



# Case Study: Hybridizing Nuclear Energy Systems in the U.S.

Mark F. Ruth

Joint ICTP-IAEA VIRTUAL Course on Nuclear–Renewable Integrated Energy Systems: Phenomenology, Research and Development

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# Team

- Bethany Frew, Daniel Levie, and Jal Desai (NREL);
- L. Todd Knighton, Dan Wendt, Cristian Rabiti, James Richards, Richard Boardman, and Shannon Bragg-Sitton (Idaho National Laboratory);
- Amgad Elgowainy (Argonne National Laboratory);
- Dan Ludwig (Xcel Energy)

# Project Goal

Evaluate the Potential for Hybridized Nuclear Power Plants to Economically Generate Hydrogen – One Aspect of the H2@Scale Vision

Quantify the potential financial impact of hybridizing Xcel Energy's Prairie Island and Monticello nuclear power plants to produce hydrogen

**Prairie Island – 1096 MW**



Credit: Xcel Energy

**Monticello – 671 MW**



Credit: Xcel Energy

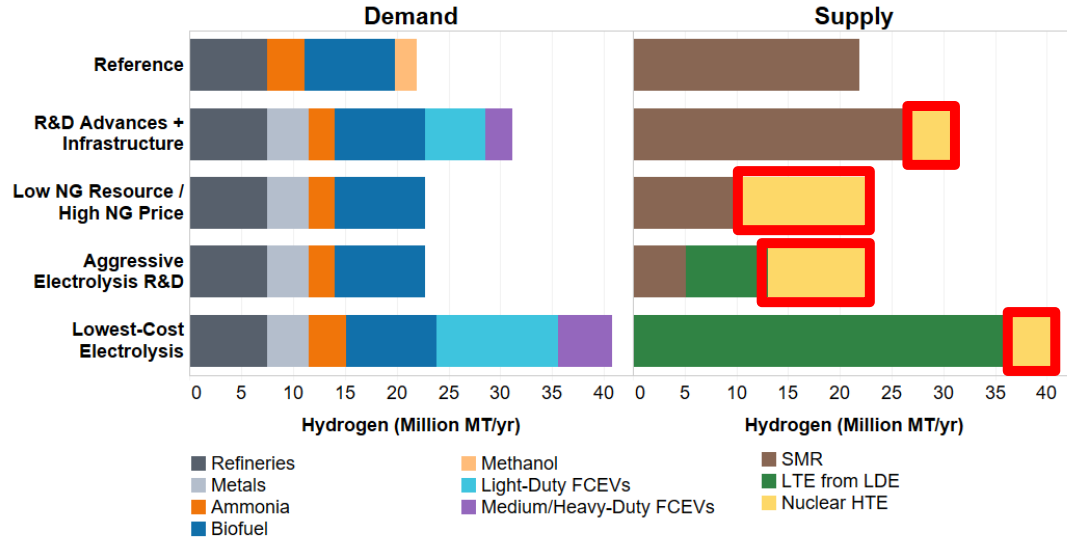
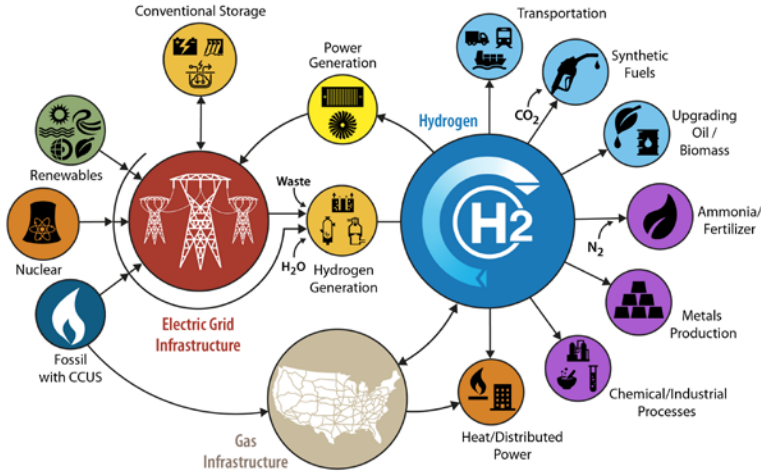
# Additional Objectives

## Evaluate the Potential for Hybridized Nuclear Power Plants to Economically Generate Hydrogen – One Aspect of the H2@Scale Vision

- Provide investment grade information for supporting Xcel Energy's greenhouse gas (GHG) reduction efforts to be used for internal and external stakeholder reviews and approvals.
- Quantify opportunity while considering impacts on generation required to meet all loads in the region
- Improve understanding of the potential for hybridized nuclear power plants to achieve the \$2/kg hydrogen production cost target
- Develop tools and capabilities that better characterize hybridized hydrogen production on the grid so new opportunities can be analyzed.

# Interest in Hydrogen

## Using Nuclear Energy to Produce Hydrogen is a Key Opportunity for H2@Scale



<https://www.energy.gov/eere/fuelcells/h2scale>

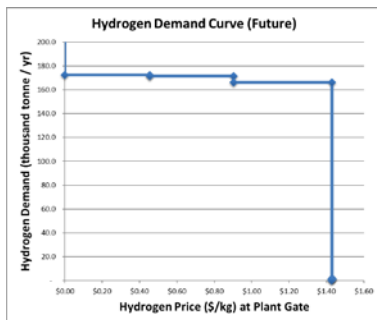
<https://www.nrel.gov/docs/fy21osti/77610.pdf>

Analysis of the economic potential of H2@Scale indicates that nuclear energy may provide a large quantity of hydrogen in the future (yellow bars in the righthand figure). This project is analyzing the economics of that opportunity

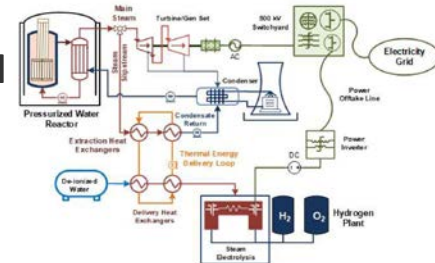
# Overall Approach

Use Best-in-Class Analysis Tools and Transfer Information Between them to Address Analysis Questions

**Hydrogen Market Assessment**  
(Delivery-adjusted demand curves)



**Hydrogen System Cost and Performance Estimates**

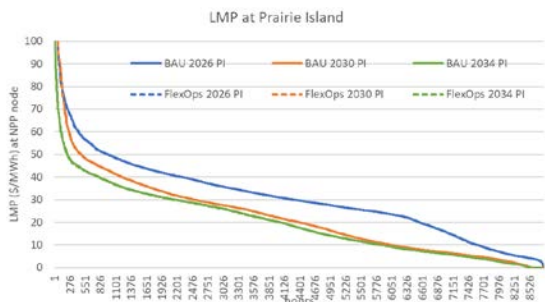


**Hydrogen System Configuration Optimization**

	Annual APC	Annual NPP Net Operating Income	Annual System Wide Market Cost (Total)	Annual System Wide Market Cost (Net)
BAU 2026	516.1	151.3	835.5	835.5
BAU 2030	342.82	28.1	662.02	662.02
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H2 2026				
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**Figures of Merit**

**In-depth electricity system modeling**



Previous analyses\* used a price-taker approach for grid modeling. This approach addresses the impacts of changing NPP generation on grid operations – essential to estimate impacts on an integrated utility like Xcel Energy.

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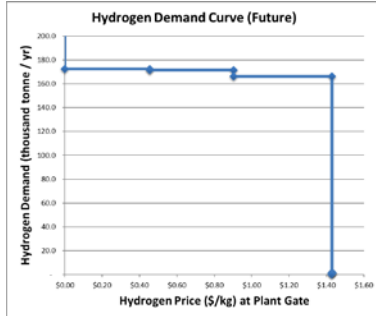
# Figures of Merit

- 1. Annual Adjusted Production Cost (APC):** total variable cost of non-NPP generation in Northern States Power (NSP) footprint, accounting for sales/purchases with neighboring zones (which may have different locational prices), summed across all hours.
  - Adapted from Midcontinent Independent System Operator (MISO) metric
- 2. Annual NPP Net Operating Income:** difference between the annual income (energy + operating reserves + H2) and annual operating cost (fixed costs + additional FlexOps cost) of an individual NPP
  - Standard pro forma calculation
- 3. System-wide market costs:** APC plus Annual NPP Operating Cost. Two methods:
  - A. Total Cost** – do not include H2 revenue (i.e., does not benefit end rate payers)
  - B. Net Cost** – include H2 revenue (i.e., benefits end rate payers)

