CD 1.0283 0.0288 0.0154 0.7363 0.0000 0.0018 CL= 1.289 CD=0.01724 CM=-0.1943
7.00	S TURB S SEP CD UPPER 0.9012 0.0269 0.0136 LOWER 0.6517 0.0000 0.0015* TOTAL CL= 1.401 CD=0.01505 CM=-0.1964	S TURB S SEP CD 1.0043 0.0320 0.0161 0.9564 0.0000 0.0019 CL= 1.393 CD=0.01804 CM=-0.1946	S TURB S SEP CD 1.0351 0.0336 0.0170 0.7306 0.0000 0.0017 CL= 1.390 CD=0.01870 CM=-0.1941

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 1500000 MU=3.0	R= 1500000 MU=1.3	R= 1500000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0070 0.0368 0.0176	1.0070 0.0368 0.0176	1.0379 0.0391 0.0188
	LOWER 0.6431 0.0000 0.0014*	0.9564 0.0000 0.0017	0.7246 0.0000 0.0016
	TOTAL CL= 1.493 CD=0.01899	CL= 1.493 CD=0.01936	CL= 1.489 CD=0.02036
	CM=-0.1943	CM=-0.1943	CM=-0.1934
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0277 0.0442 0.0201*	1.0277 0.0442 0.0201*	1.0388 0.0456 0.0208*
	LOWER 0.6337 0.0000 0.0013*	0.9564 0.0000 0.0016	0.7193 0.0000 0.0015
	TOTAL CL= 1.589 CD=0.02142	CL= 1.589 CD=0.02175	CL= 1.586 CD=0.02221
	CM=-0.1928	CM=-0.1928	CM=-0.1923
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0363 0.0534 0.0228*	1.0363 0.0534 0.0228*	1.0390 0.0539 0.0230*
	LOWER 0.6225 0.0000 0.0012*	0.9293 0.0000 0.0015	0.7148 0.0000 0.0014
	TOTAL CL= 1.680 CD=0.02394	CL= 1.680 CD=0.02424	CL= 1.679 CD=0.02432
	CM=-0.1906	CM=-0.1906	CM=-0.1903

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA (DEG.)	R= 2000000 MU=3.0	R= 2000000 MU=1.3	R= 2000000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.0873 0.0180 0.0015* LOWER 1.0055 0.4654 0.0071* TOTAL CL=-0.112 CD=0.00867 CM=-0.1751	S TURB S SEP CD 1.0043 0.0000 0.0054 1.0055 0.4654 0.0071* CL=-0.097 CD=0.01257 CM=-0.1764	S TURB S SEP CD 0.8461 0.0000 0.0052 1.0205 0.4687 0.0074* CL=-0.097 CD=0.01261 CM=-0.1764
-6.00	S TURB S SEP CD UPPER 0.0931 0.0172 0.0016 LOWER 0.7027 0.0000 0.0033 TOTAL CL=-0.002 CD=0.00496 CM=-0.1752	S TURB S SEP CD 1.0043 0.0000 0.0058 0.9635 0.4329 0.0059 CL= 0.013 CD=0.01166 CM=-0.1788	S TURB S SEP CD 0.8667 0.0000 0.0056 1.0167 0.4468 0.0064 CL= 0.013 CD=0.01201 CM=-0.1788
-5.00	S TURB S SEP CD UPPER 0.4112 0.0000 0.0034 LOWER 0.7004 0.0000 0.0031* TOTAL CL= 0.123 CD=0.00651 CM=-0.1811	S TURB S SEP CD 1.0043 0.0000 0.0062 0.9635 0.4087 0.0053 CL= 0.123 CD=0.01150 CM=-0.1811	S TURB S SEP CD 0.8859 0.0000 0.0060 1.0081 0.4213 0.0056 CL= 0.123 CD=0.01164 CM=-0.1811
-4.00	S TURB S SEP CD UPPER 0.4887 0.0000 0.0040 LOWER 0.6980 0.0000 0.0029* TOTAL CL= 0.233 CD=0.00695 CM=-0.1834	S TURB S SEP CD 1.0043 0.0004 0.0067 0.9635 0.3820 0.0048 CL= 0.232 CD=0.01152 CM=-0.1834	S TURB S SEP CD 0.9045 0.0003 0.0065 0.9946 0.3887 0.0050 CL= 0.232 CD=0.01147 CM=-0.1834
-3.00	S TURB S SEP CD UPPER 0.5462 0.0009 0.0046 LOWER 0.6956 0.0000 0.0027* TOTAL CL= 0.342 CD=0.00736 CM=-0.1855	S TURB S SEP CD 1.0043 0.0030 0.0072 0.9635 0.3442 0.0044 CL= 0.339 CD=0.01155 CM=-0.1853	S TURB S SEP CD 0.9207 0.0029 0.0070 0.9790 0.3497 0.0044 CL= 0.340 CD=0.01143 CM=-0.1854
-2.00	S TURB S SEP CD UPPER 0.5891 0.0032 0.0051 LOWER 0.6932 0.0000 0.0026* TOTAL CL= 0.449 CD=0.00771 CM=-0.1872	S TURB S SEP CD 1.0043 0.0051 0.0077 0.9635 0.2922 0.0039 CL= 0.447 CD=0.01167 CM=-0.1872	S TURB S SEP CD 0.9378 0.0050 0.0075 0.9617 0.2915 0.0039 CL= 0.447 CD=0.01148 CM=-0.1872
-1.00	S TURB S SEP CD UPPER 0.6201 0.0048 0.0056 LOWER 0.6907 0.0000 0.0024* TOTAL CL= 0.557 CD=0.00803 CM=-0.1889	S TURB S SEP CD 1.0043 0.0071 0.0083 0.9635 0.2144 0.0036 CL= 0.555 CD=0.01188 CM=-0.1889	S TURB S SEP CD 0.9524 0.0069 0.0081 0.9440 0.1999 0.0035 CL= 0.555 CD=0.01166 CM=-0.1889
0.00	S TURB S SEP CD UPPER 0.6412 0.0064 0.0061 LOWER 0.6881 0.0000 0.0023* TOTAL CL= 0.665 CD=0.00833 CM=-0.1906	S TURB S SEP CD 1.0043 0.0091 0.0089 0.9635 0.0000 0.0033 CL= 0.662 CD=0.01223 CM=-0.1898	S TURB S SEP CD 0.9676 0.0089 0.0088 0.9246 0.0000 0.0032 CL= 0.662 CD=0.01201 CM=-0.1898
1.00	S TURB S SEP CD UPPER 0.6537 0.0079 0.0065 LOWER 0.6853 0.0000 0.0021* TOTAL CL= 0.773 CD=0.00859 CM=-0.1922	S TURB S SEP CD 1.0043 0.0112 0.0096 0.9635 0.0000 0.0030 CL= 0.769 CD=0.01264 CM=-0.1912	S TURB S SEP CD 0.9804 0.0111 0.0095 0.9039 0.0000 0.0029 CL= 0.769 CD=0.01243 CM=-0.1912
2.00	S TURB S SEP CD UPPER 0.6634 0.0094 0.0069 LOWER 0.6821 0.0000 0.0020* TOTAL CL= 0.881 CD=0.00885 CM=-0.1937	S TURB S SEP CD 1.0043 0.0136 0.0104 0.9635 0.0000 0.0028 CL= 0.875 CD=0.01315 CM=-0.1924	S TURB S SEP CD 0.9937 0.0135 0.0103 0.8886 0.0000 0.0027 CL= 0.875 CD=0.01299 CM=-0.1924
3.00	S TURB S SEP CD UPPER 0.6730 0.0110 0.0073 LOWER 0.6790 0.0000 0.0019* TOTAL CL= 0.988 CD=0.00915 CM=-0.1951	S TURB S SEP CD 1.0043 0.0162 0.0112 0.9635 0.0000 0.0026 CL= 0.981 CD=0.01373 CM=-0.1935	S TURB S SEP CD 1.0055 0.0162 0.0112 0.7527 0.0000 0.0022 CL= 0.981 CD=0.01337 CM=-0.1935
4.00	S TURB S SEP CD UPPER 0.6839 0.0127 0.0078 LOWER 0.6749 0.0000 0.0018* TOTAL CL= 1.095 CD=0.00951 CM=-0.1964	S TURB S SEP CD 1.0043 0.0190 0.0121 0.9635 0.0000 0.0023 CL= 1.086 CD=0.01441 CM=-0.1943	S TURB S SEP CD 1.0148 0.0192 0.0122 0.7506 0.0000 0.0020 CL= 1.086 CD=0.01422 CM=-0.1943
5.00	S TURB S SEP CD UPPER 0.6976 0.0146 0.0083 LOWER 0.6688 0.0000 0.0016* TOTAL CL= 1.201 CD=0.00994 CM=-0.1975	S TURB S SEP CD 1.0043 0.0221 0.0130 0.9635 0.0000 0.0022 CL= 1.190 CD=0.01519 CM=-0.1950	S TURB S SEP CD 1.0229 0.0230 0.0134 0.7486 0.0000 0.0019 CL= 1.189 CD=0.01532 CM=-0.1947
6.00	S TURB S SEP CD UPPER 0.7144 0.0168 0.0090 LOWER 0.6603 0.0000 0.0015* TOTAL CL= 1.307 CD=0.01048 CM=-0.1985	S TURB S SEP CD 1.0043 0.0260 0.0142 0.9635 0.0000 0.0020 CL= 1.293 CD=0.01618 CM=-0.1953	S TURB S SEP CD 1.0318 0.0270 0.0148 0.7458 0.0000 0.0018 CL= 1.292 CD=0.01653 CM=-0.1949
7.00	S TURB S SEP CD UPPER 0.9394 0.0264 0.0136 LOWER 0.6517 0.0000 0.0014* TOTAL CL= 1.401 CD=0.01505 CM=-0.1966	S TURB S SEP CD 1.0043 0.0299 0.0153 0.9564 0.0000 0.0018 CL= 1.396 CD=0.01718 CM=-0.1954	S TURB S SEP CD 1.0365 0.0316 0.0163 0.7417 0.0000 0.0016 CL= 1.393 CD=0.01790 CM=-0.1948

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 2000000 MU=3.0	R= 2000000 MU=1.3	R= 2000000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0070 0.0344 0.0167	1.0070 0.0344 0.0167	1.0386 0.0369 0.0179
	LOWER 0.6431 0.0000 0.0013*	0.9564 0.0000 0.0017	0.7360 0.0000 0.0015
	TOTAL CL= 1.497 CD=0.01801	CL= 1.497 CD=0.01839	CL= 1.493 CD=0.01946
	CM=-0.1951	CM=-0.1951	CM=-0.1942
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0277 0.0416 0.0192*	1.0277 0.0416 0.0192*	1.0389 0.0431 0.0198
	LOWER 0.6337 0.0000 0.0012	0.9564 0.0000 0.0015	0.7294 0.0000 0.0014
	TOTAL CL= 1.593 CD=0.02036	CL= 1.593 CD=0.02070	CL= 1.591 CD=0.02120
	CM=-0.1938	CM=-0.1938	CM=-0.1932
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0363 0.0502 0.0217*	1.0363 0.0502 0.0217*	1.0391 0.0508 0.0219*
	LOWER 0.6225 0.0000 0.0011*	0.9293 0.0000 0.0014	0.7233 0.0000 0.0013
	TOTAL CL= 1.686 CD=0.02277	CL= 1.686 CD=0.02308	CL= 1.685 CD=0.02319
	CM=-0.1917	CM=-0.1917	CM=-0.1915

