

Assessment of IEEE 1547 Low-Voltage Ride-Through Criteria Impact on Bulk Power System Dynamics Following Transmission Path Fault

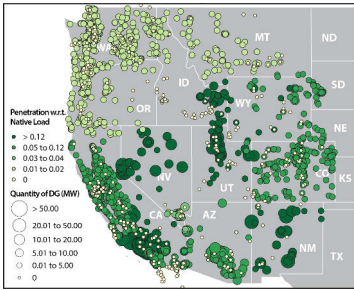
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Initial PSLF Simulation: Western Interconnection, Path 61, Fault Induced Delayed Voltage Recovery

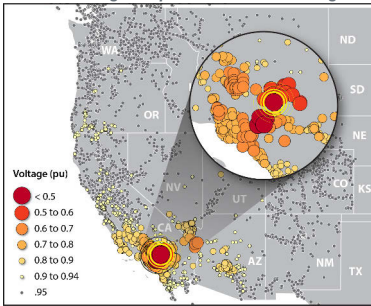
- Heavy Summer 2023 planning case with high levels of utility scale (~17%) and distributed renewable energy (~5%).
- More than 21,000 buses; 190 GW of load; 9 GW of photovoltaic distributed generation acting as negative load.
- Distributed generation (DG) modeled within dynamic composite load model (CMPLDWG).
- Three-phase fault on 500-kV Lugo bus; $Z = 0 + j0.034$, cleared after six cycles with associated Lugo-Victorville line trip.

DG on the Western Interconnection



- Based on work from the Western Wind and Solar Integration Study Phase 3.
- Output at power flow instance.

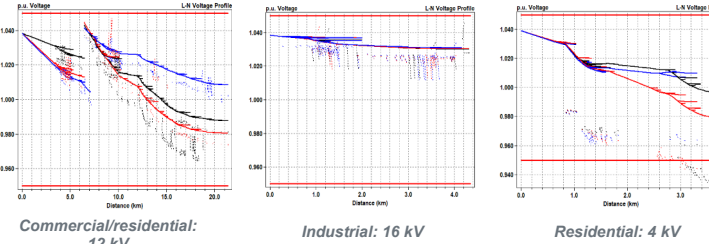
Bus voltages in per unit at fault clearing



- Wide impact on voltage profiles, particularly in Southern California.
- Spatial voltage profile at fault-clearing moment in simulation.

OpenDSS Feeder Simulations with PSLF-Generated Voltage Profiles

California Feeders with Secondaries

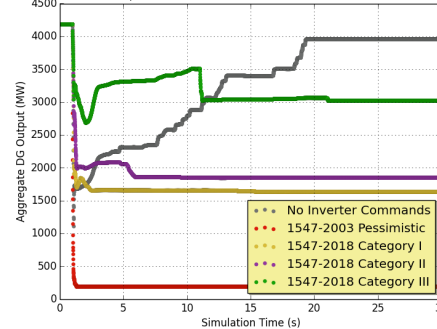


- 123 unique voltage profiles from PSLF Path 61 fault simulation.
- 50 inverters compliant to relevant IEEE 1547 ride-through criteria on each feeder, located on secondaries.
- Proportional representation of residential/commercial/industrial feeders based on impacted region.
- Four simulations of each unique voltage profile dependent on type of ride-through criteria.
- All ride-through control based on pessimistic interpretation of standard—i.e., if current injection is not explicitly required, then current injection is assumed to be zero.

IEEE 1547 Implementation Envelopes

Voltage	IEEE 1547: 2013 Pessimistic	IEEE 1547: 2018 Category I	IEEE 1547: 2018 Category II	IEEE 1547: 2018 Category III
$V < 0.3$	Immediate trip	Immediate trip	Immediate trip	Momentary cessation; trip after 1.0 s
$0.3 \leq V < 0.5$		Momentary cessation; trip after 0.32 s	Momentary cessation; trip after 0.32 s	Continuous operation; trip after 10.0 s
$0.5 \leq V < 0.65$		Momentary cessation; trip after 0.16 s	Trip after: $3 s + (8.7 \text{ s/p.u.}) \times (V - 0.65 \text{ p.u.})$	Continuous operation; trip after 20.0 s
$0.65 \leq V < 0.7$		Trip after $0.7 s + (4 \text{ s/p.u.}) \times (V - 0.7 \text{ p.u.})$	Continuous operation	Continuous operation
$0.7 \leq V < 0.88$	Continuous operation	Continuous operation	Continuous operation	Continuous operation
$0.88 < V$	Continuous operation	Continuous operation	Continuous operation	Continuous operation

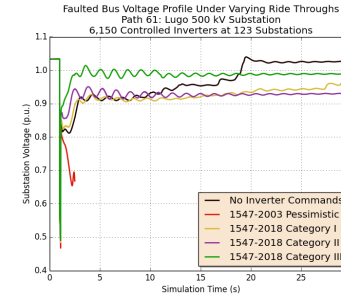
Aggregate DG Output Under Varying Ride Throughs



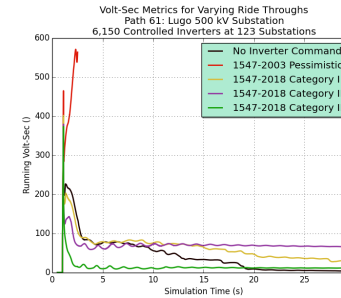
- FIDVR occurs.
- Prolonged low voltages at nearly 1,000 buses.
- Indicative that type of distributed generation ride-through criteria will heavily influence aggregate distributed generation output.

Western Interconnection Response with OpenDSS Distributed Generation Commands

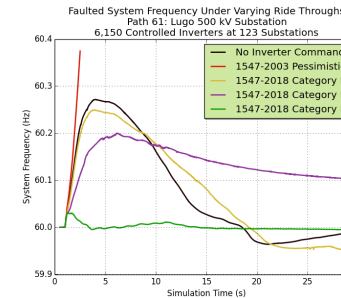
Path 61 fault scenario re-simulated but with explicit distributed generation commands at the 123 buses from OpenDSS simulations



- Pessimistic case results in simulation divergence.
- Categories I and II exhibit similar voltage recoveries.
- Category III results in no FIDVR.
- None show the complete recovery seen in the original simulation because of lack of full distributed generation recovery.



- Running volt-sec metric: $\sum_{n=1}^N \Delta t(\max(0, v_L - b_n^t))$
- N : bus count; Δt : simulation time step; v_L : voltage cutoff (0.95); b_n^t : bus n voltage at time t
- Captures system-wide voltage profile.
- Corroborates no FIDVR with Category III ride-through.



- Center-of-inertia frequency: $\omega(t) = \frac{\sum_{i=1}^G (MVA_i \cdot \omega(t_i))}{\sum_{i=1}^G MVA_i}$
- G : generator count; MVA_i : generator i MVA rating; $\omega(t_i)$: generator i frequency
- High frequencies because of low voltage -> static load decrease.
- Category II is similar to original.
- Category III shows large improvement over initial frequency.

Key Findings

- Under heavy loading conditions, the Western Interconnection is susceptible to widespread voltage influences from transmission faults.
- Categories I and II yield similar real power results. Category III yields a respectively smaller total real power output.
- FIDVR events can persist well beyond the trip times specified in the IEEE 2018 ride-through criteria.