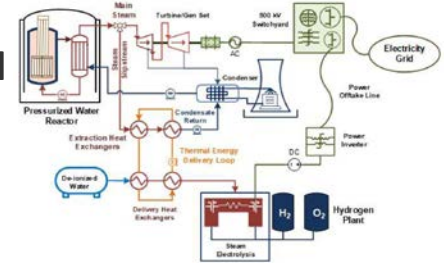
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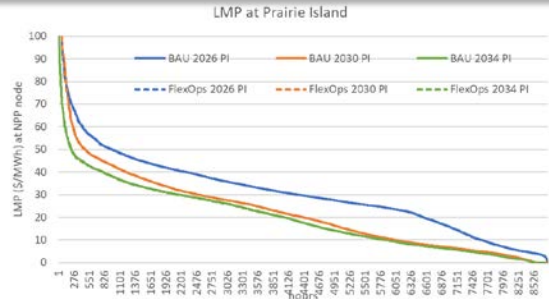
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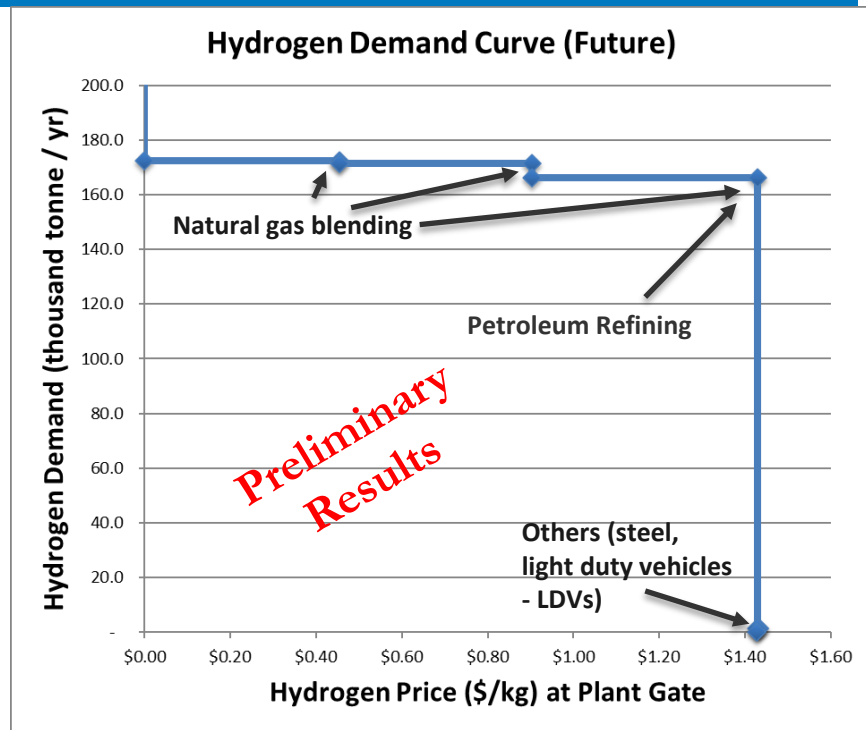
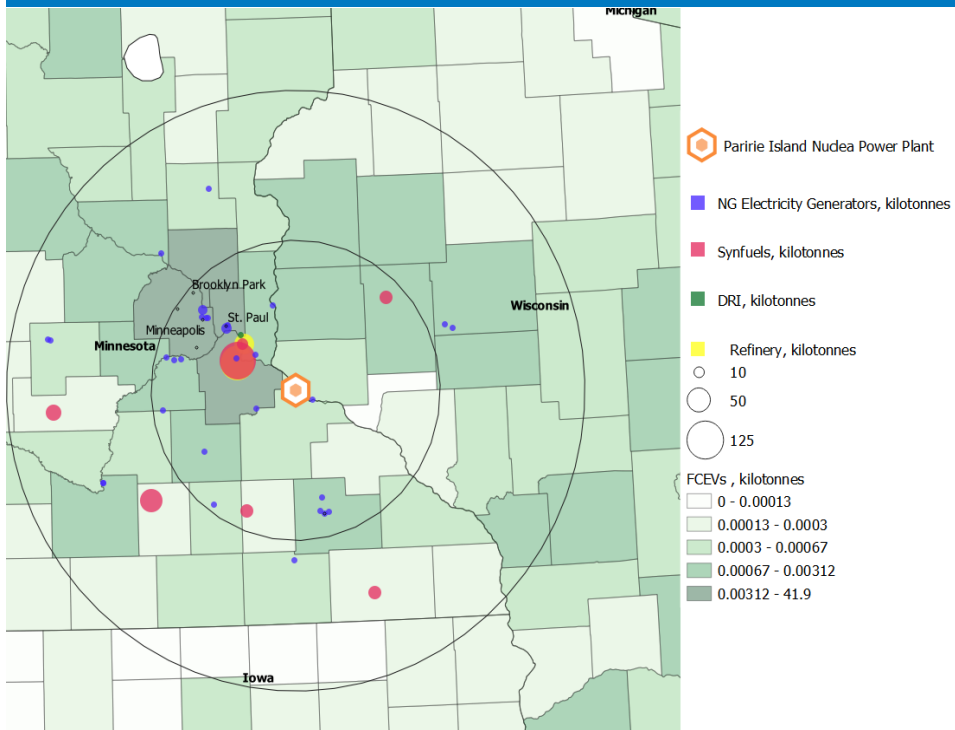
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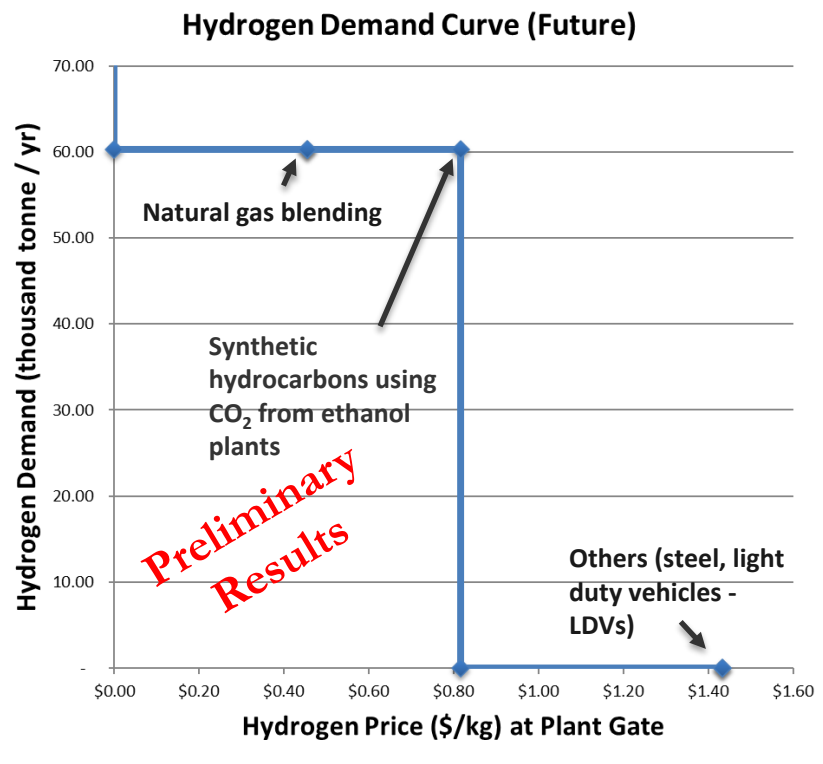
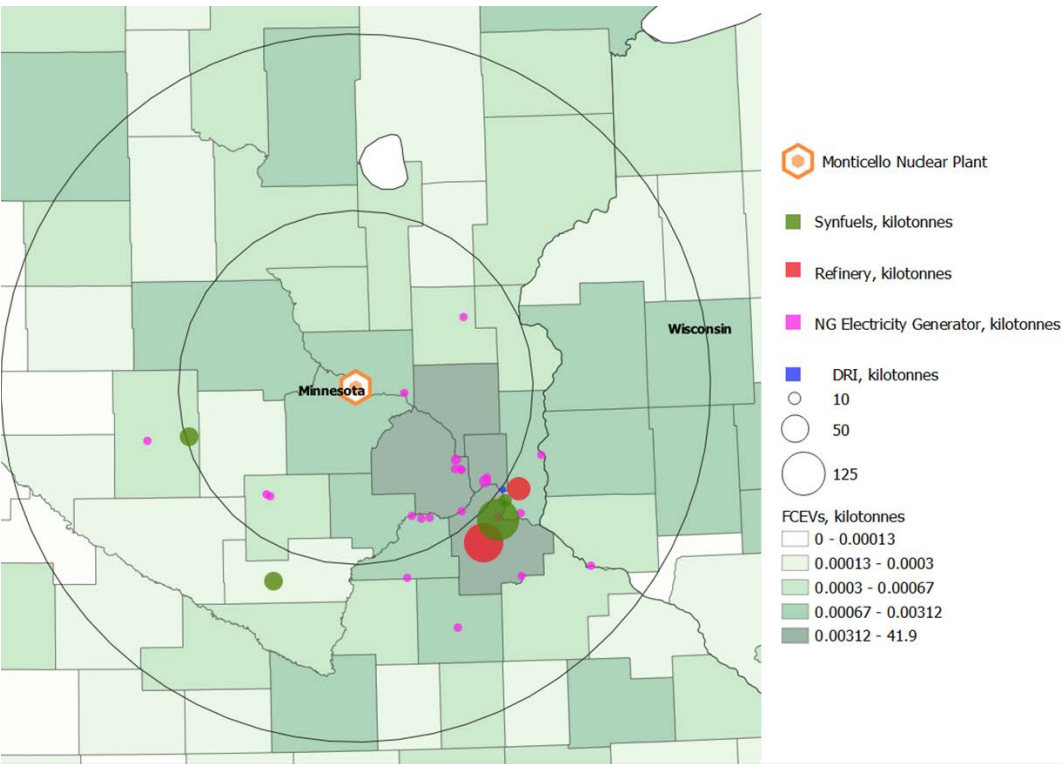
- Hydrogen demand for refineries: based on reported average H<sub>2</sub> use/BBL of crude processed at refinery
- Hydrogen for steel refining (direct reduction of iron - DRI): based on capacity of exiting steel plants, assuming 30 kg\_H<sub>2</sub>/MT of steel (i.e., 30% H<sub>2</sub>/70% NG by energy)
- Hydrogen for synthetic hydrocarbon production: based on CO<sub>2</sub> available from adjacent ethanol plants and 3:1 H<sub>2</sub>:CO<sub>2</sub> mole ratio
- Hydrogen for blending with natural gas for power generation: assuming 30% blending ratio by volume
- ✓ Demand curve is adjusted with H<sub>2</sub> compression and delivery cost
- ✓ Threshold H<sub>2</sub> price set to breakeven with steam methane reformed-H<sub>2</sub> for refineries, fuel cell electric vehicles and DRI, and to breakeven with NG on (higher heating value - HHV) Btu cost basis for blending
  - Assumed \$22.2 tax per metric ton of CO<sub>2</sub>