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 2500000 MU=3.0	R= 2500000 MU=1.3	R= 2500000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.0903 0.0114 0.0014 LOWER 1.0055 0.4562 0.0069* TOTAL CL=-0.106 CD=0.00827 CM=-0.1755	S TURB S SEP CD 1.0043 0.0000 0.0053 1.0055 0.4562 0.0069* CL=-0.097 CD=0.01215 CM=-0.1764	S TURB S SEP CD 0.8671 0.0000 0.0051 1.0206 0.4600 0.0071* CL=-0.097 CD=0.01224 CM=-0.1764
-6.00	S TURB S SEP CD UPPER 0.3673 0.0000 0.0029 LOWER 0.7045 0.0000 0.0032 TOTAL CL= 0.013 CD=0.00608 CM=-0.1788	S TURB S SEP CD 1.0043 0.0000 0.0056 0.9635 0.4211 0.0056 CL= 0.013 CD=0.01128 CM=-0.1788	S TURB S SEP CD 0.8861 0.0000 0.0055 1.0184 0.4394 0.0063 CL= 0.013 CD=0.01174 CM=-0.1788
-5.00	S TURB S SEP CD UPPER 0.4600 0.0000 0.0035 LOWER 0.7021 0.0000 0.0030* TOTAL CL= 0.123 CD=0.00650 CM=-0.1811	S TURB S SEP CD 1.0043 0.0000 0.0060 0.9635 0.3954 0.0051 CL= 0.123 CD=0.01109 CM=-0.1811	S TURB S SEP CD 0.9027 0.0000 0.0058 1.0104 0.4111 0.0055 CL= 0.123 CD=0.01131 CM=-0.1811
-4.00	S TURB S SEP CD UPPER 0.5226 0.0000 0.0040 LOWER 0.6997 0.0000 0.0028* TOTAL CL= 0.233 CD=0.00683 CM=-0.1834	S TURB S SEP CD 1.0043 0.0000 0.0064 0.9635 0.3666 0.0046 CL= 0.233 CD=0.01109 CM=-0.1834	S TURB S SEP CD 0.9189 0.0000 0.0063 0.9985 0.3757 0.0048 CL= 0.233 CD=0.01110 CM=-0.1834
-3.00	S TURB S SEP CD UPPER 0.5717 0.0000 0.0046 LOWER 0.6972 0.0000 0.0026* TOTAL CL= 0.343 CD=0.00720 CM=-0.1857	S TURB S SEP CD 1.0043 0.0011 0.0070 0.9635 0.3259 0.0042 CL= 0.341 CD=0.01115 CM=-0.1856	S TURB S SEP CD 0.9345 0.0010 0.0068 0.9849 0.3345 0.0043 CL= 0.342 CD=0.01109 CM=-0.1856
-2.00	S TURB S SEP CD UPPER 0.6085 0.0015 0.0051 LOWER 0.6948 0.0000 0.0025* TOTAL CL= 0.451 CD=0.00752 CM=-0.1876	S TURB S SEP CD 1.0043 0.0038 0.0075 0.9635 0.2691 0.0038 CL= 0.449 CD=0.01127 CM=-0.1874	S TURB S SEP CD 0.9496 0.0037 0.0073 0.9695 0.2724 0.0038 CL= 0.449 CD=0.01115 CM=-0.1874
-1.00	S TURB S SEP CD UPPER 0.6341 0.0036 0.0055 LOWER 0.6923 0.0000 0.0023* TOTAL CL= 0.559 CD=0.00780 CM=-0.1892	S TURB S SEP CD 1.0043 0.0058 0.0080 0.9635 0.1806 0.0035 CL= 0.556 CD=0.01148 CM=-0.1890	S TURB S SEP CD 0.9633 0.0057 0.0079 0.9536 0.1732 0.0034 CL= 0.556 CD=0.01132 CM=-0.1890
0.00	S TURB S SEP CD UPPER 0.6496 0.0052 0.0059 LOWER 0.6897 0.0000 0.0022* TOTAL CL= 0.666 CD=0.00804 CM=-0.1909	S TURB S SEP CD 1.0043 0.0079 0.0086 0.9635 0.0000 0.0032 CL= 0.663 CD=0.01182 CM=-0.1901	S TURB S SEP CD 0.9757 0.0077 0.0085 0.9362 0.0000 0.0031 CL= 0.663 CD=0.01165 CM=-0.1902
1.00	S TURB S SEP CD UPPER 0.6598 0.0067 0.0062 LOWER 0.6870 0.0000 0.0020* TOTAL CL= 0.774 CD=0.00827 CM=-0.1925	S TURB S SEP CD 1.0043 0.0100 0.0093 0.9635 0.0000 0.0029 CL= 0.770 CD=0.01221 CM=-0.1916	S TURB S SEP CD 0.9887 0.0099 0.0092 0.9184 0.0000 0.0029 CL= 0.770 CD=0.01208 CM=-0.1916
2.00	S TURB S SEP CD UPPER 0.6690 0.0082 0.0066 LOWER 0.6840 0.0000 0.0019* TOTAL CL= 0.882 CD=0.00852 CM=-0.1941	S TURB S SEP CD 1.0043 0.0123 0.0100 0.9635 0.0000 0.0027 CL= 0.877 CD=0.01270 CM=-0.1928	S TURB S SEP CD 0.9995 0.0123 0.0100 0.8995 0.0000 0.0026 CL= 0.877 CD=0.01259 CM=-0.1928
3.00	S TURB S SEP CD UPPER 0.6788 0.0098 0.0070 LOWER 0.6805 0.0000 0.0018* TOTAL CL= 0.989 CD=0.00881 CM=-0.1955	S TURB S SEP CD 1.0043 0.0149 0.0108 0.9635 0.0000 0.0025 CL= 0.983 CD=0.01326 CM=-0.1939	S TURB S SEP CD 1.0092 0.0149 0.0108 0.8860 0.0000 0.0024 CL= 0.983 CD=0.01323 CM=-0.1939
4.00	S TURB S SEP CD UPPER 0.6910 0.0115 0.0075 LOWER 0.6762 0.0000 0.0017* TOTAL CL= 1.097 CD=0.00917 CM=-0.1968	S TURB S SEP CD 1.0043 0.0177 0.0116 0.9635 0.0000 0.0023 CL= 1.088 CD=0.01390 CM=-0.1948	S TURB S SEP CD 1.0187 0.0179 0.0118 0.7556 0.0000 0.0020 CL= 1.088 CD=0.01377 CM=-0.1947
5.00	S TURB S SEP CD UPPER 0.7049 0.0134 0.0080 LOWER 0.6702 0.0000 0.0016* TOTAL CL= 1.203 CD=0.00959 CM=-0.1980	S TURB S SEP CD 1.0043 0.0207 0.0125 0.9635 0.0000 0.0021 CL= 1.193 CD=0.01464 CM=-0.1955	S TURB S SEP CD 1.0259 0.0212 0.0129 0.7532 0.0000 0.0018 CL= 1.192 CD=0.01473 CM=-0.1953
6.00	S TURB S SEP CD UPPER 0.7242 0.0156 0.0087 LOWER 0.6613 0.0000 0.0015* TOTAL CL= 1.309 CD=0.01015 CM=-0.1989	S TURB S SEP CD 1.0043 0.0241 0.0136 0.9635 0.0000 0.0019 CL= 1.296 CD=0.01548 CM=-0.1959	S TURB S SEP CD 1.0340 0.0255 0.0143 0.7508 0.0000 0.0017 CL= 1.294 CD=0.01599 CM=-0.1954
7.00	S TURB S SEP CD UPPER 0.9549 0.0255 0.0134 LOWER 0.6525 0.0000 0.0013* TOTAL CL= 1.403 CD=0.01478 CM=-0.1970	S TURB S SEP CD 1.0043 0.0282 0.0148 0.9564 0.0000 0.0018 CL= 1.398 CD=0.01654 CM=-0.1960	S TURB S SEP CD 1.0375 0.0300 0.0157 0.7484 0.0000 0.0016 CL= 1.396 CD=0.01730 CM=-0.1953

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 2500000 MU=3.0	R= 2500000 MU=1.3	R= 2500000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0070 0.0327 0.0161	1.0070 0.0327 0.0161	1.0388 0.0352 0.0173
	LOWER 0.6436 0.0000 0.0013*	0.9564 0.0000 0.0016	0.7446 0.0000 0.0015
	TOTAL CL= 1.500 CD=0.01731	CL= 1.500 CD=0.01770	CL= 1.496 CD=0.01879
	CM=-0.1958	CM=-0.1958	CM=-0.1948
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0277 0.0397 0.0184*	1.0277 0.0397 0.0184*	1.0391 0.0412 0.0191
	LOWER 0.6339 0.0000 0.0012	0.9564 0.0000 0.0015	0.7391 0.0000 0.0014
	TOTAL CL= 1.596 CD=0.01958	CL= 1.596 CD=0.01993	CL= 1.594 CD=0.02046
	CM=-0.1945	CM=-0.1945	CM=-0.1939
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0363 0.0478 0.0208*	1.0363 0.0478 0.0208*	1.0392 0.0485 0.0211
	LOWER 0.6227 0.0000 0.0011*	0.9293 0.0000 0.0014	0.7320 0.0000 0.0013
	TOTAL CL= 1.690 CD=0.02191	CL= 1.690 CD=0.02223	CL= 1.689 CD=0.02236
	CM=-0.1926	CM=-0.1926	CM=-0.1923

