SIAM CSE21 – Thursday, March 4

Adaptive Mesh Refinement Large Eddy Simulation of the Supercritical Carbon Dioxide Round Turbulent Jet

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What are supercritical fluids?

- Fluids held above critical temperature and pressure
- Liquid-like density
- Gas-like viscosity
- Sensitive density, pressure, temperature relationship
- Critical point for CO_2 : T=304 K, P=7.38 MPa

Fig. 2a: 10 MWe sCO₂ power turbine compared to a 10 MWe steam turbine

Fig. 2b: Overview of project with 8Rivers Capital: https://hpc4mtls.llnl.gov/projects.html

Supercritical fluids are important for a wide range of applications

- $sCO₂$ can be utilized in a variety of industries:
	- Closed-cycle gas turbines
	- Carbon sequestration
- \cdot sCO₂ promising fluid in many fields, yet many fundamental physical aspects still unknown
- Experimental challenges with pseudocritical parameters
- Current jet research oriented toward application-specific quantities of interest.

Fig. 3: Examples of Geologic Carbon Sequestration

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Fig. 4: Another promising application of sCO₂ is in high flux thermal management.

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Project Scope

Goal: simulate flow field of turbulent sCO₂ **jet in order to gain better understanding of underlying physics.**

- Our hypothesis is that supercritical flows for canonical round turbulent jets exhibit different physical mechanisms than those of ideal gas.
- Understanding base mechanisms of supercritical flows can add to theory related to quantities of interest across all applications

PeleC

- Built on AMReX and funded by the Exascale Computing Project (ECP) through the Department of Energy (DOE), PeleC is an adaptive-mesh compressible hydrodynamics code for reacting flows
	- Models turbulence-chemistry interactions motivated by conditions in internal combustion engines
	- Can additionally handle embedded boundary conditions, non-ideal EoS, and allows for implementation of adaptive mesh refinement (AMR)
- Utilizes 2nd order finite volume formulation using the Piecewise Parabolic Method (PPM) in space and a standard RK2 time integrator to approximate solutions.
- To learn more visit: https://github.com/AMReX-Combustion/PeleC

Fig 5: Injection of natural gas in a piston-bowl geometry performed using PeleC

Equations of State (EoS)

Gamma Law for Ideal Gas

$$
p=(\gamma-1)\rho\epsilon
$$

Used for Jet verification with air

Soave-Redlich-Kwong for Non-Ideal Gas

$$
\begin{aligned} p &= \frac{RT}{V_m - b} - \frac{a\,\alpha}{V_m\,(V_m + b)} \\ a &= \frac{0.42747\,R^2\,T_c^2}{P_c} \\ b &= \frac{0.08664\,R\,T_c}{P_c} \\ \alpha &= \left(1 + \left(0.48508 + 1.55171\,\omega - 0.15613\,\omega^2\right)\left(1 - T_r^{\,0.5}\right)\right)^2 \\ T_r &= \frac{T}{T_c} \end{aligned}
$$

where ω is the acentric factor for the species.

Needed to more accurately handle drastic density and specific heat changes across critical point

Gallagher, B. (2012). "Equation of State Unit". Retrieved from http://flash.uchicago.edu/~jbgallag/2012/flash4_ug/node22.html#SECTION0631000000000000000.

Soave, Giorgio (1972). "Equilibrium constants from a modified Redlich-Kwong equation of state". *Chemical Engineering Science*. 27(6): 1197–1203. doi:10.1016/0009-2509(72)80096-4.

Rasmussen, E., Shashank, Y., & Martin, M. (2021). "How equation of state selection impacts accuracy near the critical point: Forced convection supercritical CO2 flow over a cylinder." The Journal of Supercritical Fluids. 1 https://doi.org/10.1016/j.supflu.2020.105141

Martin, M., Rasmussen, E. & Shashank, Y. (2019). "Nonlinear Heat Transfer from Particles in Supercritical Carbon Dioxide Near the Critical Point." Journal of Thermal Science and Engineering Applications. 034501 (5 pages). https://doi.org/10.1115/1.4045222

Large Eddy Simulation (LES) modeling

- Dynamic Smagorinsky Model for compressible flow
	- Filter type: 3 point box filter approximation
	- Filter-Grid ratio: 2

Martín, M. Pino, U. Piomelli, and G. V. Candler (2000). "Subgrid-Scale Models for Compressible Large-Eddy Simulations." *Theoretical and Computational Fluid Dynamics.* 13(5): 361–376

Sagaut, P. and R. Grohens (1999). "Discrete filters for large eddy simulation." *International Journal for Numerical Methods in Fluids.* 31: 1195-1220