# H2 Applications and Developed Delivery-& Carbon Cost-Adjusted Demand Curves for Prairie Island



Primary hydrogen demands: petroleum refining and blending for power generation

# H2 Applications and Developed Delivery-& Carbon Cost-Adjusted Demand Curves for Monticello

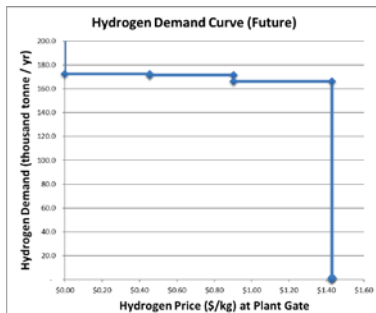


Delivery adjusted demand curve for Monticello shown on right

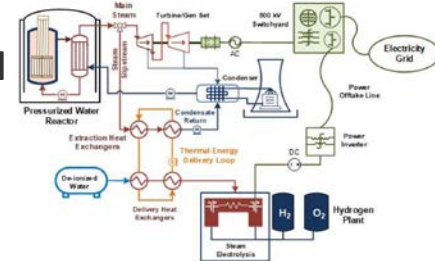
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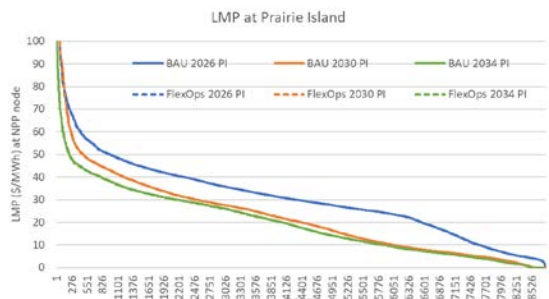


Hydrogen System Cost and Performance Estimates



Hydrogen System Configuration Optimization

In-depth electricity system modeling



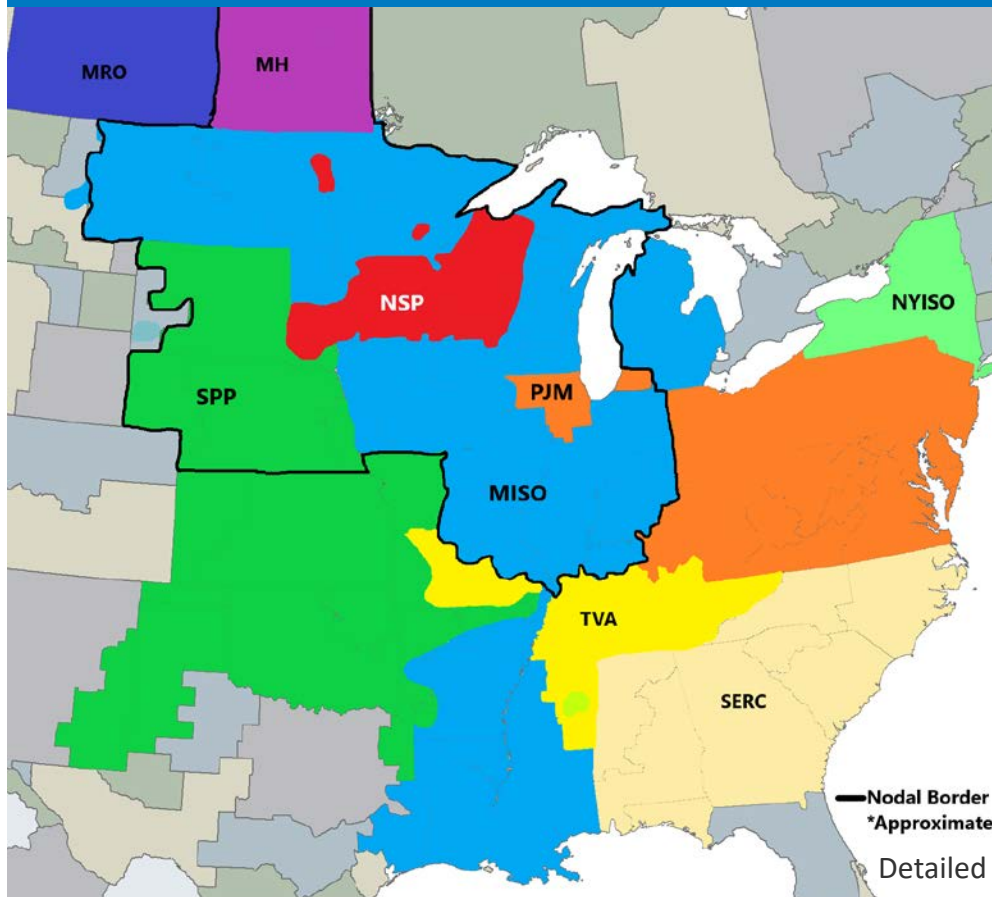
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# Electricity System Modeling: Nodal Hourly Production Cost Models for NSP and Zonal for Neighboring Regions



- Generation and transmission
  - Xcel Energy's Integrated Resource Plan within the Northern States Power (NSP) Territory
  - ReEDS capacity expansion model results for other regions
- Operating strategy and costs
  - PLEXOS Production Cost Modeling
  - Nodal resolution within the black boundary: 15,605 nodes with full unit commitment and operating reserves representation
  - All other zones: zonal resolution (i.e., copperplate inside of zone), no unit commitment, and generally no operating reserves

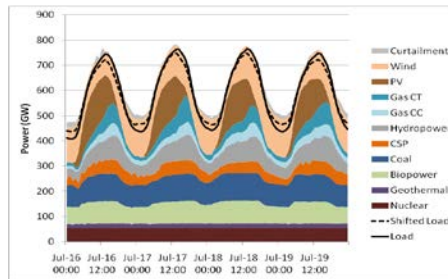
# PLEXOS modeling for hourly system operation

- **Commercial-grade production cost software**
- **Hourly chronological optimization**
  - Minimizes system wide variable cost
- **Commits and dispatches generating units based on:**
  - Electricity demand
  - Operating parameters of generators (ramp rates, minimum generation level, outages, etc.)
  - Transmission grid parameters (flow limits, contingencies)
  - Operating reserve requirements
- **Used for system generation and transmission planning**
  - Increasingly used for real-time operation