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 3000000 MU=3.0	R= 3000000 MU=1.3	R= 3000000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.2640 0.0000 0.0022 LOWER 1.0055 0.4483 0.0067 TOTAL CL=-0.097 CD=0.00882 CM=-0.1764	S TURB S SEP CD 1.0043 0.0000 0.0052 1.0055 0.4483 0.0067 CL=-0.097 CD=0.01181 CM=-0.1764	S TURB S SEP CD 0.8806 0.0000 0.0050 1.0207 0.4524 0.0069* CL=-0.097 CD=0.01194 CM=-0.1764
-6.00	S TURB S SEP CD UPPER 0.4212 0.0000 0.0031 LOWER 0.7062 0.0000 0.0031 TOTAL CL= 0.013 CD=0.00615 CM=-0.1788	S TURB S SEP CD 1.0043 0.0000 0.0055 0.9635 0.4110 0.0055 CL= 0.013 CD=0.01097 CM=-0.1788	S TURB S SEP CD 0.8991 0.0000 0.0054 1.0192 0.4309 0.0061 CL= 0.013 CD=0.01146 CM=-0.1788
-5.00	S TURB S SEP CD UPPER 0.4945 0.0000 0.0036 LOWER 0.7037 0.0000 0.0029* TOTAL CL= 0.123 CD=0.00647 CM=-0.1811	S TURB S SEP CD 1.0043 0.0000 0.0058 0.9635 0.3838 0.0049 CL= 0.123 CD=0.01079 CM=-0.1811	S TURB S SEP CD 0.9144 0.0000 0.0057 1.0121 0.4015 0.0053 CL= 0.123 CD=0.01105 CM=-0.1811
-4.00	S TURB S SEP CD UPPER 0.5483 0.0000 0.0041 LOWER 0.7011 0.0000 0.0027* TOTAL CL= 0.233 CD=0.00676 CM=-0.1834	S TURB S SEP CD 1.0043 0.0000 0.0062 0.9635 0.3532 0.0045 CL= 0.233 CD=0.01074 CM=-0.1834	S TURB S SEP CD 0.9296 0.0000 0.0061 1.0014 0.3644 0.0047 CL= 0.233 CD=0.01080 CM=-0.1834
-3.00	S TURB S SEP CD UPPER 0.5910 0.0000 0.0045 LOWER 0.6987 0.0000 0.0025* TOTAL CL= 0.343 CD=0.00705 CM=-0.1857	S TURB S SEP CD 1.0043 0.0000 0.0068 0.9635 0.3096 0.0041 CL= 0.343 CD=0.01083 CM=-0.1857	S TURB S SEP CD 0.9444 0.0000 0.0066 0.9893 0.3211 0.0042 CL= 0.343 CD=0.01082 CM=-0.1857
-2.00	S TURB S SEP CD UPPER 0.6228 0.0003 0.0050 LOWER 0.6962 0.0000 0.0024* TOTAL CL= 0.452 CD=0.00736 CM=-0.1879	S TURB S SEP CD 1.0043 0.0024 0.0073 0.9635 0.2481 0.0037 CL= 0.450 CD=0.01095 CM=-0.1876	S TURB S SEP CD 0.9578 0.0023 0.0071 0.9754 0.2552 0.0037 CL= 0.450 CD=0.01088 CM=-0.1876
-1.00	S TURB S SEP CD UPPER 0.6437 0.0024 0.0054 LOWER 0.6937 0.0000 0.0022* TOTAL CL= 0.560 CD=0.00761 CM=-0.1896	S TURB S SEP CD 1.0043 0.0047 0.0078 0.9635 0.1515 0.0034 CL= 0.557 CD=0.01116 CM=-0.1892	S TURB S SEP CD 0.9700 0.0046 0.0077 0.9602 0.1487 0.0034 CL= 0.557 CD=0.01105 CM=-0.1892
0.00	S TURB S SEP CD UPPER 0.6553 0.0041 0.0057 LOWER 0.6911 0.0000 0.0021* TOTAL CL= 0.668 CD=0.00781 CM=-0.1912	S TURB S SEP CD 1.0043 0.0068 0.0084 0.9635 0.0000 0.0031 CL= 0.665 CD=0.01149 CM=-0.1904	S TURB S SEP CD 0.9821 0.0067 0.0083 0.9442 0.0000 0.0031 CL= 0.665 CD=0.01137 CM=-0.1905
1.00	S TURB S SEP CD UPPER 0.6647 0.0057 0.0060 LOWER 0.6885 0.0000 0.0020* TOTAL CL= 0.776 CD=0.00803 CM=-0.1929	S TURB S SEP CD 1.0043 0.0090 0.0090 0.9635 0.0000 0.0029 CL= 0.772 CD=0.01188 CM=-0.1919	S TURB S SEP CD 0.9935 0.0089 0.0090 0.9284 0.0000 0.0028 CL= 0.772 CD=0.01178 CM=-0.1919
2.00	S TURB S SEP CD UPPER 0.6738 0.0072 0.0064 LOWER 0.6856 0.0000 0.0019* TOTAL CL= 0.883 CD=0.00828 CM=-0.1944	S TURB S SEP CD 1.0043 0.0112 0.0097 0.9635 0.0000 0.0026 CL= 0.878 CD=0.01234 CM=-0.1931	S TURB S SEP CD 1.0039 0.0112 0.0097 0.9108 0.0000 0.0026 CL= 0.878 CD=0.01228 CM=-0.1931
3.00	S TURB S SEP CD UPPER 0.6845 0.0088 0.0068 LOWER 0.6823 0.0000 0.0017 TOTAL CL= 0.991 CD=0.00857 CM=-0.1958	S TURB S SEP CD 1.0043 0.0138 0.0105 0.9635 0.0000 0.0024 CL= 0.984 CD=0.01288 CM=-0.1942	S TURB S SEP CD 1.0122 0.0139 0.0105 0.8940 0.0000 0.0024 CL= 0.984 CD=0.01289 CM=-0.1942
4.00	S TURB S SEP CD UPPER 0.6970 0.0105 0.0073 LOWER 0.6783 0.0000 0.0016 TOTAL CL= 1.098 CD=0.00892 CM=-0.1972	S TURB S SEP CD 1.0043 0.0165 0.0113 0.9635 0.0000 0.0022 CL= 1.089 CD=0.01350 CM=-0.1951	S TURB S SEP CD 1.0212 0.0168 0.0115 0.8808 0.0000 0.0022 CL= 1.089 CD=0.01364 CM=-0.1950
5.00	S TURB S SEP CD UPPER 0.7114 0.0124 0.0078 LOWER 0.6730 0.0000 0.0015* TOTAL CL= 1.205 CD=0.00934 CM=-0.1983	S TURB S SEP CD 1.0043 0.0195 0.0122 0.9635 0.0000 0.0020 CL= 1.194 CD=0.01421 CM=-0.1959	S TURB S SEP CD 1.0285 0.0201 0.0125 0.7580 0.0000 0.0018 CL= 1.193 CD=0.01434 CM=-0.1957
6.00	S TURB S SEP CD UPPER 0.8511 0.0178 0.0103 LOWER 0.6646 0.0000 0.0014* TOTAL CL= 1.306 CD=0.01176 CM=-0.1981	S TURB S SEP CD 1.0043 0.0228 0.0131 0.9635 0.0000 0.0019 CL= 1.298 CD=0.01502 CM=-0.1964	S TURB S SEP CD 1.0352 0.0239 0.0138 0.7552 0.0000 0.0017 CL= 1.296 CD=0.01546 CM=-0.1960
7.00	S TURB S SEP CD UPPER 0.9638 0.0246 0.0132 LOWER 0.6556 0.0000 0.0013* TOTAL CL= 1.404 CD=0.01451 CM=-0.1973	S TURB S SEP CD 1.0043 0.0265 0.0142 0.9564 0.0000 0.0017 CL= 1.401 CD=0.01593 CM=-0.1966	S TURB S SEP CD 1.0383 0.0287 0.0153 0.7524 0.0000 0.0016 CL= 1.398 CD=0.01682 CM=-0.1958

B.L.SUMMARY AIRFOIL S825 17% ALPHA0= 6.114 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 3000000 MU=3.0	R= 3000000 MU=1.3	R= 3000000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0070 0.0308 0.0154	1.0070 0.0308 0.0154	1.0389 0.0338 0.0168
	LOWER 0.6467 0.0000 0.0012	0.9564 0.0000 0.0016	0.7498 0.0000 0.0015
	TOTAL CL= 1.503 CD=0.01666	CL= 1.503 CD=0.01703	CL= 1.498 CD=0.01824
	CM=-0.1965	CM=-0.1965	CM=-0.1954
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0277 0.0381 0.0179	1.0277 0.0381 0.0179	1.0391 0.0396 0.0185
	LOWER 0.6372 0.0000 0.0011	0.9564 0.0000 0.0015	0.7464 0.0000 0.0014
	TOTAL CL= 1.599 CD=0.01898	CL= 1.599 CD=0.01932	CL= 1.596 CD=0.01987
	CM=-0.1951	CM=-0.1951	CM=-0.1945
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0363 0.0459 0.0202*	1.0363 0.0459 0.0202*	1.0393 0.0466 0.0205
	LOWER 0.6265 0.0000 0.0010*	0.9293 0.0000 0.0014	0.7406 0.0000 0.0012
	TOTAL CL= 1.693 CD=0.02124	CL= 1.693 CD=0.02155	CL= 1.692 CD=0.02171
	CM=-0.1933	CM=-0.1933	CM=-0.1930

AIRFOIL S826 14%				-7.00	-6.00	-5.00	-4.00	-3.00	-2.00	-1.00	0.00	1.00
N	X	Y	NUE	CP-DISTR.	FOR THE	ABOVE	ALPHA	REL.	CHORD	LINE		
1	1.00000	0.00000	0.00	0.265	0.265	0.265	0.266	0.267	0.269	0.271	0.274	0.277
2	0.99668	0.00103	1.00	0.249	0.247	0.246	0.246	0.246	0.246	0.247	0.249	0.250
3	0.98719	0.00431	2.00	0.170	0.167	0.164	0.162	0.161	0.160	0.159	0.159	0.160
4	0.97251	0.00982	3.00	0.044	0.039	0.034	0.030	0.027	0.024	0.021	0.019	0.018
5	0.95355	0.01695	4.00	-0.102	-0.110	-0.117	-0.124	-0.130	-0.136	-0.141	-0.145	-0.148
6	0.93072	0.02479	5.00	-0.227	-0.238	-0.249	-0.259	-0.269	-0.277	-0.285	-0.292	-0.299
7	0.90391	0.03262	6.00	-0.279	-0.293	-0.307	-0.320	-0.333	-0.344	-0.355	-0.365	-0.374
8	0.87287	0.04029	7.00	-0.276	-0.293	-0.310	-0.326	-0.341	-0.355	-0.369	-0.382	-0.394
9	0.83778	0.04798	8.00	-0.278	-0.298	-0.317	-0.336	-0.354	-0.371	-0.388	-0.403	-0.418
10	0.79915	0.05572	9.00	-0.283	-0.306	-0.329	-0.350	-0.371	-0.392	-0.412	-0.431	-0.449
11	0.75749	0.06341	10.00	-0.292	-0.319	-0.344	-0.370	-0.394	-0.418	-0.441	-0.464	-0.486
12	0.71333	0.07095	11.00	-0.305	-0.335	-0.364	-0.393	-0.422	-0.449	-0.477	-0.503	-0.529
13	0.66724	0.07816	12.00	-0.321	-0.355	-0.389	-0.422	-0.455	-0.487	-0.518	-0.549	-0.579
14	0.61980	0.08489	13.00	-0.341	-0.379	-0.418	-0.455	-0.493	-0.530	-0.566	-0.602	-0.637
15	0.57161	0.09094	14.00	-0.364	-0.407	-0.450	-0.494	-0.536	-0.579	-0.621	-0.662	-0.704
16	0.52324	0.09607	15.00	-0.389	-0.438	-0.487	-0.536	-0.585	-0.634	-0.683	-0.731	-0.779
17	0.47526	0.10005	16.00	-0.415	-0.471	-0.527	-0.584	-0.640	-0.696	-0.752	-0.808	-0.864
18	0.42820	0.10249	17.00	-0.443	-0.506	-0.570	-0.635	-0.699	-0.764	-0.829	-0.894	-0.959
19	0.38228	0.10294	18.00	-0.427	-0.497	-0.568	-0.640	-0.712	-0.785	-0.858	-0.931	-1.005
20	0.33736	0.10133	19.00	-0.364	-0.440	-0.516	-0.594	-0.672	-0.751	-0.831	-0.912	-0.993
21	0.29361	0.09807	20.00	-0.297	-0.377	-0.460	-0.543	-0.629	-0.715	-0.803	-0.891	-0.981
22	0.25149	0.09343	21.00	-0.222	-0.309	-0.397	-0.488	-0.581	-0.675	-0.771	-0.869	-0.968
23	0.21146	0.08758	22.00	-0.139	-0.232	-0.328	-0.426	-0.528	-0.631	-0.737	-0.845	-0.956
24	0.17395	0.08068	23.00	-0.047	-0.146	-0.250	-0.357	-0.467	-0.581	-0.698	-0.819	-0.942
25	0.13934	0.07288	24.00	0.060	-0.047	-0.158	-0.275	-0.396	-0.522	-0.652	-0.787	-0.926
26	0.10801	0.06434	25.00	0.183	0.070	-0.050	-0.177	-0.311	-0.450	-0.596	-0.748	-0.906
27	0.08026	0.05519	26.00	0.331	0.211	0.083	-0.055	-0.202	-0.357	-0.521	-0.693	-0.874
28	0.05636	0.04562	27.00	0.504	0.382	0.247	0.100	-0.061	-0.234	-0.419	-0.616	-0.825
29	0.03651	0.03580	28.00	0.706	0.590	0.455	0.302	0.130	-0.060	-0.269	-0.495	-0.738
30	0.02088	0.02596	29.00	0.908	0.820	0.703	0.558	0.384	0.182	-0.048	-0.306	-0.592
31	0.00954	0.01638	30.00	0.995	0.994	0.946	0.850	0.708	0.519	0.284	0.002	-0.326
32	0.00255	0.00748	31.00	0.481	0.736	0.906	0.990	0.988	0.901	0.728	0.469	0.125
33	0.00018	0.00159	31.77	-1.668	-0.826	-0.142	0.382	0.747	0.952	0.996	0.880	0.603
34	0.00000	-0.00005	32.02	-3.399	-2.158	-1.121	-0.288	0.339	0.758	0.971	0.977	0.775
35	0.00021	-0.00146	32.27	-6.338	-4.467	-2.868	-1.543	-0.494	0.279	0.773	0.989	0.927
36	0.00093	-0.00274	32.52	-4.942	-3.560	-2.359	-1.339	-0.502	0.151	0.619	0.902	1.000
37	0.00216	-0.00403	32.77	-4.064	-2.983	-2.029	-1.204	-0.508	0.056	0.490	0.791	0.960
38	0.00367	-0.00525	33.00	-3.498	-2.606	-1.810	-1.112	-0.512	-0.012	0.389	0.690	0.889
39	0.01367	-0.01035	34.00	-2.135	-1.659	-1.221	-0.821	-0.460	-0.138	0.145	0.388	0.590
40	0.02920	-0.01518	35.00	-1.505	-1.199	-0.911	-0.642	-0.393	-0.163	0.046	0.235	0.404
41	0.04998	-0.01960	36.00	-1.147	-0.928	-0.720	-0.523	-0.336	-0.161	0.002	0.153	0.293
42	0.07580	-0.02362	37.00	-0.911	-0.744	-0.585	-0.432	-0.286	-0.147	-0.015	0.109	0.226
43	0.10637	-0.02729	38.00	-0.746	-0.615	-0.487	-0.364	-0.245	-0.131	-0.022	0.082	0.182
44	0.14133	-0.03091	39.00	-0.624	-0.516	-0.412	-0.310	-0.211	-0.115	-0.023	0.066	0.152
45	0.17965	-0.03486	40.00	-0.619	-0.524	-0.431	-0.340	-0.251	-0.164	-0.080	0.001	0.080
46	0.21987	-0.03855	41.00	-0.699	-0.610	-0.523	-0.437	-0.352	-0.270	-0.189	-0.110	-0.033
47	0.26153	-0.04064	42.00	-0.705	-0.625	-0.546	-0.468	-0.391	-0.315	-0.241	-0.168	-0.097
48	0.30497	-0.04051	43.00	-0.649	-0.579	-0.510	-0.442	-0.374	-0.307	-0.241	-0.176	-0.112
49	0.35027	-0.03794	44.00	-0.559	-0.499	-0.440	-0.381	-0.323	-0.265	-0.208	-0.151	-0.095
50	0.39779	-0.03280	45.00	-0.395	-0.347	-0.300	-0.252	-0.204	-0.157	-0.110	-0.063	-0.016
51	0.44785	-0.02563	46.00	-0.241	-0.202	-0.164	-0.125	-0.087	-0.048	-0.009	0.029	0.067
52	0.50032	-0.01720	47.00	-0.090	-0.060	-0.029	0.001	0.032	0.063	0.094	0.126	0.157
53	0.55484	-0.00841	48.00	0.030	0.054	0.079	0.103	0.128	0.154	0.179	0.204	0.230
54	0.61055	-0.00015	49.00	0.124	0.144	0.164	0.184	0.204	0.225	0.246	0.267	0.288
55	0.66644	0.00699	50.00	0.199	0.215	0.231	0.248	0.265	0.282	0.299	0.317	0.334
56	0.72142	0.01254	51.00	0.259	0.272	0.285	0.299	0.313	0.327	0.342	0.357	0.372
57	0.77434	0.01621	52.00	0.307	0.318	0.329	0.340	0.352	0.364	0.376	0.388	0.401
58	0.82409	0.01784	53.00	0.346	0.354	0.363	0.373	0.382	0.392	0.403	0.413	0.424
59	0.86953	0.01741	54.00	0.376	0.383	0.391	0.399	0.407	0.415	0.423	0.432	0.442
60	0.90945	0.01498	55.00	0.388	0.394	0.400	0.406	0.413	0.420	0.427	0.435	0.443
61	0.94257	0.01113	56.00	0.376	0.380	0.385	0.391	0.396	0.402	0.409	0.415	0.422
62	0.96813	0.00689	57.00	0.347	0.350	0.354	0.359	0.364	0.369	0.374	0.380	0.386
63	0.98604	0.00324	58.00	0.311	0.313	0.316	0.319	0.323	0.327	0.332	0.337	0.342
64	0.99655	0.00084	59.00	0.279	0.280	0.282	0.284	0.287	0.290	0.293	0.297	0.302
65	1.00000	0.00000	60.00	0.265	0.265	0.265	0.266	0.267	0.269	0.271	0.274	0.277

