**Gallery of Fluid Motion**

## **Visualizations of direct fuel injection effects in a supersonic cavity flameholder**

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Supersonic combustion has received considerable interest in recent years due to emphasis on hypersonic vehicle development [\[1\]](#page-2-0), reusable launch systems, and air-breathing rocket engines [\[2\]](#page-2-0). Combustion and flame stabilization at high supersonic flows is challenging mainly due to small residence times for fuel-oxidizer mixing and ignition. Cavity-based flameholders are a viable technique for providing flame stabilization in these applications. They enable flow deceleration and recirculation, thus increasing the residence time for adequate mixing of fuel and for subsequent combustion. Direct fuel injection into the cavity has been found to be advantageous compared to passive injection strategies with regard to greater control of local stoichiometry and fuel residence times [\[3\]](#page-2-0); however, a theoretical understanding of turbulent mixing and combustion between the fuel jet and supersonic air stream has not yet been fully developed. The main contribution of this work is to address these interactions via high-fidelity combustion simulations and cutting-edge visualization.

We employ PELEC  $[4,5]$ , an open-source compressible reacting flow solver, to study the combustion and flow dynamics in a representative cavity flameholder. We solve the compressible multispecies Navier-Stokes equations with finite-rate  $H_2$ -air chemistry. The solver employs adaptive-mesh-refinement (AMR) techniques on a Cartesian grid framework with a cut-cell-based formulation for representing complex geometries. Adaptive-mesh refinement is enabled at locations with high density gradients, vorticity, and temperature for resolving shock waves, shear-layer turbulence, and flames, respectively. We use an open-source cinematic package BLENDER [\[6\]](#page-2-0) that provides physics-based volume rendering for visualizing the flow and combustion phenomena resolved by our simulations.

The geometry examined in this work is shown in Fig.  $1(a)$  and involves supersonic flow over a cavity with a ramp-shaped trailing edge. The use of a ramp shape has been found to be advantageous compared to a rectangular shape with regard to reduction in drag and shear-layer oscillations [\[7\]](#page-2-0). We study direct fuel injection into this cavity at two different locations, labeled as cases C1 and C2. The first step was to run a nonreacting simulation without fuel injection to statistically stationary

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FIG. 1. (a) Schematic of the cavity geometry used in our simulation, (b) flow features from a nonreacting simulation such as shock waves and shear layers, (c) numerical schlieren and corresponding numerical grid with AMR where each box is an  $8 \times 8 \times 8$  grid, (d) temperature snapshots on a midplane slice, and (e) temperature distribution within the cavity at statistical steady state for cases C1 and C2. Please refer to the full video at [https://doi.org/10.1103/APS.DFD.2020.GFM.V0026.](https://doi.org/10.1103/APS.DFD.2020.GFM.V0026)

state. The stabilized flow structures such as oblique shock waves, shear-layer turbulence, and shockboundary-layer interactions are as shown in Fig.  $1(b)$ . These flow structures are resolved using three levels of AMR (base level at  $512 \times 128 \times 32$  grid), as indicated in Fig. 1(c), which shows a numerical schlieren snapshot along with the corresponding computational mesh.

A reacting flow simulation for each injection location was initialized using the nonreacting flow fields. Figure 1(d) shows a snapshot of temperature for cases C1 and C2 after achieving statistically stationary states in the reacting simulation. The compression waves emanating from

<span id="page-2-0"></span>the shear layer are only slightly altered by fuel injection, with greater impact in case C1 due to farther jet penetration. The important difference between the two injection scenarios, elucidated from the visualization, is the interaction between the fuel jet and shear layer as shown in Fig.  $1(e)$ . The fuel jet in case C1 is injected into a low-momentum region, while the downstream C2 injection is in the vicinity of shear-layer turbulence. There is greater penetration of the fuel jet into the cavity in case C1, while it disintegrates close to the inlet in case C2. The increased jet penetration into the cavity for case C1 results in a low-frequency oscillatory behavior (∼4 kHz) between pressure and heat release [4], while high-frequency oscillations (∼30 kHz) consistent with closed-box acoustics are observed in case C2. Furthermore, case C1 results in richer combustion and higher peak temperatures, while enhanced mixing in case C2 enables leaner combustion at lower temperatures. This high-fidelity simulation study, enabled by AMR, state-of-the-art visualization tools, and high-performance computing, elucidates important implications with regard to direct fuel injection, with downstream injection within the cavity potentially having more favorable properties when designing cavity flameholders.

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- [1] D. B. Le, C. P. Goyne, R. H. Krauss, and J. C. McDaniel, Experimental study of a dual-mode scramjet isolator, [J. Propul. Power](https://doi.org/10.2514/1.32591) **24**, 1050 (2008).
- [2] J. Taylor, F. Flanagan, A. Dunlop, S. D. Grimshaw, and R. Miller, Super aggressive S-ducts for air breathing rocket engines, J. Turbomach. **143**[, 061015 \(2021\).](https://doi.org/10.1115/1.4050596)
- [3] [F. W. Barnes and C. Segal, Cavity-based flameholding for chemically-reacting supersonic flows,](https://doi.org/10.1016/j.paerosci.2015.04.002) Prog. Aerosp. Sci. **76**, 24 (2015).
- [4] H. Sitaraman, S. Yellapantula, M. T. H. de Frahan, B. Perry, J. Rood, R. Grout, and M. Day, Adaptive mesh [based combustion simulations of direct fuel injection effects in a supersonic cavity flame-holder,](https://doi.org/10.1016/j.combustflame.2021.111531) Combust. Flame **232**, 111531 (2021).
- [5] [https://github.com/AMReX-Combustion/PeleC.](https://github.com/AMReX-Combustion/PeleC)
- [6] Blender online community, Blender—A 3D modelling and rendering package (Blender Foundation, Blender Institute, Amsterdam, 2021).
- [7] X. Zhang, A. Rona, and J. A. Edwards, The effect of trailing edge geometry on cavity flow oscillation driven by a supersonic shear layer, Aeronaut. J. **102**, 129 (1998).