Locational prices,  
production cost

Dispatch  
information,  
curtailment,  
fuel usage

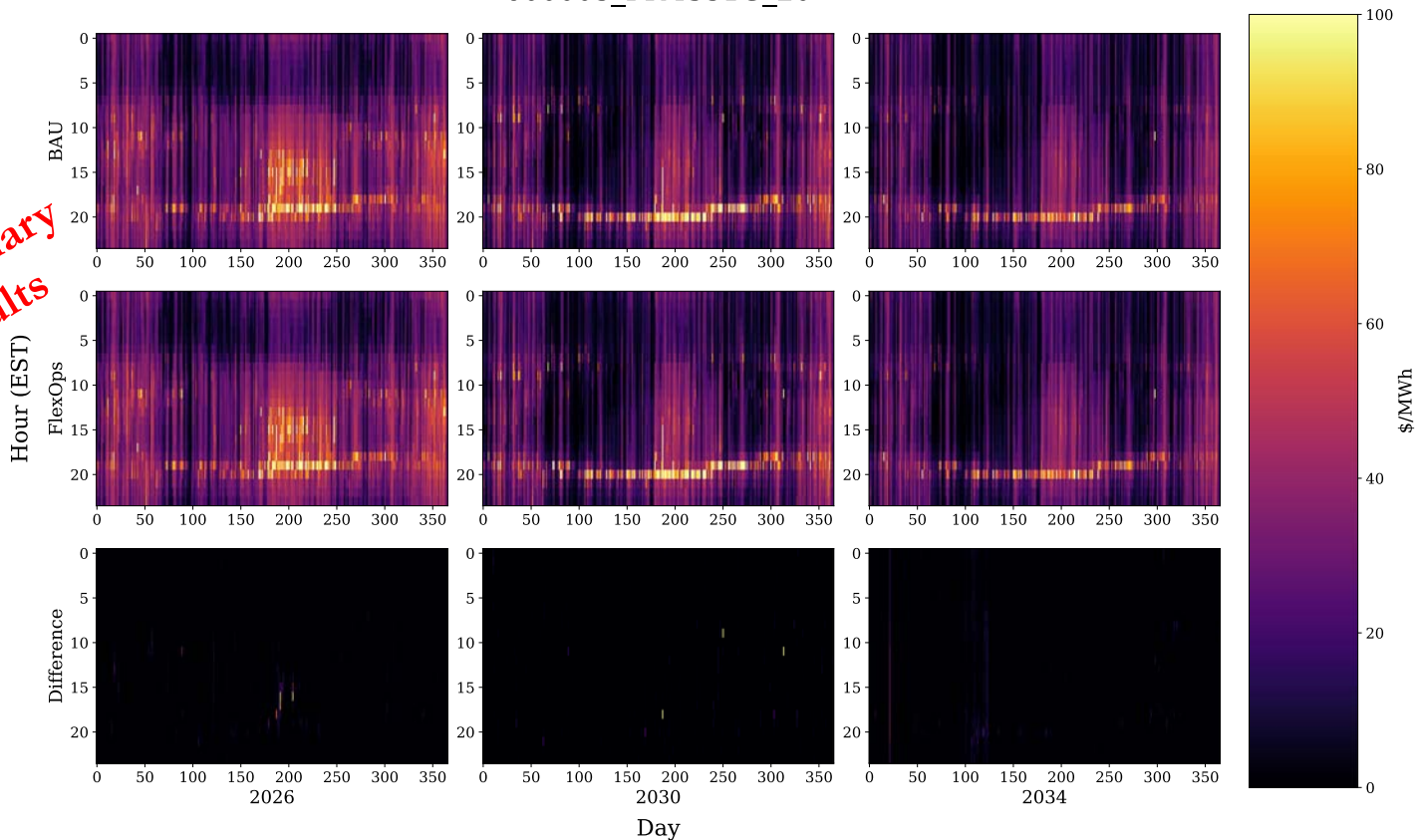


Transmission  
congestion

# Prairie Island LMP Heat Map

600003\_PR IS31G\_20

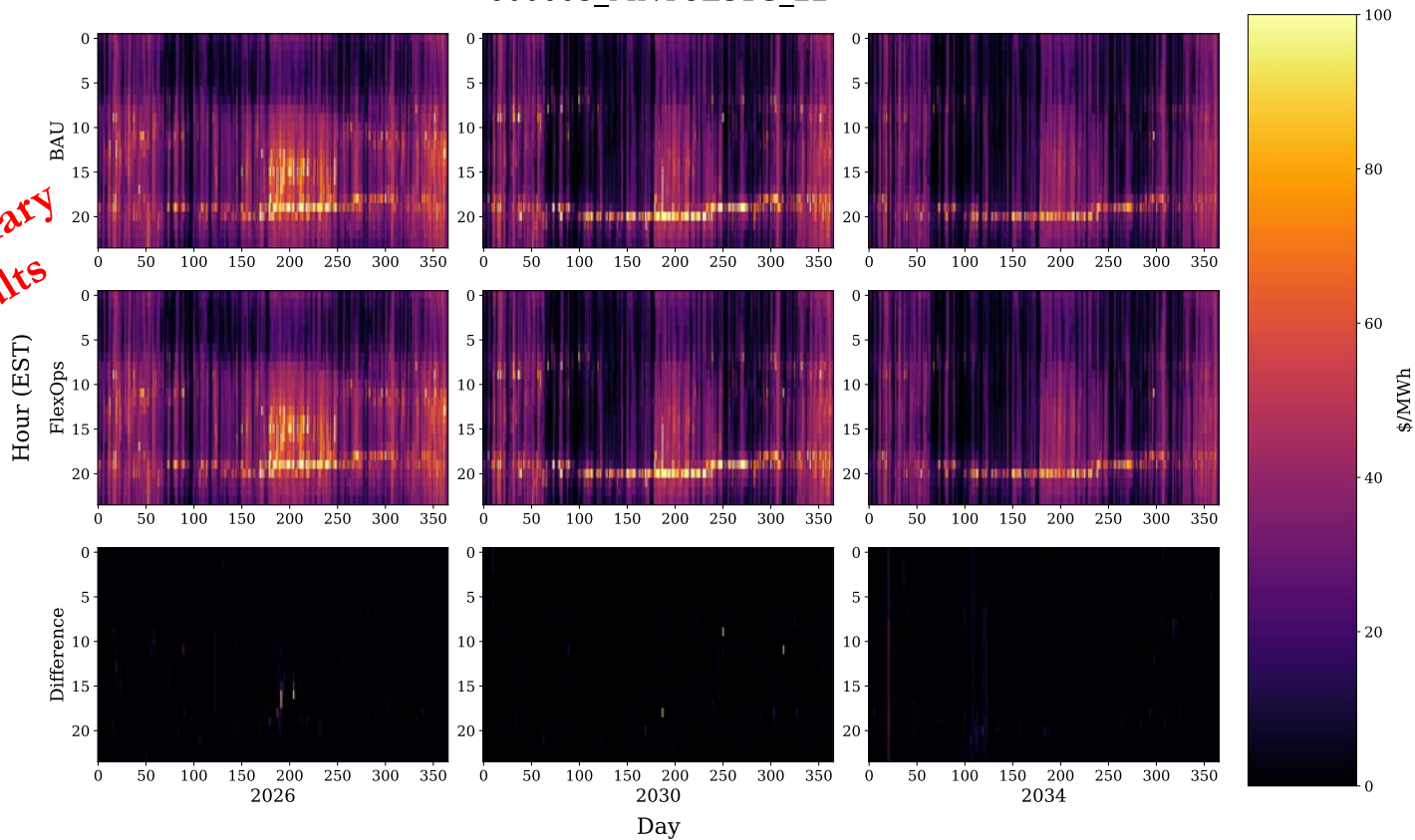
**Preliminary  
Results**



# Monticello LMP Heat Map

600005\_MNTCE31G\_22

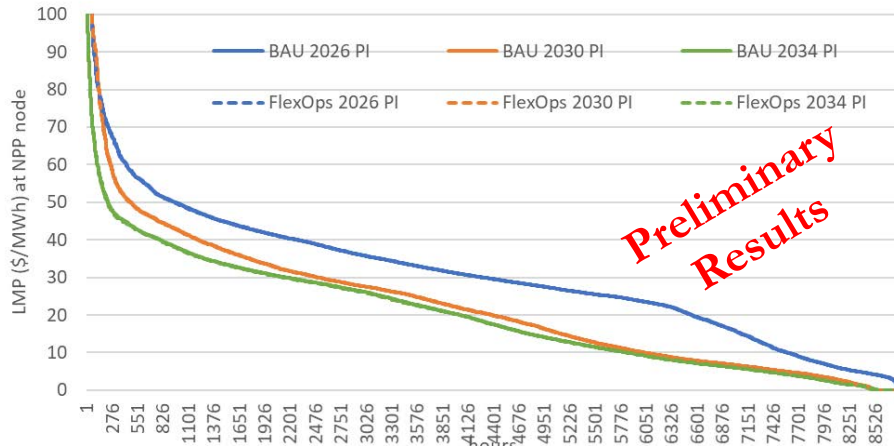
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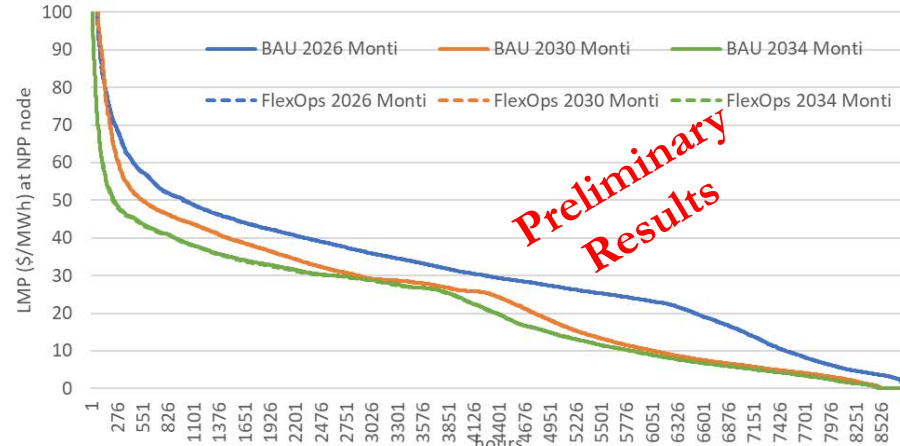