ALPHA0= 6.52 DEGREES CM0=-0.1802 ETA= 1.102

AIRFOIL S826 14%			2.00	3.00	4.00	5.00	6.00	7.00	8.00	9.00	10.00	
N	X	Y	NUE	CP-DISTR.	FOR THE	ABOVE	ALPHA	REL.	CHORD	LINE		
1	1.00000	0.00000	0.00	0.281	0.285	0.289	0.294	0.299	0.305	0.311	0.317	0.324
2	0.99668	0.00103	1.00	0.253	0.255	0.259	0.262	0.266	0.271	0.276	0.281	0.287
3	0.98719	0.00431	2.00	0.161	0.162	0.164	0.167	0.170	0.174	0.178	0.182	0.187
4	0.97251	0.00982	3.00	0.018	0.018	0.018	0.020	0.021	0.024	0.027	0.030	0.034
5	0.95355	0.01695	4.00	-0.151	-0.153	-0.155	-0.155	-0.155	-0.155	-0.153	-0.151	-0.148
6	0.93072	0.02479	5.00	-0.304	-0.309	-0.313	-0.316	-0.318	-0.320	-0.321	-0.321	-0.320
7	0.90391	0.03262	6.00	-0.383	-0.391	-0.397	-0.403	-0.408	-0.413	-0.416	-0.419	-0.420
8	0.87287	0.04029	7.00	-0.405	-0.415	-0.425	-0.434	-0.442	-0.449	-0.455	-0.460	-0.465
9	0.83778	0.04798	8.00	-0.433	-0.446	-0.459	-0.471	-0.481	-0.492	-0.501	-0.509	-0.516
10	0.79915	0.05572	9.00	-0.466	-0.483	-0.499	-0.514	-0.528	-0.542	-0.554	-0.566	-0.576
11	0.75749	0.06341	10.00	-0.507	-0.527	-0.547	-0.565	-0.583	-0.600	-0.616	-0.631	-0.645
12	0.71333	0.07095	11.00	-0.554	-0.578	-0.602	-0.625	-0.646	-0.667	-0.688	-0.707	-0.725
13	0.66724	0.07816	12.00	-0.609	-0.638	-0.666	-0.693	-0.720	-0.745	-0.770	-0.794	-0.817
14	0.61980	0.08489	13.00	-0.672	-0.706	-0.739	-0.772	-0.804	-0.834	-0.865	-0.894	-0.922
15	0.57161	0.09094	14.00	-0.744	-0.784	-0.823	-0.862	-0.900	-0.937	-0.973	-1.009	-1.043
16	0.52324	0.09607	15.00	-0.826	-0.873	-0.919	-0.965	-1.010	-1.054	-1.098	-1.140	-1.182
17	0.47526	0.10005	16.00	-0.919	-0.974	-1.028	-1.083	-1.136	-1.189	-1.241	-1.292	-1.343
18	0.42820	0.10249	17.00	-1.023	-1.088	-1.152	-1.216	-1.280	-1.343	-1.405	-1.467	-1.528
19	0.38228	0.10294	18.00	-1.078	-1.152	-1.226	-1.300	-1.373	-1.446	-1.519	-1.591	-1.662
20	0.33736	0.10133	19.00	-1.075	-1.157	-1.239	-1.321	-1.403	-1.486	-1.568	-1.650	-1.732
21	0.29361	0.09807	20.00	-1.071	-1.163	-1.254	-1.347	-1.439	-1.532	-1.625	-1.719	-1.812
22	0.25149	0.09343	21.00	-1.069	-1.171	-1.274	-1.377	-1.482	-1.587	-1.693	-1.800	-1.906
23	0.21146	0.08758	22.00	-1.068	-1.182	-1.298	-1.415	-1.534	-1.654	-1.775	-1.897	-2.020
24	0.17395	0.08068	23.00	-1.068	-1.197	-1.328	-1.462	-1.598	-1.736	-1.875	-2.017	-2.160
25	0.13934	0.07288	24.00	-1.068	-1.215	-1.365	-1.519	-1.676	-1.836	-1.998	-2.164	-2.332
26	0.10801	0.06434	25.00	-1.069	-1.237	-1.411	-1.590	-1.773	-1.962	-2.154	-2.350	-2.551
27	0.08026	0.05519	26.00	-1.062	-1.259	-1.462	-1.673	-1.891	-2.115	-2.346	-2.583	-2.826
28	0.05636	0.04562	27.00	-1.046	-1.277	-1.520	-1.774	-2.038	-2.311	-2.595	-2.888	-3.190
29	0.03651	0.03580	28.00	-0.999	-1.277	-1.572	-1.882	-2.209	-2.551	-2.908	-3.280	-3.665
30	0.02088	0.02596	29.00	-0.905	-1.244	-1.610	-2.002	-2.419	-2.861	-3.327	-3.818	-4.331
31	0.00954	0.01638	30.00	-0.699	-1.117	-1.580	-2.087	-2.637	-3.230	-3.865	-4.541	-5.258
32	0.00255	0.00748	31.00	-0.303	-0.816	-1.412	-2.091	-2.852	-3.694	-4.616	-5.617	-6.696
33	0.00018	0.00159	31.77	0.167	-0.429	-1.184	-2.096	-3.165	-4.390	-5.769	-7.299	-8.980
34	0.00000	-0.00005	32.02	0.365	-0.250	-1.072	-2.099	-3.330	-4.762	-6.395	-8.227	-10.254
35	0.00021	-0.00146	32.27	0.586	-0.033	-0.930	-2.103	-3.551	-5.271	-7.263	-9.524	-12.050
36	0.00093	-0.00274	32.52	0.912	0.638	0.180	-0.464	-1.291	-2.301	-3.493	-4.865	-6.416
37	0.00216	-0.00403	32.77	0.997	0.901	0.672	0.312	-0.180	-0.804	-1.557	-2.440	-3.452
38	0.00367	-0.00525	33.00	0.988	0.986	0.883	0.679	0.375	-0.030	-0.535	-1.138	-1.841
39	0.01367	-0.01035	34.00	0.753	0.874	0.955	0.995	0.994	0.953	0.870	0.747	0.583
40	0.02920	-0.01518	35.00	0.552	0.679	0.785	0.870	0.934	0.977	0.998	0.997	0.975
41	0.04998	-0.01960	36.00	0.420	0.535	0.638	0.728	0.805	0.870	0.921	0.960	0.986
42	0.07580	-0.02362	37.00	0.335	0.436	0.529	0.613	0.690	0.759	0.819	0.870	0.913
43	0.10637	-0.02729	38.00	0.275	0.364	0.447	0.525	0.597	0.664	0.724	0.779	0.828
44	0.14133	-0.03091	39.00	0.234	0.312	0.386	0.457	0.523	0.586	0.644	0.698	0.748
45	0.17965	-0.03486	40.00	0.156	0.230	0.300	0.368	0.432	0.494	0.552	0.607	0.658
46	0.21987	-0.03855	41.00	0.041	0.114	0.184	0.251	0.316	0.379	0.439	0.496	0.551
47	0.26153	-0.04064	42.00	-0.027	0.041	0.108	0.172	0.234	0.295	0.353	0.410	0.464
48	0.30497	-0.04051	43.00	-0.049	0.012	0.073	0.132	0.189	0.245	0.300	0.353	0.404
49	0.35027	-0.03794	44.00	-0.040	0.015	0.068	0.121	0.172	0.223	0.272	0.321	0.368
50	0.39779	-0.03280	45.00	0.030	0.075	0.120	0.165	0.208	0.252	0.294	0.335	0.376
51	0.44785	-0.02563	46.00	0.105	0.143	0.180	0.218	0.254	0.291	0.326	0.362	0.396
52	0.50032	-0.01720	47.00	0.188	0.219	0.249	0.280	0.310	0.341	0.370	0.400	0.429
53	0.55484	-0.00841	48.00	0.255	0.281	0.307	0.332	0.357	0.383	0.408	0.433	0.458
54	0.61055	-0.00015	49.00	0.309	0.331	0.352	0.374	0.395	0.417	0.438	0.459	0.481
55	0.66644	0.00699	50.00	0.352	0.370	0.389	0.407	0.425	0.444	0.462	0.481	0.499
56	0.72142	0.01254	51.00	0.387	0.402	0.418	0.433	0.449	0.465	0.481	0.497	0.513
57	0.77434	0.01621	52.00	0.414	0.427	0.440	0.454	0.468	0.481	0.495	0.509	0.524
58	0.82409	0.01784	53.00	0.435	0.446	0.458	0.470	0.481	0.494	0.506	0.518	0.531
59	0.86953	0.01741	54.00	0.451	0.461	0.471	0.481	0.491	0.502	0.512	0.523	0.534
60	0.90945	0.01498	55.00	0.451	0.460	0.468	0.477	0.486	0.496	0.506	0.515	0.526
61	0.94257	0.01113	56.00	0.430	0.437	0.445	0.453	0.462	0.470	0.479	0.488	0.498
62	0.96813	0.00689	57.00	0.393	0.400	0.407	0.414	0.422	0.430	0.439	0.447	0.456
63	0.98604	0.00324	58.00	0.348	0.354	0.360	0.367	0.374	0.382	0.390	0.398	0.406
64	0.99655	0.00084	59.00	0.306	0.311	0.317	0.323	0.329	0.336	0.343	0.350	0.358
65	1.00000	0.00000	60.00	0.281	0.285	0.289	0.294	0.299	0.305	0.311	0.317	0.324