Schematic

- 3D Simulation
- Slice at z=0 for visualizations
- Buffer zone implemented with adaptive mesh refinement (AMR)
- Ambient temperature and pressure set to match inlet condition
- # of cells on coarse grid (x ,y, z): 80, 200, 80
- AMR max level: 4
- Refine when vorticity $_{ERR}$ > 5000

Performing LES in HPC environment

- Simulations utilize 576 MPI Ranks
	- 36 ranks per node across 16 nodes
	- Roughly 17k cells per MPI Rank
- Each plot file contains approximately 34 GB of data
- We use the NREL Eagle supercomputer to perform simulations
- PeleC has been shown to scale very well on this system and other HPC systems (e.g. ORNL Summit)
- Dynamic load balancing of AMR levels allows for maximum utilization of the system
- The Intel suite of compilers was used

Boundary Conditions

Inflow

- diameter = .01 cm
- input velocity scaled to predetermined mean velocity + noise scaled by r.m.s. profiles calculated via direct numerical simulation (DNS)

$$
v = \langle v_{\text{DNS}} \rangle + (v_{\text{DNS}}' + \beta v_{\text{DNS}}' r_1 \sin \theta_1) \cdot r_2 \sin \theta_2
$$

\n
$$
u = u_{\text{DNS}}' + \beta u_{\text{DNS}}' r_3 \sin \theta_3
$$

\n
$$
w = w_{\text{DNS}}' + \beta w_{\text{DNS}}' r_4 \sin \theta_4
$$

\n
$$
r_i = \sqrt{-2.0 \log(X_i)}
$$

\n
$$
\theta_j = 2\pi X_j
$$

 X_n is a random number between 0 and 1

Outflow

- Impose zero gradient at boundary
- Do not implement AMR at boundary

Exploring Injections Near the Pseudocritical Point

• We want to look at cases near the critical point to study large changes in specific heat

National Institute of Standards and Technology. "Isobaric Properties for Carbon Dioxide." *NIST Chemistry WebBook, SRD 69,* 2018,

https://webbook.nist.gov/cgi/fluid.cgi?P=10.1325&TLow=300&THigh=375&TInc=1&Applet=on&Digits=6&ID=C124389&Action=Load&Type=IsoBar&TUnit=K&PUnit=MPa&DUnit=g%2Fml&HUnit=kJ%2Fmol&WUnit=m%2Fs&VisUnit=cP&STUnit=N%2Fm&R efState=DEF. Accessed 23 October 2019.

- M \approx .262
- Initial # of cells (x, y, z) : 80, 120, 80
- AMR max level: 3
- Refine when vorticity $_{\text{ERR}}$ > 100

Note: Current simulations do not include a subgrid scale model; future ones will. The following is a coarse grid, capability establishing simulation.

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- Plots saved every 300 time steps
- Slices made every 30 cm in y direction from $y =$ 30 to 120
- Means calculated with last 10 plot files

sCO2 Jet: Velocity Profiles

- Profiles begin to collapse into one curve in self-similar region expected by theory.

Note: Simulation has not yet reached statistically stationary steady state

sCO ² Jet: Centerline Scaling

- Jet has only just reached
y/d=60 in simulation so
relationship is still
undetermined.
Note: Simulation has not yet reach
statistically stationary steady state y/d=60 in simulation so relationship is still undetermined.

Note: Simulation has not yet reached

Variation with Axial Distance of Mean Velocity along Centerline

sCO ² Jet: Reynolds Stresses

- General trends for Reynolds stresses match experimental data but magnitude is very high due to current time in simulation.

Note: Simulation has not yet reached statistically stationary steady state

Current Status of Simulations

- All three cases have run to completion: 2 flow throughs of coarse (max 1 level) refinement and 10 subsequent flow throughs of fine (max 4 level) refinement.
- 100 plots saved per flow through
- Means calculated with last 200 plot files

Post-Processing Large Datasets in HPC environments

At this point, all three cases have reached statistically stationary steady state, but we are now having issues with slicing large datasets in the HPC environment.

Currently, building custom post-processing tools to extract data.

Acknowledgements

- This research was supported in part by an appointment with the National Science Foundation (NSF) Mathematical Sciences Graduate Internship (MSGI) Program sponsored by the NSF Division of Mathematical Sciences. This program is administered by the Oak Ridge Institute for Science and Education (ORISE) through an interagency agreement between the U.S. Department of Energy (DOE) and NSF. ORISE is managed for DOE by ORAU. All opinions expressed in this paper are the author's and do not necessarily reflect the policies and views of NSF, ORAU/ORISE, or DOE.
- The research was performed using computational resources sponsored by the Department of Energy's Office of Energy Efficiency and Renewable Energy and located at the National Renewable Energy Laboratory.
- This work was supported by the Department of Energy's Office of Science through the Exascale Computing Project (ECP), managed through Oak Ridge National Laboratory.

Questions?

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NREL/PR-2C00-79440