# Price Duration Curves

LMP at Prairie Island



LMP at Monti

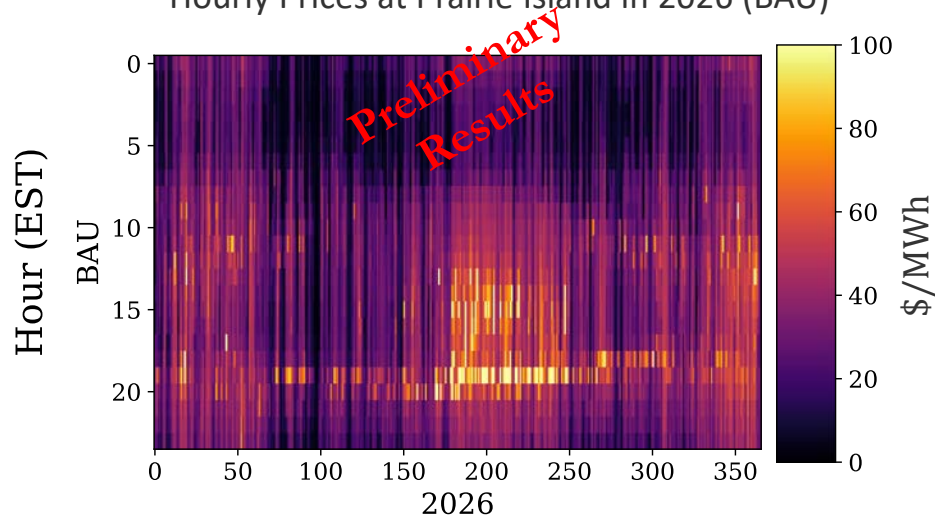


Minimum prices across the scenarios range from -0.00005 to -0.41 \$/MWh (just negative enough to cause the NPPs to flex)

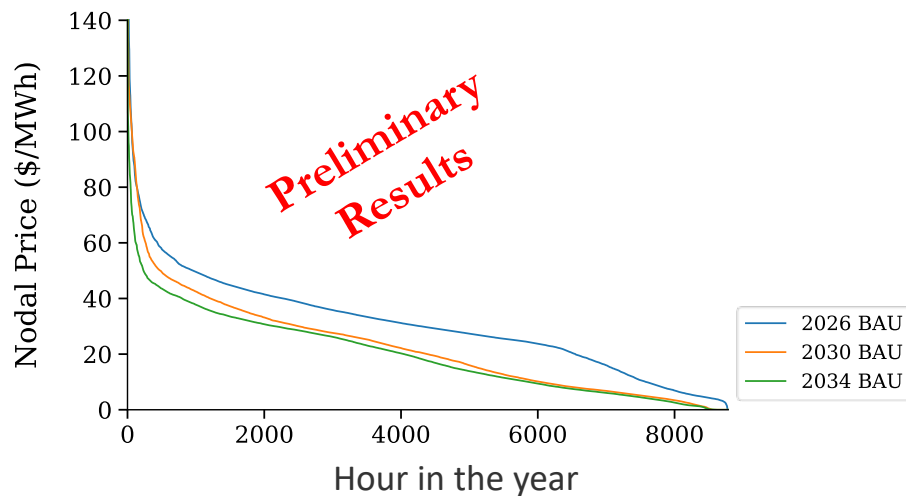
# Used Production Cost Modeling to Estimate Hourly Locational Marginal Prices (LMPs)

Estimated LMPs for each hour of the years 2026, 2030, and 2034 at both NPPs under business-as-usual (BAU) (must-run) and FlexOps (reduce generation when revenue < cost – i.e.,  $LMP < \$0/MWh$ ) operating strategies.

Hourly Prices at Prairie Island in 2026 (BAU)



Price Duration Curves for Prairie Island

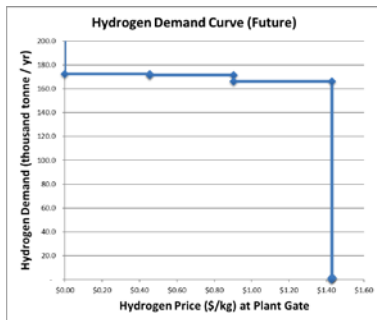


Ramping is minimal (<48 hours/yr) in FlexOps scenarios over all years

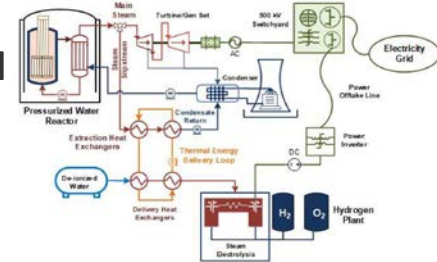
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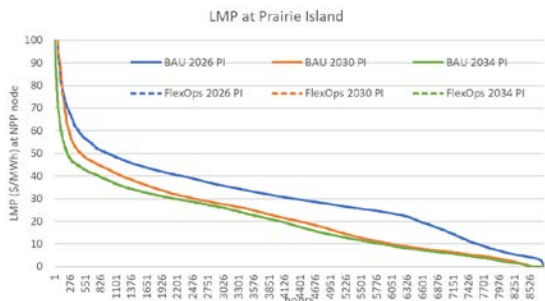


**Hydrogen System Cost and Performance Estimates**



**Hydrogen System Configuration Optimization**

**In-depth electricity system modeling**



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## HTSE Cost and Performance Characterization

- Light Water Reactor (LWR)-integrated HTSE process model developed using AspenTech HYSYS software to evaluate system mass & energy balances; model results used as basis for calculation of system performance parameters including specific energy consumption and system efficiency
  - Thermal Delivery Loop (TDL) used to supply LWR nuclear process heat for HTSE process feed water vaporization
  - Electrical power supplied by LWR for electrolyzer and balance of plant power demands; LWR power cycle model used to estimate reduction in electrical power generation resulting from diverting LWR power cycle steam to TDL to meet HTSE plant thermal demands.
- System capital costs obtained based on equipment sizing parameters computed by HYSYS process model. AspenTech Process Economic Analyzer and cost data from previous HTSE system design reports used to estimate HTSE system capital costs for present analysis.
  - Modular construction system design basis: 25 MW-dc HTSE modules assembled in offsite manufacturing facility and installed in parallel to achieve specified H<sub>2</sub> production capacity. Each HTSE module specified to include feed stream conditioning, heat recuperation, product purification, and sweep gas supply equipment. Cost reductions for modular components achieved through economies of mass production; 95% learning curve used to estimate modular system component costs for Nth-of-a-kind HTSE plant.
  - Scalable (non-modular) equipment used to provide nuclear process heat to HTSE modules, high-pressure compression of hydrogen product, and common plant support functionality (water purification, process control, etc.). Scalable equipment sizing varies with HTSE plant capacity, and capital cost reductions are realized through conventional economies of scale

Parameter	Large Scale Production System Design Basis
Stack Operating T	800°C [1]
Stack Operating P	<b>5 bar</b>
Cell Voltage	<b>1.285 V/cell</b>
Stack Inlet H <sub>2</sub> O Composition	90 mol% [1]
Steam Utilization	<b>80%</b>
Cell Area	144 cm <sup>2</sup> [1]
HTSE modular block capacity	25 MW-dc (1000x capacity increase from [1])
Cells per HTSE modular block	<b>136,000</b>
Current Density	<b>1.0 A/cm<sup>2</sup></b>
Area Specific Resistance	0.375 Ω-cm <sup>2</sup>
Operating Mode	Constant V
Sweep Gas	Air [1]
Sweep Gas Inlet Flow Rate	Flow set to achieve 40 mol% O <sub>2</sub> in anode stream outlet
H <sub>2</sub> Product Purity	99.9 mol%
H <sub>2</sub> Product Pressure	69 bar (1000 psi)
TDL Heat Transfer Fluid	Therminol-66 [2,3]
TDL transport distance	1.0 km [4]