ALPHA0= 6.52 DEGREES CM0=-0.1802 ETA= 1.102

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA (DEG.)	R= 1000000 MU=3.0	R= 1000000 MU=1.3	R= 1000000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.0829 0.0332 0.0021 LOWER 1.0097 1.0084 0.0023* TOTAL CL=-0.078 CD=0.00445 CM=-0.1786	S TURB S SEP CD 1.0022 0.0000 0.0060 1.0097 1.0084 0.0023* CL=-0.053 CD=0.00837 CM=-0.1787	S TURB S SEP CD 0.7555 0.0000 0.0056 1.0097 1.0079 0.0024* CL=-0.053 CD=0.00798 CM=-0.1787
-6.00	S TURB S SEP CD UPPER 0.0888 0.0321 0.0022 LOWER 1.0096 0.2550 0.0062* TOTAL CL= 0.031 CD=0.00844 CM=-0.1768	S TURB S SEP CD 1.0022 0.0000 0.0065 1.0096 0.2550 0.0062* CL= 0.057 CD=0.01271 CM=-0.1807	S TURB S SEP CD 0.7862 0.0000 0.0061 1.0096 0.2550 0.0062* CL= 0.057 CD=0.01229 CM=-0.1807
-5.00	S TURB S SEP CD UPPER 0.3519 0.0000 0.0037 LOWER 1.0093 0.1912 0.0055* TOTAL CL= 0.167 CD=0.00917 CM=-0.1828	S TURB S SEP CD 1.0022 0.0018 0.0070 1.0093 0.1912 0.0055* CL= 0.166 CD=0.01247 CM=-0.1825	S TURB S SEP CD 0.8116 0.0008 0.0065 1.0093 0.1912 0.0055* CL= 0.167 CD=0.01201 CM=-0.1826
-4.00	S TURB S SEP CD UPPER 0.4343 0.0011 0.0044 LOWER 0.6496 0.0000 0.0030 TOTAL CL= 0.276 CD=0.00738 CM=-0.1845	S TURB S SEP CD 1.0033 0.0044 0.0075 0.9564 0.0000 0.0046 CL= 0.273 CD=0.01212 CM=-0.1838	S TURB S SEP CD 0.8404 0.0037 0.0071 1.0015 0.0000 0.0049* CL= 0.274 CD=0.01193 CM=-0.1839
-3.00	S TURB S SEP CD UPPER 0.4818 0.0035 0.0050 LOWER 0.6425 0.0000 0.0027* TOTAL CL= 0.384 CD=0.00771 CM=-0.1860	S TURB S SEP CD 1.0034 0.0064 0.0081 0.9564 0.0000 0.0042 CL= 0.381 CD=0.01227 CM=-0.1853	S TURB S SEP CD 0.8631 0.0057 0.0076 0.9849 0.0000 0.0043 CL= 0.382 CD=0.01194 CM=-0.1854
-2.00	S TURB S SEP CD UPPER 0.5118 0.0052 0.0054 LOWER 0.6372 0.0000 0.0026* TOTAL CL= 0.492 CD=0.00798 CM=-0.1876	S TURB S SEP CD 1.0034 0.0083 0.0087 0.9564 0.0000 0.0038 CL= 0.489 CD=0.01251 CM=-0.1867	S TURB S SEP CD 0.8902 0.0076 0.0082 0.9601 0.0000 0.0039 CL= 0.489 CD=0.01210 CM=-0.1869
-1.00	S TURB S SEP CD UPPER 0.5316 0.0067 0.0058 LOWER 0.6321 0.0000 0.0024* TOTAL CL= 0.600 CD=0.00823 CM=-0.1891	S TURB S SEP CD 1.0034 0.0103 0.0093 0.9564 0.0000 0.0035 CL= 0.596 CD=0.01286 CM=-0.1881	S TURB S SEP CD 0.9104 0.0096 0.0089 0.9341 0.0000 0.0035 CL= 0.597 CD=0.01239 CM=-0.1883
0.00	S TURB S SEP CD UPPER 0.5449 0.0082 0.0062 LOWER 0.6270 0.0000 0.0023* TOTAL CL= 0.708 CD=0.00846 CM=-0.1906	S TURB S SEP CD 1.0034 0.0125 0.0100 0.9564 0.0000 0.0033 CL= 0.703 CD=0.01328 CM=-0.1894	S TURB S SEP CD 0.9326 0.0122 0.0097 0.9043 0.0000 0.0032 CL= 0.703 CD=0.01287 CM=-0.1895
1.00	S TURB S SEP CD UPPER 0.5542 0.0096 0.0066 LOWER 0.6215 0.0000 0.0021* TOTAL CL= 0.816 CD=0.00869 CM=-0.1921	S TURB S SEP CD 1.0034 0.0150 0.0108 0.9564 0.0000 0.0030 CL= 0.809 CD=0.01379 CM=-0.1906	S TURB S SEP CD 0.9527 0.0146 0.0105 0.8803 0.0000 0.0029 CL= 0.810 CD=0.01340 CM=-0.1907
2.00	S TURB S SEP CD UPPER 0.5626 0.0112 0.0069* LOWER 0.6151 0.0000 0.0020* TOTAL CL= 0.923 CD=0.00893 CM=-0.1936	S TURB S SEP CD 1.0034 0.0176 0.0116 0.9564 0.0000 0.0028 CL= 0.915 CD=0.01440 CM=-0.1916	S TURB S SEP CD 0.9705 0.0173 0.0114 0.7453 0.0000 0.0024 CL= 0.915 CD=0.01382 CM=-0.1917
3.00	S TURB S SEP CD UPPER 0.5712 0.0129 0.0074* LOWER 0.6063 0.0000 0.0019* TOTAL CL= 1.030 CD=0.00921 CM=-0.1949	S TURB S SEP CD 1.0034 0.0204 0.0126 0.9564 0.0000 0.0025 CL= 1.020 CD=0.01512 CM=-0.1925	S TURB S SEP CD 0.9881 0.0202 0.0124 0.7373 0.0000 0.0022 CL= 1.021 CD=0.01468 CM=-0.1926
4.00	S TURB S SEP CD UPPER 0.5812 0.0147 0.0078 LOWER 0.5934 0.0000 0.0017* TOTAL CL= 1.137 CD=0.00954 CM=-0.1961	S TURB S SEP CD 1.0034 0.0235 0.0136 0.9564 0.0000 0.0023 CL= 1.125 CD=0.01594 CM=-0.1933	S TURB S SEP CD 1.0010 0.0235 0.0136 0.7283 0.0000 0.0021 CL= 1.125 CD=0.01565 CM=-0.1933
5.00	S TURB S SEP CD UPPER 0.5939 0.0167 0.0084 LOWER 0.5786 0.0000 0.0016* TOTAL CL= 1.243 CD=0.00995 CM=-0.1972	S TURB S SEP CD 1.0034 0.0270 0.0147 0.9564 0.0000 0.0022 CL= 1.229 CD=0.01688 CM=-0.1938	S TURB S SEP CD 1.0131 0.0272 0.0149 0.7179 0.0000 0.0019 CL= 1.228 CD=0.01679 CM=-0.1937
6.00	S TURB S SEP CD UPPER 0.6099 0.0190 0.0090 LOWER 0.5621 0.0000 0.0015* TOTAL CL= 1.349 CD=0.01048 CM=-0.1981	S TURB S SEP CD 1.0034 0.0309 0.0160 0.9564 0.0000 0.0020 CL= 1.331 CD=0.01795 CM=-0.1941	S TURB S SEP CD 1.0259 0.0317 0.0164 0.7060 0.0000 0.0018 CL= 1.330 CD=0.01820 CM=-0.1938
7.00	S TURB S SEP CD UPPER 0.9914 0.0347 0.0170 LOWER 0.5478 0.0000 0.0014* TOTAL CL= 1.434 CD=0.01836 CM=-0.1943	S TURB S SEP CD 1.0034 0.0353 0.0173* 0.9564 0.0000 0.0018 CL= 1.433 CD=0.01917 CM=-0.1941	S TURB S SEP CD 1.0335 0.0368 0.0182* 0.6915 0.0000 0.0016 CL= 1.431 CD=0.01983 CM=-0.1936

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEC.)	R= 1000000 MU=3.0	R= 1000000 MU=1.3	R= 1000000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0324 0.0422 0.0200*	1.0324 0.0422 0.0200*	1.0367 0.0425 0.0201*
	LOWER 0.5341 0.0000 0.0013*	0.9564 0.0000 0.0017	0.6765 0.0000 0.0015
	TOTAL CL= 1.530 CD=0.02123	CL= 1.530 CD=0.02166	CL= 1.530 CD=0.02163
	CM=-0.1931	CM=-0.1931	CM=-0.1930
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0368 0.0498 0.0223*	1.0368 0.0498 0.0223*	1.0370 0.0498 0.0223*
	LOWER 0.5195 0.0000 0.0012*	0.9564 0.0000 0.0016	0.6655 0.0000 0.0014
	TOTAL CL= 1.625 CD=0.02345	CL= 1.625 CD=0.02384	CL= 1.625 CD=0.02369
	CM=-0.1918	CM=-0.1918	CM=-0.1918
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0370 0.0588 0.0247*	1.0370 0.0588 0.0247*	1.0371 0.0588 0.0247*
	LOWER 0.4949 0.0000 0.0011	0.9303 0.0000 0.0014	0.6571 0.0000 0.0013
	TOTAL CL= 1.717 CD=0.02577	CL= 1.717 CD=0.02614	CL= 1.717 CD=0.02602
	CM=-0.1898	CM=-0.1898	CM=-0.1898

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA (DEG.)	R= 1500000 MU=3.0	R= 1500000 MU=1.3	R= 1500000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.0876 0.0216 0.0018 LOWER 1.0097 0.2765 0.0066* TOTAL CL=-0.069 CD=0.00834 CM=-0.1763	S TURB S SEP CD 1.0022 0.0000 0.0057 1.0097 0.2765 0.0066* CL=-0.053 CD=0.01226 CM=-0.1787	S TURB S SEP CD 0.8173 0.0000 0.0054 1.0098 0.2777 0.0066* CL=-0.053 CD=0.01204 CM=-0.1787
-6.00	S TURB S SEP CD UPPER 0.3395 0.0000 0.0031 LOWER 1.0096 0.2236 0.0058* TOTAL CL= 0.057 CD=0.00895 CM=-0.1807	S TURB S SEP CD 1.0022 0.0000 0.0061 1.0096 0.2236 0.0058* CL= 0.057 CD=0.01187 CM=-0.1807	S TURB S SEP CD 0.8374 0.0000 0.0058 1.0097 0.2238 0.0058* CL= 0.057 CD=0.01162 CM=-0.1807
-5.00	S TURB S SEP CD UPPER 0.4292 0.0000 0.0038 LOWER 1.0093 0.1526 0.0051* TOTAL CL= 0.167 CD=0.00891 CM=-0.1828	S TURB S SEP CD 1.0022 0.0000 0.0065 1.0093 0.1526 0.0051* CL= 0.167 CD=0.01162 CM=-0.1828	S TURB S SEP CD 0.8586 0.0000 0.0062 1.0094 0.1527 0.0051* CL= 0.167 CD=0.01136 CM=-0.1828
-4.00	S TURB S SEP CD UPPER 0.4801 0.0000 0.0043 LOWER 0.6556 0.0000 0.0027 TOTAL CL= 0.277 CD=0.00701 CM=-0.1848	S TURB S SEP CD 1.0033 0.0007 0.0070 0.9564 0.0000 0.0043 CL= 0.277 CD=0.01131 CM=-0.1846	S TURB S SEP CD 0.8827 0.0005 0.0068 1.0036 0.0000 0.0046* CL= 0.277 CD=0.01134 CM=-0.1847
-3.00	S TURB S SEP CD UPPER 0.5117 0.0005 0.0047 LOWER 0.6474 0.0000 0.0025* TOTAL CL= 0.387 CD=0.00725 CM=-0.1867	S TURB S SEP CD 1.0034 0.0037 0.0075 0.9564 0.0000 0.0039 CL= 0.384 CD=0.01146 CM=-0.1859	S TURB S SEP CD 0.8999 0.0034 0.0073 0.9916 0.0000 0.0041 CL= 0.384 CD=0.01136 CM=-0.1860
-2.00	S TURB S SEP CD UPPER 0.5327 0.0027 0.0051 LOWER 0.6407 0.0000 0.0024* TOTAL CL= 0.494 CD=0.00745 CM=-0.1882	S TURB S SEP CD 1.0034 0.0058 0.0081 0.9564 0.0000 0.0036 CL= 0.491 CD=0.01170 CM=-0.1874	S TURB S SEP CD 0.9200 0.0056 0.0078 0.9721 0.0000 0.0037 CL= 0.491 CD=0.01150 CM=-0.1874
-1.00	S TURB S SEP CD UPPER 0.5457 0.0044 0.0054 LOWER 0.6346 0.0000 0.0022* TOTAL CL= 0.602 CD=0.00762 CM=-0.1897	S TURB S SEP CD 1.0034 0.0079 0.0087 0.9564 0.0000 0.0033 CL= 0.599 CD=0.01201 CM=-0.1888	S TURB S SEP CD 0.9373 0.0076 0.0084 0.9508 0.0000 0.0033 CL= 0.599 CD=0.01177 CM=-0.1889
0.00	S TURB S SEP CD UPPER 0.5549 0.0059 0.0057 LOWER 0.6287 0.0000 0.0021* TOTAL CL= 0.710 CD=0.00780 CM=-0.1913	S TURB S SEP CD 1.0034 0.0100 0.0093 0.9564 0.0000 0.0031 CL= 0.706 CD=0.01240 CM=-0.1901	S TURB S SEP CD 0.9553 0.0098 0.0091 0.9313 0.0000 0.0030 CL= 0.706 CD=0.01216 CM=-0.1902
1.00	S TURB S SEP CD UPPER 0.5630 0.0074 0.0060 LOWER 0.6226 0.0000 0.0019* TOTAL CL= 0.818 CD=0.00799 CM=-0.1928	S TURB S SEP CD 1.0034 0.0123 0.0101 0.9564 0.0000 0.0028 CL= 0.812 CD=0.01288 CM=-0.1913	S TURB S SEP CD 0.9698 0.0121 0.0099 0.9048 0.0000 0.0028 CL= 0.813 CD=0.01262 CM=-0.1914
2.00	S TURB S SEP CD UPPER 0.5712 0.0089 0.0064 LOWER 0.6154 0.0000 0.0018* TOTAL CL= 0.926 CD=0.00821 CM=-0.1942	S TURB S SEP CD 1.0034 0.0149 0.0108 0.9564 0.0000 0.0026 CL= 0.918 CD=0.01343 CM=-0.1924	S TURB S SEP CD 0.9853 0.0148 0.0107 0.8846 0.0000 0.0025 CL= 0.919 CD=0.01323 CM=-0.1925
3.00	S TURB S SEP CD UPPER 0.5805 0.0105 0.0068 LOWER 0.6063 0.0000 0.0017* TOTAL CL= 1.033 CD=0.00848 CM=-0.1956	S TURB S SEP CD 1.0034 0.0177 0.0117 0.9564 0.0000 0.0024 CL= 1.024 CD=0.01408 CM=-0.1934	S TURB S SEP CD 0.9986 0.0176 0.0116 0.7592 0.0000 0.0021 CL= 1.024 CD=0.01377 CM=-0.1934
4.00	S TURB S SEP CD UPPER 0.5921 0.0123 0.0072 LOWER 0.5934 0.0000 0.0016* TOTAL CL= 1.140 CD=0.00879 CM=-0.1969	S TURB S SEP CD 1.0034 0.0210 0.0127 0.9564 0.0000 0.0022 CL= 1.128 CD=0.01492 CM=-0.1941	S TURB S SEP CD 1.0096 0.0211 0.0128 0.7507 0.0000 0.0020 CL= 1.128 CD=0.01476 CM=-0.1940
5.00	S TURB S SEP CD UPPER 0.6053 0.0142 0.0077 LOWER 0.5786 0.0000 0.0015 TOTAL CL= 1.247 CD=0.00917 CM=-0.1981	S TURB S SEP CD 1.0034 0.0243 0.0137 0.9564 0.0000 0.0020 CL= 1.233 CD=0.01578 CM=-0.1947	S TURB S SEP CD 1.0187 0.0247 0.0140 0.7423 0.0000 0.0018 CL= 1.232 CD=0.01581 CM=-0.1945
6.00	S TURB S SEP CD UPPER 0.6247 0.0165 0.0084 LOWER 0.5621 0.0000 0.0013* TOTAL CL= 1.353 CD=0.00970 CM=-0.1990	S TURB S SEP CD 1.0034 0.0280 0.0149 0.9564 0.0000 0.0019 CL= 1.336 CD=0.01675 CM=-0.1950	S TURB S SEP CD 1.0312 0.0290 0.0154 0.7332 0.0000 0.0017 CL= 1.334 CD=0.01715 CM=-0.1947
7.00	S TURB S SEP CD UPPER 0.9914 0.0316 0.0158 LOWER 0.5478 0.0000 0.0012* TOTAL CL= 1.439 CD=0.01702 CM=-0.1954	S TURB S SEP CD 1.0034 0.0321 0.0161 0.9564 0.0000 0.0017 CL= 1.438 CD=0.01784 CM=-0.1952	S TURB S SEP CD 1.0355 0.0338 0.0170 0.7221 0.0000 0.0016 CL= 1.435 CD=0.01861 CM=-0.1946

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 1500000 MU=3.0	R= 1500000 MU=1.3	R= 1500000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0324 0.0389 0.0186*	1.0324 0.0389 0.0186*	1.0369 0.0393 0.0188*
	LOWER 0.5341 0.0000 0.0012*	0.9564 0.0000 0.0016	0.7090 0.0000 0.0015
	TOTAL CL= 1.535 CD=0.01980	CL= 1.535 CD=0.02024	CL= 1.535 CD=0.02029
	CM=-0.1943	CM=-0.1943	CM=-0.1942
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0368 0.0457 0.0208*	1.0368 0.0457 0.0208*	1.0371 0.0458 0.0208*
	LOWER 0.5195 0.0000 0.0011	0.9564 0.0000 0.0015	0.6956 0.0000 0.0013
	TOTAL CL= 1.632 CD=0.02188	CL= 1.632 CD=0.02228	CL= 1.632 CD=0.02217
	CM=-0.1932	CM=-0.1932	CM=-0.1932
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0370 0.0542 0.0231*	1.0370 0.0542 0.0231*	1.0372 0.0543 0.0231*
	LOWER 0.4949 0.0000 0.0010	0.9303 0.0000 0.0014	0.6795 0.0000 0.0012
	TOTAL CL= 1.725 CD=0.02406	CL= 1.725 CD=0.02444	CL= 1.725 CD=0.02435
	CM=-0.1914	CM=-0.1914	CM=-0.1914

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEC.)	R= 2000000 MU=3.0	R= 2000000 MU=1.3	R= 2000000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.2873 0.0000 0.0025 LOWER 1.0097 0.2571 0.0063* TOTAL CL=-0.053 CD=0.00885 CM=-0.1787	S TURB S SEP CD 1.0022 0.0000 0.0055 1.0097 0.2571 0.0063* CL=-0.053 CD=0.01178 CM=-0.1787	S TURB S SEP CD 0.8474 0.0000 0.0053 1.0098 0.2579 0.0063* CL=-0.053 CD=0.01161 CM=-0.1787
-6.00	S TURB S SEP CD UPPER 0.4107 0.0000 0.0033 LOWER 1.0096 0.1985 0.0056* TOTAL CL= 0.057 CD=0.00888 CM=-0.1807	S TURB S SEP CD 1.0022 0.0000 0.0058 1.0096 0.1985 0.0056* CL= 0.057 CD=0.01139 CM=-0.1807	S TURB S SEP CD 0.8652 0.0000 0.0056 1.0097 0.1988 0.0056* CL= 0.057 CD=0.01121 CM=-0.1807
-5.00	S TURB S SEP CD UPPER 0.4698 0.0000 0.0038 LOWER 1.0093 0.0000 0.0049* TOTAL CL= 0.167 CD=0.00874 CM=-0.1828	S TURB S SEP CD 1.0022 0.0000 0.0062 1.0093 0.0000 0.0049* CL= 0.167 CD=0.01114 CM=-0.1828	S TURB S SEP CD 0.8858 0.0000 0.0060 1.0095 0.1062 0.0049* CL= 0.167 CD=0.01096 CM=-0.1828
-4.00	S TURB S SEP CD UPPER 0.5062 0.0000 0.0042 LOWER 0.6613 0.0000 0.0026 TOTAL CL= 0.277 CD=0.00676 CM=-0.1848	S TURB S SEP CD 1.0033 0.0000 0.0067 0.9564 0.0000 0.0041 CL= 0.277 CD=0.01078 CM=-0.1848	S TURB S SEP CD 0.9038 0.0000 0.0065 1.0059 0.0000 0.0044 CL= 0.277 CD=0.01088 CM=-0.1848
-3.00	S TURB S SEP CD UPPER 0.5297 0.0000 0.0045 LOWER 0.6518 0.0000 0.0024* TOTAL CL= 0.387 CD=0.00693 CM=-0.1868	S TURB S SEP CD 1.0034 0.0014 0.0072 0.9564 0.0000 0.0038 CL= 0.386 CD=0.01096 CM=-0.1865	S TURB S SEP CD 0.9204 0.0011 0.0070 0.9961 0.0000 0.0039 CL= 0.386 CD=0.01094 CM=-0.1866
-2.00	S TURB S SEP CD UPPER 0.5443 0.0006 0.0049 LOWER 0.6445 0.0000 0.0022* TOTAL CL= 0.497 CD=0.00710 CM=-0.1887	S TURB S SEP CD 1.0034 0.0041 0.0077 0.9564 0.0000 0.0035 CL= 0.493 CD=0.01119 CM=-0.1878	S TURB S SEP CD 0.9377 0.0039 0.0075 0.9792 0.0000 0.0035 CL= 0.493 CD=0.01110 CM=-0.1879
-1.00	S TURB S SEP CD UPPER 0.5537 0.0026 0.0051 LOWER 0.6382 0.0000 0.0021* TOTAL CL= 0.604 CD=0.00724 CM=-0.1902	S TURB S SEP CD 1.0034 0.0063 0.0083 0.9564 0.0000 0.0032 CL= 0.600 CD=0.01149 CM=-0.1892	S TURB S SEP CD 0.9529 0.0061 0.0081 0.9607 0.0000 0.0032 CL= 0.601 CD=0.01134 CM=-0.1893
0.00	S TURB S SEP CD UPPER 0.5618 0.0043 0.0054 LOWER 0.6324 0.0000 0.0020* TOTAL CL= 0.712 CD=0.00740 CM=-0.1917	S TURB S SEP CD 1.0034 0.0085 0.0089 0.9564 0.0000 0.0029 CL= 0.708 CD=0.01187 CM=-0.1906	S TURB S SEP CD 0.9669 0.0083 0.0088 0.9427 0.0000 0.0029 CL= 0.708 CD=0.01169 CM=-0.1906
1.00	S TURB S SEP CD UPPER 0.5697 0.0058 0.0057 LOWER 0.6265 0.0000 0.0018* TOTAL CL= 0.820 CD=0.00758 CM=-0.1933	S TURB S SEP CD 1.0034 0.0107 0.0096 0.9564 0.0000 0.0027 CL= 0.814 CD=0.01231 CM=-0.1918	S TURB S SEP CD 0.9811 0.0106 0.0095 0.9210 0.0000 0.0027 CL= 0.814 CD=0.01215 CM=-0.1919
2.00	S TURB S SEP CD UPPER 0.5784 0.0074 0.0061 LOWER 0.6199 0.0000 0.0017 TOTAL CL= 0.928 CD=0.00779 CM=-0.1947	S TURB S SEP CD 1.0034 0.0132 0.0103 0.9564 0.0000 0.0025 CL= 0.921 CD=0.01284 CM=-0.1929	S TURB S SEP CD 0.9933 0.0131 0.0103 0.8982 0.0000 0.0024 CL= 0.921 CD=0.01271 CM=-0.1930
3.00	S TURB S SEP CD UPPER 0.5889 0.0089 0.0064 LOWER 0.6119 0.0000 0.0016* TOTAL CL= 1.035 CD=0.00805 CM=-0.1961	S TURB S SEP CD 1.0034 0.0160 0.0111 0.9564 0.0000 0.0023 CL= 1.026 CD=0.01345 CM=-0.1939	S TURB S SEP CD 1.0039 0.0160 0.0112 0.8823 0.0000 0.0022 CL= 1.026 CD=0.01340 CM=-0.1939
4.00	S TURB S SEP CD UPPER 0.6006 0.0106 0.0069 LOWER 0.5998 0.0000 0.0015* TOTAL CL= 1.143 CD=0.00835 CM=-0.1974	S TURB S SEP CD 1.0034 0.0189 0.0120 0.9564 0.0000 0.0021 CL= 1.131 CD=0.01416 CM=-0.1947	S TURB S SEP CD 1.0146 0.0191 0.0122 0.7678 0.0000 0.0019 CL= 1.131 CD=0.01408 CM=-0.1947
5.00	S TURB S SEP CD UPPER 0.6150 0.0126 0.0073 LOWER 0.5850 0.0000 0.0014 TOTAL CL= 1.249 CD=0.00873 CM=-0.1986	S TURB S SEP CD 1.0034 0.0221 0.0130 0.9564 0.0000 0.0020 CL= 1.236 CD=0.01495 CM=-0.1954	S TURB S SEP CD 1.0235 0.0226 0.0133 0.7589 0.0000 0.0018 CL= 1.235 CD=0.01508 CM=-0.1953
6.00	S TURB S SEP CD UPPER 0.8290 0.0200 0.0109 LOWER 0.5682 0.0000 0.0013 TOTAL CL= 1.348 CD=0.01215 CM=-0.1978	S TURB S SEP CD 1.0034 0.0256 0.0140 0.9564 0.0000 0.0018 CL= 1.339 CD=0.01586 CM=-0.1959	S TURB S SEP CD 1.0328 0.0270 0.0148 0.7501 0.0000 0.0017 CL= 1.337 CD=0.01642 CM=-0.1954
7.00	S TURB S SEP CD UPPER 0.9914 0.0289 0.0149 LOWER 0.5531 0.0000 0.0012* TOTAL CL= 1.443 CD=0.01606 CM=-0.1963	S TURB S SEP CD 1.0034 0.0295 0.0152 0.9564 0.0000 0.0017 CL= 1.442 CD=0.01687 CM=-0.1961	S TURB S SEP CD 1.0366 0.0317 0.0163 0.7414 0.0000 0.0015 CL= 1.439 CD=0.01781 CM=-0.1953