[1] O'Brien et al, Intl J Hydrogen Energy 45 (2020)

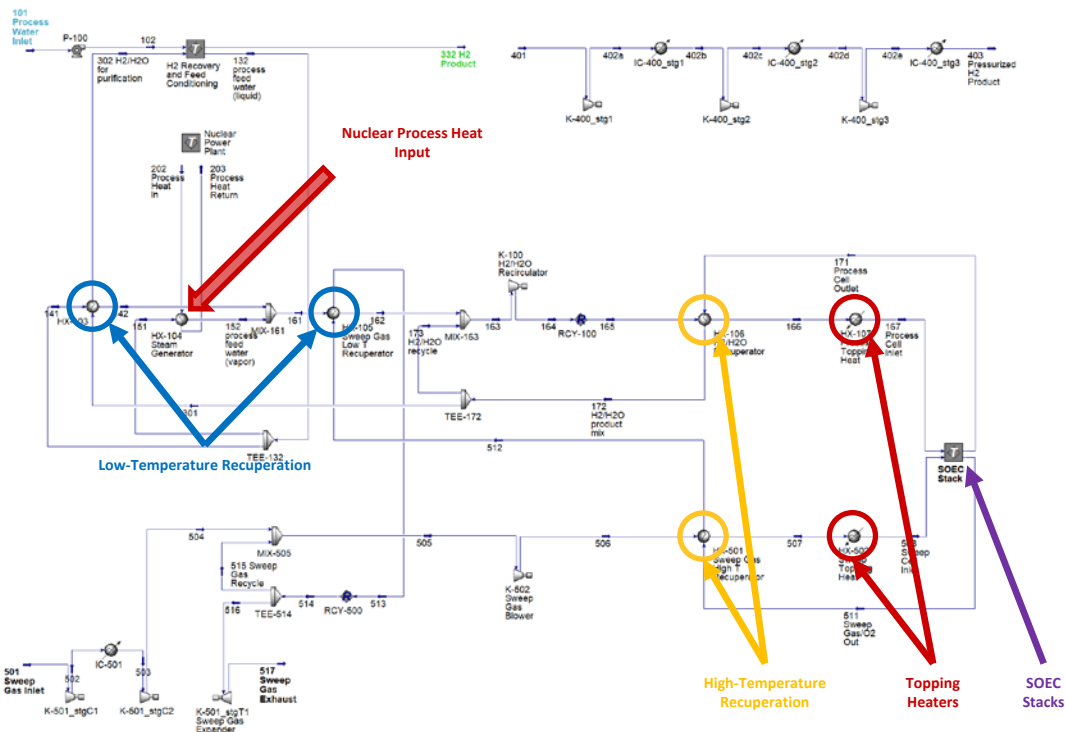
[2] O'Brien et al, INL/EXT-17-43269 (2017)

[3] Frick et al, INL/CON-18-46075 (2019)

[4] Vedros et al, INL/EXT-20-60104 (2020)

# Approach

# HTSE Cost and Performance Characterization



## Process Operating Mode Simulations

### • Normal Operating Mode

- Design point operating specifications listed in Table (right)
- Constant voltage SOEC stack operating mode results in decrease in stack operating current associated with cell degradation; Effect of stack degradation captured in capacity factor specification - HTSE process availability (95%) x cell degradation adjustment factor (95.3%) = 90.5%
- Economic model includes allowance for annual stack replacements to restore design capacity at the start of each operating year

### • Hot Standby Operating Mode

- Stack operating temperature, pressure, inlet composition, and inlet flow rate (process gas and sweep gas) maintained at nominal values using TDL steam generator, process and sweep gas blowers, electric topping heaters, and recycle of H<sub>2</sub>/H<sub>2</sub>O process gas from stack outlet and H<sub>2</sub> from product recovery
- 0% stack power during hot standby mode; stack inlet and outlet compositions equal during hot standby operating mode (zero steam utilization)
- H<sub>2</sub>O component flow rate into product recovery subprocess maintained at design point value

# Accomplishment

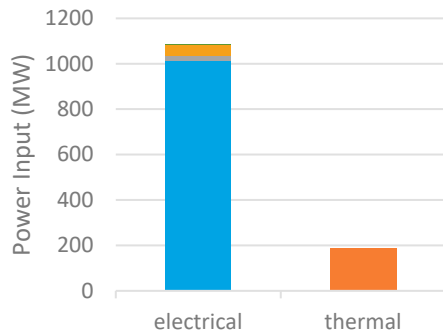
## Updated High Temperature Steam Electrolysis (HTSE) Performance and Cost Estimates to Improve Characterization of “Hot Standby Mode” and Credibility

	Large Scale H <sub>2</sub> Production Design Basis
Plant Design Capacity	1086 MW-e
Design Hydrogen Production Capacity	697 tpd
Process Power Requirement, Normal Electrical Thermal	1086 MW-ac 187 MW-t
Process Power Requirement, Hot Standby Electrical Thermal	9.3 MW-ac (0.9% nominal) 35.5 MW-t (19% nominal)
Specific Energy Consumption Electrical Thermal	37.4 kWh-ac/kg H <sub>2</sub> 6.4 kWh-t/kg H <sub>2</sub>
System H <sub>2</sub> Production Efficiency (energy content of product H <sub>2</sub> divided by electrical energy equivalent input)	88.9% HHV basis
System CAPEX (Nth-of-a-kind – NOAK)* Stack Cost Direct Capital Costs Total Capital Investment	\$155/kW-dc \$514/kW-ac \$656/kW-ac
Annual Operating & Maintenance (O&M) Costs* Fixed (labor, maintenance, overhead) Variable (stacks, water, energy excluded)	\$17.95/kWe-yr \$5.06/MWh-e

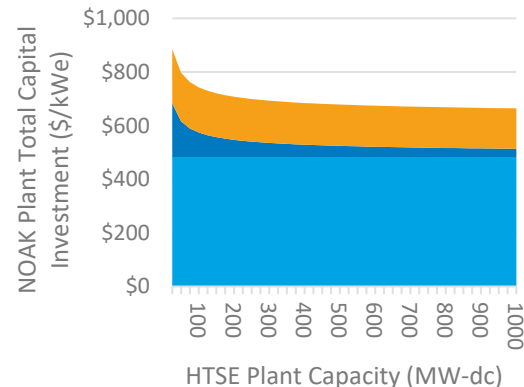
**Preliminary Results**

Improved process modeling to better estimate energy requirements (including “Hot Standby” requirements)

Established non-proprietary capital cost estimates using stack costs based on HFTO HTSE H<sub>2</sub> Production Record and balance-of-plant equipment costs estimated from AspenTech Process Economic Analyzer and literature data sources



- steam generators
- electrolyzers
- topping heaters
- compressors
- pumps



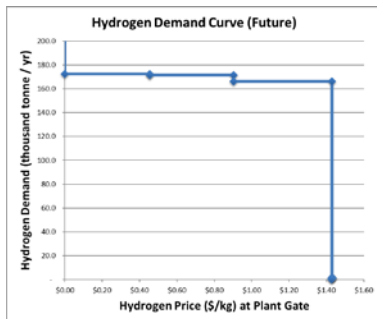
- Modular Equip
- Scalable Equip
- Indirect Costs

\* 2016 USD, scales with plant capacity

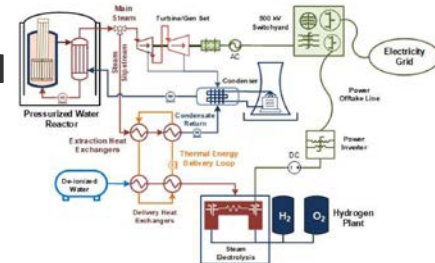
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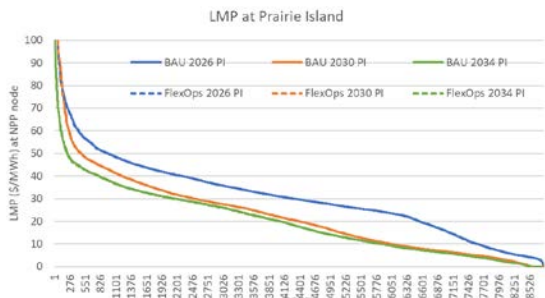