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEC.)	R= 2000000 MU=3.0	R= 2000000 MU=1.3	R= 2000000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0324 0.0366 0.0178*	1.0324 0.0366 0.0178*	1.0371 0.0370 0.0180*
	LOWER 0.5386 0.0000 0.0011	0.9564 0.0000 0.0015	0.7309 0.0000 0.0014
	TOTAL CL= 1.539 CD=0.01885	CL= 1.539 CD=0.01930	CL= 1.538 CD=0.01939
	CM=-0.1951	CM=-0.1951	CM=-0.1950
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0368 0.0430 0.0198*	1.0368 0.0430 0.0198*	1.0372 0.0431 0.0199*
	LOWER 0.5242 0.0000 0.0010	0.9564 0.0000 0.0014	0.7181 0.0000 0.0013
	TOTAL CL= 1.636 CD=0.02085	CL= 1.636 CD=0.02125	CL= 1.636 CD=0.02117
	CM=-0.1942	CM=-0.1942	CM=-0.1941
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0370 0.0510 0.0220*	1.0370 0.0510 0.0220*	1.0373 0.0512 0.0220*
	LOWER 0.5046 0.0000 0.0009	0.9303 0.0000 0.0013	0.7043 0.0000 0.0012
	TOTAL CL= 1.730 CD=0.02292	CL= 1.730 CD=0.02330	CL= 1.730 CD=0.02323
	CM=-0.1926	CM=-0.1926	CM=-0.1925

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEC.)	R= 2500000 MU=3.0	R= 2500000 MU=1.3	R= 2500000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.3774 0.0000 0.0029 LOWER 1.0097 0.2400 0.0061* TOTAL CL=-0.053 CD=0.00897 CM=-0.1787	S TURB S SEP CD 1.0022 0.0000 0.0053 1.0097 0.2400 0.0061* CL=-0.053 CD=0.01140 CM=-0.1787	S TURB S SEP CD 0.8675 0.0000 0.0052 1.0099 0.2408 0.0061* CL=-0.053 CD=0.01127 CM=-0.1787
-6.00	S TURB S SEP CD UPPER 0.4508 0.0000 0.0034 LOWER 1.0096 0.1773 0.0054* TOTAL CL= 0.057 CD=0.00876 CM=-0.1807	S TURB S SEP CD 1.0022 0.0000 0.0057 1.0096 0.1773 0.0054* CL= 0.057 CD=0.01102 CM=-0.1807	S TURB S SEP CD 0.8852 0.0000 0.0055 1.0098 0.1777 0.0054* CL= 0.057 CD=0.01089 CM=-0.1807
-5.00	S TURB S SEP CD UPPER 0.4953 0.0000 0.0038 LOWER 1.0093 0.0000 0.0048* TOTAL CL= 0.167 CD=0.00857 CM=-0.1828	S TURB S SEP CD 1.0022 0.0000 0.0060 1.0093 0.0000 0.0048* CL= 0.167 CD=0.01080 CM=-0.1828	S TURB S SEP CD 0.9021 0.0000 0.0059 1.0096 0.0000 0.0048* CL= 0.167 CD=0.01067 CM=-0.1828
-4.00	S TURB S SEP CD UPPER 0.5234 0.0000 0.0041 LOWER 0.6663 0.0000 0.0025 TOTAL CL= 0.277 CD=0.00660 CM=-0.1848	S TURB S SEP CD 1.0033 0.0000 0.0064 0.9564 0.0000 0.0040 CL= 0.277 CD=0.01038 CM=-0.1848	S TURB S SEP CD 0.9183 0.0000 0.0063 1.0068 0.0000 0.0043 CL= 0.277 CD=0.01053 CM=-0.1848
-3.00	S TURB S SEP CD UPPER 0.5410 0.0000 0.0044 LOWER 0.6560 0.0000 0.0023* TOTAL CL= 0.387 CD=0.00669 CM=-0.1868	S TURB S SEP CD 1.0034 0.0000 0.0069 0.9564 0.0000 0.0036 CL= 0.387 CD=0.01058 CM=-0.1868	S TURB S SEP CD 0.9342 0.0000 0.0068 0.9982 0.0000 0.0038 CL= 0.387 CD=0.01061 CM=-0.1868
-2.00	S TURB S SEP CD UPPER 0.5514 0.0000 0.0047 LOWER 0.6479 0.0000 0.0022* TOTAL CL= 0.497 CD=0.00682 CM=-0.1889	S TURB S SEP CD 1.0034 0.0025 0.0075 0.9564 0.0000 0.0034 CL= 0.495 CD=0.01082 CM=-0.1882	S TURB S SEP CD 0.9487 0.0024 0.0073 0.9840 0.0000 0.0035 CL= 0.495 CD=0.01077 CM=-0.1883
-1.00	S TURB S SEP CD UPPER 0.5596 0.0010 0.0049 LOWER 0.6414 0.0000 0.0020* TOTAL CL= 0.606 CD=0.00696 CM=-0.1907	S TURB S SEP CD 1.0034 0.0050 0.0080 0.9564 0.0000 0.0031 CL= 0.602 CD=0.01111 CM=-0.1896	S TURB S SEP CD 0.9624 0.0048 0.0079 0.9671 0.0000 0.0031 CL= 0.602 CD=0.01100 CM=-0.1896
0.00	S TURB S SEP CD UPPER 0.5674 0.0029 0.0052 LOWER 0.6355 0.0000 0.0019* TOTAL CL= 0.714 CD=0.00711 CM=-0.1921	S TURB S SEP CD 1.0034 0.0072 0.0086 0.9564 0.0000 0.0029 CL= 0.709 CD=0.01146 CM=-0.1909	S TURB S SEP CD 0.9751 0.0071 0.0085 0.9505 0.0000 0.0028 CL= 0.709 CD=0.01134 CM=-0.1910
1.00	S TURB S SEP CD UPPER 0.5754 0.0046 0.0055 LOWER 0.6297 0.0000 0.0018 TOTAL CL= 0.822 CD=0.00729 CM=-0.1936	S TURB S SEP CD 1.0034 0.0095 0.0093 0.9564 0.0000 0.0026 CL= 0.816 CD=0.01189 CM=-0.1922	S TURB S SEP CD 0.9877 0.0094 0.0092 0.9321 0.0000 0.0026 CL= 0.816 CD=0.01178 CM=-0.1922
2.00	S TURB S SEP CD UPPER 0.5851 0.0061 0.0058 LOWER 0.6235 0.0000 0.0017 TOTAL CL= 0.930 CD=0.00750 CM=-0.1951	S TURB S SEP CD 1.0034 0.0119 0.0100 0.9564 0.0000 0.0024 CL= 0.922 CD=0.01240 CM=-0.1933	S TURB S SEP CD 0.9988 0.0119 0.0099 0.9114 0.0000 0.0024 CL= 0.922 CD=0.01232 CM=-0.1934
3.00	S TURB S SEP CD UPPER 0.5959 0.0077 0.0062 LOWER 0.6163 0.0000 0.0016 TOTAL CL= 1.037 CD=0.00776 CM=-0.1965	S TURB S SEP CD 1.0034 0.0146 0.0107 0.9564 0.0000 0.0022 CL= 1.028 CD=0.01299 CM=-0.1943	S TURB S SEP CD 1.0079 0.0147 0.0108 0.8935 0.0000 0.0022 CL= 1.028 CD=0.01297 CM=-0.1943
4.00	S TURB S SEP CD UPPER 0.6079 0.0094 0.0066 LOWER 0.6063 0.0000 0.0015* TOTAL CL= 1.144 CD=0.00806 CM=-0.1978	S TURB S SEP CD 1.0034 0.0175 0.0116 0.9564 0.0000 0.0021 CL= 1.133 CD=0.01366 CM=-0.1952	S TURB S SEP CD 1.0173 0.0177 0.0118 0.7809 0.0000 0.0019 CL= 1.133 CD=0.01363 CM=-0.1951
5.00	S TURB S SEP CD UPPER 0.6242 0.0113 0.0071 LOWER 0.5921 0.0000 0.0013 TOTAL CL= 1.251 CD=0.00844 CM=-0.1991	S TURB S SEP CD 1.0034 0.0206 0.0125 0.9564 0.0000 0.0019 CL= 1.238 CD=0.01441 CM=-0.1959	S TURB S SEP CD 1.0267 0.0212 0.0129 0.7727 0.0000 0.0017 CL= 1.237 CD=0.01461 CM=-0.1957
6.00	S TURB S SEP CD UPPER 0.8948 0.0205 0.0115 LOWER 0.5754 0.0000 0.0012 TOTAL CL= 1.347 CD=0.01271 CM=-0.1976	S TURB S SEP CD 1.0034 0.0240 0.0135 0.9564 0.0000 0.0018 CL= 1.342 CD=0.01527 CM=-0.1964	S TURB S SEP CD 1.0338 0.0251 0.0142 0.7645 0.0000 0.0016 CL= 1.340 CD=0.01578 CM=-0.1960
7.00	S TURB S SEP CD UPPER 0.9914 0.0272 0.0143 LOWER 0.5602 0.0000 0.0011* TOTAL CL= 1.445 CD=0.01544 CM=-0.1969	S TURB S SEP CD 1.0034 0.0278 0.0146 0.9564 0.0000 0.0016 CL= 1.445 CD=0.01624 CM=-0.1967	S TURB S SEP CD 1.0368 0.0296 0.0156 0.7545 0.0000 0.0015 CL= 1.442 CD=0.01710 CM=-0.1961

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEG.)	R= 2500000 MU=3.0	R= 2500000 MU=1.3	R= 2500000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0324 0.0347 0.0171*	1.0324 0.0347 0.0171*	1.0371 0.0352 0.0173*
	LOWER 0.5447 0.0000 0.0011	0.9564 0.0000 0.0015	0.7454 0.0000 0.0014
	TOTAL CL= 1.542 CD=0.01814	CL= 1.542 CD=0.01858	CL= 1.541 CD=0.01871
	CM=-0.1958	CM=-0.1958	CM=-0.1956
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0368 0.0410 0.0191*	1.0368 0.0410 0.0191*	1.0373 0.0411 0.0191*
	LOWER 0.5306 0.0000 0.0010	0.9564 0.0000 0.0014	0.7353 0.0000 0.0013
	TOTAL CL= 1.640 CD=0.02009	CL= 1.640 CD=0.02048	CL= 1.640 CD=0.02043
	CM=-0.1949	CM=-0.1949	CM=-0.1949
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0370 0.0485 0.0212*	1.0370 0.0485 0.0212*	1.0374 0.0487 0.0212*
	LOWER 0.5142 0.0000 0.0009	0.9303 0.0000 0.0013	0.7226 0.0000 0.0012
	TOTAL CL= 1.735 CD=0.02208	CL= 1.735 CD=0.02245	CL= 1.734 CD=0.02241
	CM=-0.1935	CM=-0.1935	CM=-0.1934