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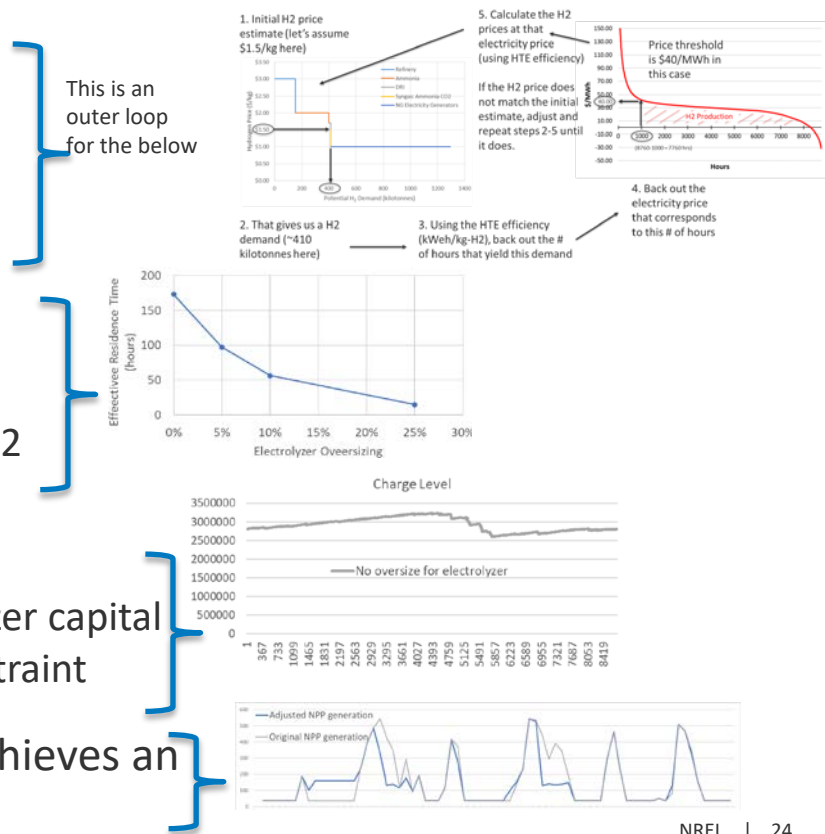
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# Price-Taker Co-optimization: Demand Curve, Electrolyzer Size, and Storage Size

- **H2 demand curve**
    - Sets “electricity price threshold”
  - **Electrolyzer size**
    - Sets minimum and maximum generation
    - Tradeoff between electrolyzer capital cost and H2 production/storage/revenues
  - **Storage size**
    - Tradeoff between storage capital cost, electrolyzer capital cost, H2 revenues, and constant H2 output constraint
- **Final result:** fixed NPP generation profile that achieves an equilibrium between all of these dimensions





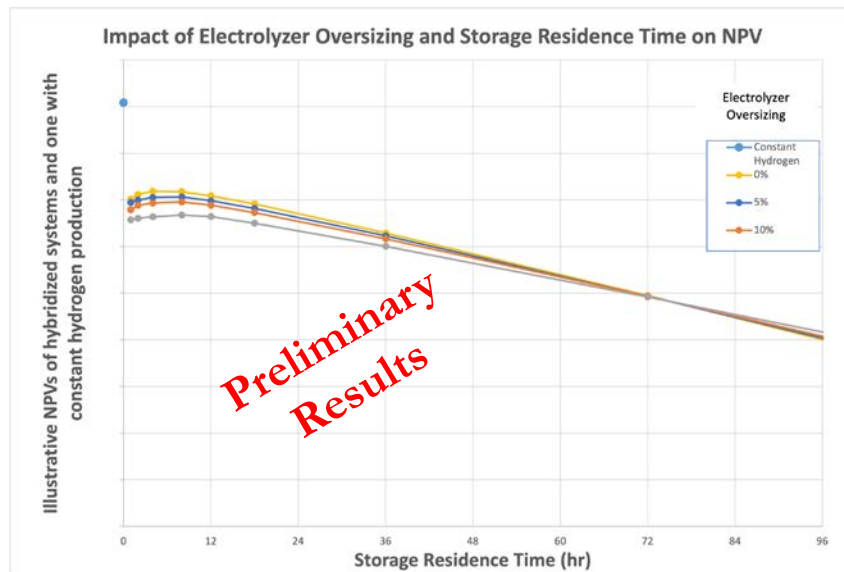
# Accomplishment

# Hybrid NPP Producing Hydrogen: Price-Taker Optimization Results

A hydrogen price greater than those in the demand curves is necessary to pay back a near-term investment.

Constant hydrogen production is found to be more profitable than hybridization. A later construction date increases the value of hybridization

When hybridized, net present value (NPV) is maximized with short storage residence times (4-8 hr) and minimum oversizing of the electrolyzer



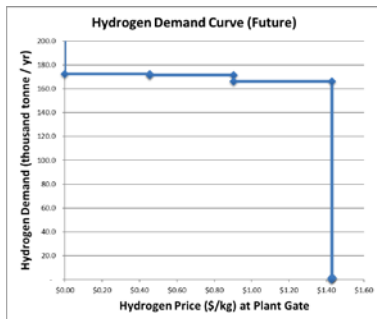
	Electrolyzer Size	Annual Hydrogen Sales	Capacity Factor in 2026
Constant Hydrogen	713 MW <sub>e</sub>	166,100 kg/yr	98%
0% Oversizing	1,037 MW <sub>e</sub>	143,608 kg/yr	58%
5% Oversizing	1,037 MW <sub>e</sub>	136,769 kg/yr	56%
10% Oversizing	1,037 MW <sub>e</sub>	130,552 kg/yr	54%
25% Oversizing	1,037 MW <sub>e</sub>	114,886 kg/yr	48%

**Preliminary Results**

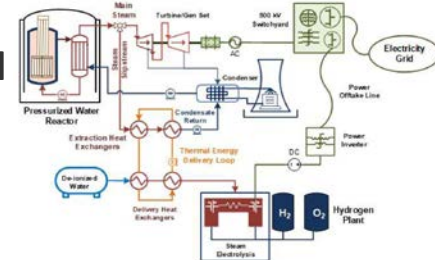
# Overall Approach

Use Best-in-Class Analysis Tools and Transfer Information Between them to Address Analysis Questions

Hydrogen Market Assessment (Delivery-adjusted demand curves)

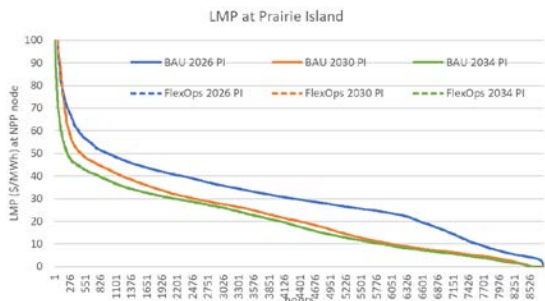


Hydrogen System Cost and Performance Estimates



Hydrogen System Configuration Optimization

In-depth electricity system modeling



	Annual APC	Annual NPP Net Operating Income	Annual System Wide Market Cost (Total)	Annual System Wide Market Cost (Net)
BAU 2026	516.1	151.3	835.5	835.5
BAU 2030	342.82	28.1	662.02	662.02
BAU 2034	237.7	-14.0	557.1	557.1
FlexOps 2026	518.0	151.9	837.4	837.4
FlexOps 2030	342.55	28.4	661.96	661.96
FlexOps 2034	236.7	-15.1	558.1	558.1
H2 2026				
H2 2030				
H2 2034				

Figures of Merit

Previous analyses\* used a price-taker approach for grid modeling. This approach addresses the impacts of changing NPP generation on grid operations – essential to estimate impacts on an integrated utility like Xcel Energy.