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA (DEG.)	R= 3000000 MU=3.0	R= 3000000 MU=1.3	R= 3000000 MU=9.0
-7.00	S TURB S SEP CD UPPER 0.4215 0.0000 0.0030 LOWER 1.0097 0.2251 0.0059* TOTAL CL=-0.053 CD=0.00892 CM=-0.1787	S TURB S SEP CD 1.0022 0.0000 0.0052 1.0097 0.2251 0.0059* CL=-0.053 CD=0.01109 CM=-0.1787	S TURB S SEP CD 0.8823 0.0000 0.0051 1.0099 0.2260 0.0059* CL=-0.053 CD=0.01100 CM=-0.1787
-6.00	S TURB S SEP CD UPPER 0.4777 0.0000 0.0034 LOWER 1.0096 0.1601 0.0052* TOTAL CL= 0.057 CD=0.00864 CM=-0.1807	S TURB S SEP CD 1.0022 0.0000 0.0055 1.0096 0.1601 0.0052* CL= 0.057 CD=0.01073 CM=-0.1807	S TURB S SEP CD 0.8984 0.0000 0.0054 1.0098 0.1607 0.0052* CL= 0.057 CD=0.01062 CM=-0.1807
-5.00	S TURB S SEP CD UPPER 0.5129 0.0000 0.0038 LOWER 1.0093 0.0000 0.0047* TOTAL CL= 0.167 CD=0.00842 CM=-0.1828	S TURB S SEP CD 1.0022 0.0000 0.0059 1.0093 0.0000 0.0047* CL= 0.167 CD=0.01053 CM=-0.1828	S TURB S SEP CD 0.9132 0.0000 0.0058 1.0096 0.0000 0.0047* CL= 0.167 CD=0.01042 CM=-0.1828
-4.00	S TURB S SEP CD UPPER 0.5354 0.0000 0.0040 LOWER 0.6711 0.0000 0.0024 TOTAL CL= 0.277 CD=0.00648 CM=-0.1848	S TURB S SEP CD 1.0033 0.0000 0.0063 0.9564 0.0000 0.0039 CL= 0.277 CD=0.01011 CM=-0.1848	S TURB S SEP CD 0.9286 0.0000 0.0061 1.0076 0.0000 0.0042 CL= 0.277 CD=0.01030 CM=-0.1848
-3.00	S TURB S SEP CD UPPER 0.5479 0.0000 0.0043 LOWER 0.6601 0.0000 0.0022 TOTAL CL= 0.387 CD=0.00652 CM=-0.1868	S TURB S SEP CD 1.0034 0.0000 0.0067 0.9564 0.0000 0.0035 CL= 0.387 CD=0.01025 CM=-0.1868	S TURB S SEP CD 0.9435 0.0000 0.0066 0.9997 0.0000 0.0037 CL= 0.387 CD=0.01032 CM=-0.1868
-2.00	S TURB S SEP CD UPPER 0.5567 0.0000 0.0045 LOWER 0.6511 0.0000 0.0021* TOTAL CL= 0.497 CD=0.00660 CM=-0.1889	S TURB S SEP CD 1.0034 0.0010 0.0072 0.9564 0.0000 0.0033 CL= 0.496 CD=0.01052 CM=-0.1886	S TURB S SEP CD 0.9567 0.0009 0.0071 0.9872 0.0000 0.0034 CL= 0.496 CD=0.01051 CM=-0.1887
-1.00	S TURB S SEP CD UPPER 0.5645 0.0000 0.0048 LOWER 0.6441 0.0000 0.0020* TOTAL CL= 0.607 CD=0.00675 CM=-0.1909	S TURB S SEP CD 1.0034 0.0038 0.0078 0.9564 0.0000 0.0030 CL= 0.603 CD=0.01080 CM=-0.1899	S TURB S SEP CD 0.9689 0.0037 0.0077 0.9718 0.0000 0.0031 CL= 0.603 CD=0.01073 CM=-0.1899
0.00	S TURB S SEP CD UPPER 0.5722 0.0016 0.0051 LOWER 0.6382 0.0000 0.0018* TOTAL CL= 0.715 CD=0.00690 CM=-0.1925	S TURB S SEP CD 1.0034 0.0061 0.0084 0.9564 0.0000 0.0028 CL= 0.710 CD=0.01114 CM=-0.1912	S TURB S SEP CD 0.9816 0.0060 0.0083 0.9565 0.0000 0.0028 CL= 0.710 CD=0.01106 CM=-0.1912
1.00	S TURB S SEP CD UPPER 0.5807 0.0035 0.0053 LOWER 0.6324 0.0000 0.0017 TOTAL CL= 0.823 CD=0.00707 CM=-0.1939	S TURB S SEP CD 1.0034 0.0084 0.0090 0.9564 0.0000 0.0026 CL= 0.817 CD=0.01156 CM=-0.1925	S TURB S SEP CD 0.9925 0.0084 0.0089 0.9401 0.0000 0.0025 CL= 0.817 CD=0.01149 CM=-0.1925
2.00	S TURB S SEP CD UPPER 0.5910 0.0051 0.0057 LOWER 0.6264 0.0000 0.0016 TOTAL CL= 0.931 CD=0.00729 CM=-0.1954	S TURB S SEP CD 1.0034 0.0108 0.0097 0.9564 0.0000 0.0024 CL= 0.924 CD=0.01205 CM=-0.1937	S TURB S SEP CD 1.0025 0.0108 0.0097 0.9213 0.0000 0.0023 CL= 0.924 CD=0.01201 CM=-0.1937
3.00	S TURB S SEP CD UPPER 0.6019 0.0067 0.0060 LOWER 0.6198 0.0000 0.0015 TOTAL CL= 1.038 CD=0.00754 CM=-0.1968	S TURB S SEP CD 1.0034 0.0135 0.0104 0.9564 0.0000 0.0022 CL= 1.030 CD=0.01262 CM=-0.1947	S TURB S SEP CD 1.0112 0.0136 0.0105 0.9028 0.0000 0.0021 CL= 1.029 CD=0.01264 CM=-0.1947
4.00	S TURB S SEP CD UPPER 0.6146 0.0084 0.0064 LOWER 0.6114 0.0000 0.0014 TOTAL CL= 1.146 CD=0.00784 CM=-0.1982	S TURB S SEP CD 1.0034 0.0163 0.0112 0.9564 0.0000 0.0020 CL= 1.135 CD=0.01326 CM=-0.1956	S TURB S SEP CD 1.0191 0.0166 0.0114 0.8880 0.0000 0.0020 CL= 1.134 CD=0.01340 CM=-0.1955
5.00	S TURB S SEP CD UPPER 0.6777 0.0113 0.0075 LOWER 0.5983 0.0000 0.0013 TOTAL CL= 1.251 CD=0.00882 CM=-0.1990	S TURB S SEP CD 1.0034 0.0194 0.0121 0.9564 0.0000 0.0019 CL= 1.240 CD=0.01399 CM=-0.1963	S TURB S SEP CD 1.0289 0.0200 0.0125 0.7834 0.0000 0.0017 CL= 1.239 CD=0.01424 CM=-0.1961
6.00	S TURB S SEP CD UPPER 0.9209 0.0200 0.0115 LOWER 0.5818 0.0000 0.0012 TOTAL CL= 1.348 CD=0.01274 CM=-0.1978	S TURB S SEP CD 1.0034 0.0228 0.0131 0.9564 0.0000 0.0017 CL= 1.344 CD=0.01482 CM=-0.1968	S TURB S SEP CD 1.0346 0.0239 0.0138 0.7763 0.0000 0.0016 CL= 1.342 CD=0.01535 CM=-0.1965
7.00	S TURB S SEP CD UPPER 0.9914 0.0259 0.0138 LOWER 0.5666 0.0000 0.0011 TOTAL CL= 1.448 CD=0.01496 CM=-0.1974	S TURB S SEP CD 1.0034 0.0264 0.0142 0.9564 0.0000 0.0016 CL= 1.447 CD=0.01574 CM=-0.1972	S TURB S SEP CD 1.0370 0.0282 0.0151 0.7668 0.0000 0.0015 CL= 1.444 CD=0.01662 CM=-0.1966

B.L.SUMMARY AIRFOIL S826 14% ALPHA0= 6.520 DEG.
 *-WARNING WITH VARIABLE LIMIT ALPHA REL. CHORD LINE

ALPHA(DEC.)	R= 3000000 MU=3.0	R= 3000000 MU=1.3	R= 3000000 MU=9.0
8.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0324 0.0328 0.0164*	1.0324 0.0328 0.0164*	1.0372 0.0332 0.0167*
	LOWER 0.5502 0.0000 0.0010	0.9564 0.0000 0.0015	0.7566 0.0000 0.0014
	TOTAL CL= 1.545 CD=0.01748	CL= 1.545 CD=0.01791	CL= 1.544 CD=0.01805
	CM=-0.1965	CM=-0.1965	CM=-0.1963
9.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0368 0.0389 0.0184*	1.0368 0.0389 0.0184*	1.0373 0.0395 0.0186*
	LOWER 0.5361 0.0000 0.0010	0.9564 0.0000 0.0013	0.7469 0.0000 0.0013
	TOTAL CL= 1.643 CD=0.01934	CL= 1.643 CD=0.01973	CL= 1.642 CD=0.01984
	CM=-0.1957	CM=-0.1957	CM=-0.1955
10.00	S TURB S SEP CD	S TURB S SEP CD	S TURB S SEP CD
	UPPER 1.0370 0.0466 0.0205*	1.0370 0.0466 0.0205*	1.0374 0.0467 0.0206*
	LOWER 0.5209 0.0000 0.0009	0.9303 0.0000 0.0012	0.7368 0.0000 0.0012
	TOTAL CL= 1.738 CD=0.02142	CL= 1.738 CD=0.02178	CL= 1.738 CD=0.02176
	CM=-0.1942	CM=-0.1942	CM=-0.1941

REPORT DOCUMENTATION PAGE

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1. REPORT DATE (DD-MM-YYYY) January 2005		2. REPORT TYPE Subcontract report		3. DATES COVERED (From - To) 1994 - 1995		
4. TITLE AND SUBTITLE The S825 and S826 Airfoils			5a. CONTRACT NUMBER DE-AC36-99-GO10337			
			5b. GRANT NUMBER			
			5c. PROGRAM ELEMENT NUMBER			
6. AUTHOR(S) D.M. Somers			5d. PROJECT NUMBER NREL/SR-500-36344			
			5e. TASK NUMBER WER4.3110			
			5f. WORK UNIT NUMBER			
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Airfoils, Inc. 601 Cricklewood Drive State College, PA 16083				8. PERFORMING ORGANIZATION REPORT NUMBER AAF-4-14289-01		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Renewable Energy Laboratory 1617 Cole Blvd. Golden, CO 80401-3393				10. SPONSOR/MONITOR'S ACRONYM(S) NREL		
				11. SPONSORING/MONITORING AGENCY REPORT NUMBER NREL/SR-500-36344		
12. DISTRIBUTION AVAILABILITY STATEMENT National Technical Information Service U.S. Department of Commerce 5285 Port Royal Road Springfield, VA 22161						
13. SUPPLEMENTARY NOTES NREL Technical Monitor: J. Tangler						
14. ABSTRACT (Maximum 200 Words) A family of airfoils, the S825 and S826, for 20- to 40-meter, variable-speed and variable-pitch (toward feather), horizontal-axis wind turbines has been designed and analyzed theoretically. The two primary objectives of high maximum lift, insensitive to roughness, and low profile drag have been achieved. The constraints on the pitching moments and the airfoil thicknesses have been satisfied. The airfoils should exhibit docile stalls.						
15. SUBJECT TERMS airfoils; wind turbine; airfoil design; Pennsylvania State University; wind energy						
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT UL	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON	
a. REPORT Unclassified	b. ABSTRACT Unclassified	c. THIS PAGE Unclassified			19b. TELEPHONE NUMBER (Include area code)	

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