\* [https://www.hydrogen.energy.gov/pdfs/review20/sa175\\_boardman\\_2020\\_p.pdf](https://www.hydrogen.energy.gov/pdfs/review20/sa175_boardman_2020_p.pdf)

# Approach

# Figure of Merit: Adjusted Production Cost

$$APC_{ann} = \sum_{h=1}^{8760} \sum_{\substack{g \in \text{NSP} \\ \text{non-NPP gens}}} V_{h,g} \quad [\$/\text{hr}] \quad - \quad \underbrace{N_h}_{\substack{\text{Net Exchange with} \\ \text{NSP} \\ + \text{ if export from NSP,} \\ - \text{ if import}}} \quad * \quad \underbrace{ZP_h}_{\substack{\text{Weighted-average} \\ \text{zonal energy price} \\ \text{(LMP)}}} \quad [MWh/h] \quad * \quad [MWh/h] \quad = \quad [MWh/h] \quad * \quad [\$/\text{MWh}]$$

where

– If NSP buys:  $ZP_h = \frac{\sum_{i \in \text{selling zone nodes}} L_{h,i} * P_{h,i}}{\sum_{i \in \text{selling zone nodes}} L_{h,i}}$  Load-weighted- LMP of zone importing from

– If NSP sells:  $ZP_h = \frac{\sum_{g \in \text{NSP gens}} G_{h,g} * P_{h,i}}{\sum_{g \in \text{NSP gens}} G_{h,g}}$  Generation-weighted- LMP of NSP zone

These values will all be taken from PLEXOS outputs

# Approach

# Figure of Merit: Annual NPP Net Operating Income

$$N_{NPP,ann} = \left\{ \sum_{h=1}^{8760} \left( \sum_{p=1}^{OpResNum} RP_{h,p} R_{h,p} \right) + EP_h G_h + HP * H2_h \right\} - C_{NPP,base} - \sum_{j=1}^{Ops} O_{flex,j}$$

Operating Reserve Income (H2 scenario only)     Energy Income     H2 Income     NPP fixed costs     Additional cost for Flex Ops

All hours operated in alternate conditions

[\$/MWh x MWh/h]     [\$/MWh x MWh/h]     [\$/kg x kg/h]     [\$/yr]     [\$/h]

These values will all be taken from PLEXOS outputs, with the addition of the H2 demand curve (H2 price for a given amount of H2 produced) from ANL

# Approach

# Figure of Merit: Annual System Wide Market Costs

Since Xcel NSP currently does not have a formal policy for how to incorporate the H2 revenues into rate case accounting, we calculate two variants to bookend the benefit that H2 revenues provide to the system wide market cost

A) Total Annual System Wide Market Costs:

$$C_{cust,tot} = APC_{ann} + \overbrace{C_{NPP,ann}}^{\text{annual cost to operate the NPP}} + \overbrace{C_{non-NPP,annFix}}^{\text{annual fixed cost to operate the non-NPP generators}}$$

[\$/yr]
[\$/yr]
[\$/yr]

H2 revenues **do not help** to offset the cost that is passed on to the rate payers

B) Net Annual System Wide Market Costs:

$$C_{cust,net} = APC_{ann} + C_{NPP,ann} + C_{non-NPP,annFix} - \overbrace{\sum_{h=1}^{8760} HP * H2_h}^{\text{H2 revenues}}$$

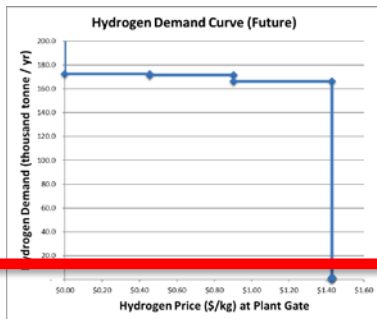
[\$/yr]
[\$/yr]
[\$/yr]
[\$/kg x kg/h]

H2 revenues **help** to offset the cost that is passed on to the rate payers

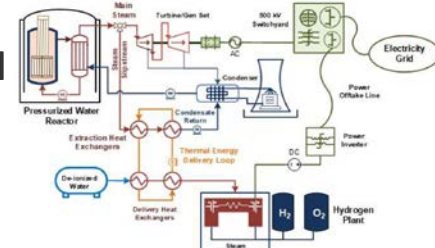
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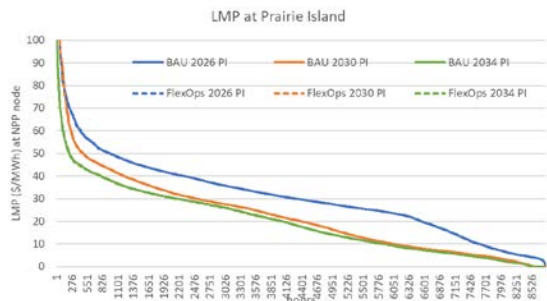
**Hydrogen Market Assessment**  
(Delivery-adjusted demand curves)



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**In-depth electricity system modeling**



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H2 2026				
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H2 2034				

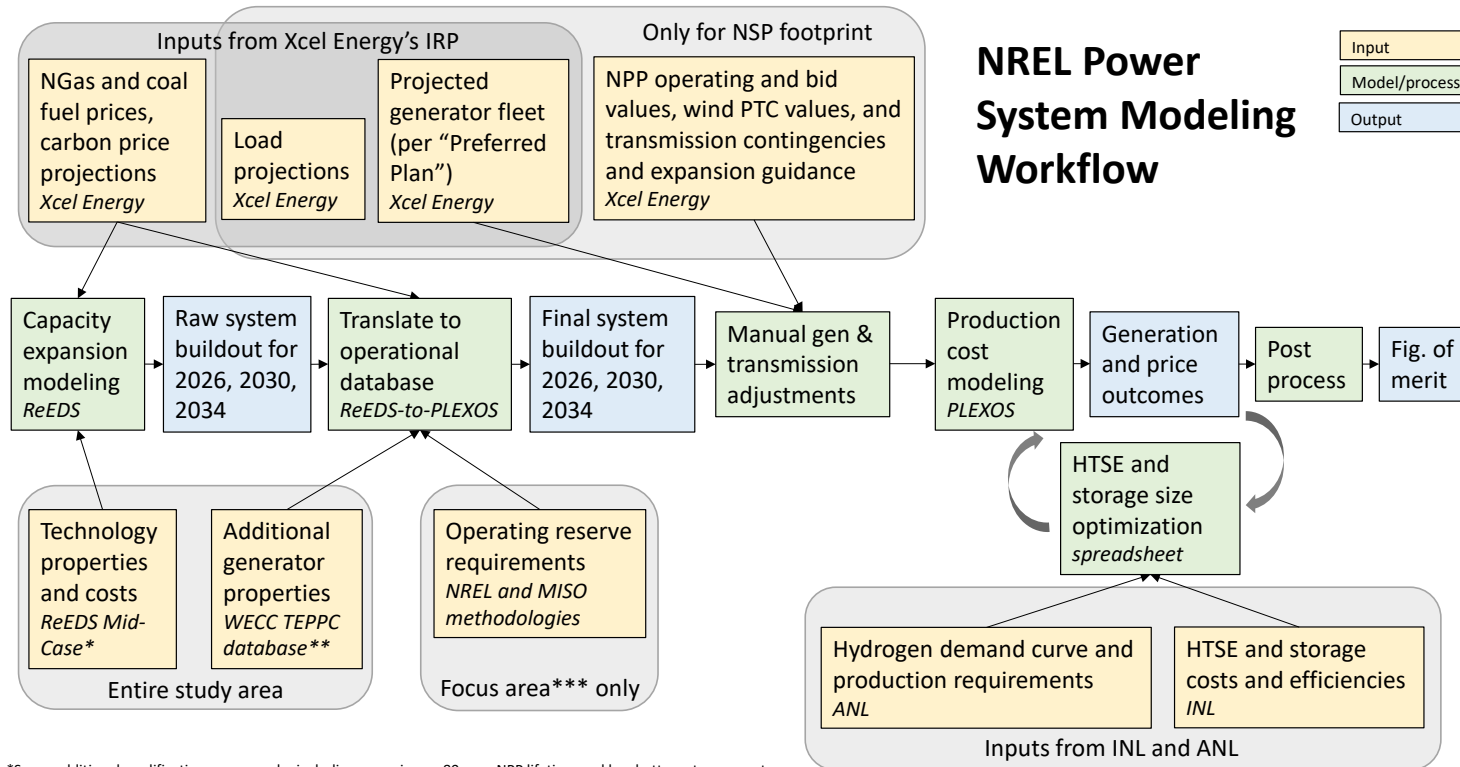
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\* [https://www.hydrogen.energy.gov/pdfs/review20/sa175\\_boardman\\_2020\\_p.pdf](https://www.hydrogen.energy.gov/pdfs/review20/sa175_boardman_2020_p.pdf)

# Approach

## Detailed Workflow for Power System Modeling



\*Some additional modifications were made, including assuming an 80-year NPP lifetime and low battery storage costs

\*\*Including min up/down time, forced outage rates, start costs, minimum generation level, max ramp rates

\*\*\*"Focus area" zones are run at a nodal resolution with full unit commitment and operating reserve representation

# Preliminary Estimates of Figures of Merit for BAU and FlexOps Scenarios

**Preliminary Results**

	Annual APC	Annual NPP Net Operating Income	Annual System Wide Market Cost (Total)	Annual System Wide Market Cost (Net)
<b>BAU 2026</b>	516.1	151.3	835.5	835.5
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<b>FlexOps 2030</b>	342.55	28.4	661.96	661.96
<b>FlexOps 2034</b>	236.7	-15.1	556.1	556.1
<b>H2 2026</b>	<b>Under Development</b>			
<b>H2 2030</b>				
<b>H2 2034</b>				

- All metrics decrease as between 2026 and 2034 due to an increase in lower marginal cost resources (e.g., wind and solar PV)
- FlexOps more favorable than BAU in 2030+2034
- NPP loses money in 2034 for both BAU & FlexOps due to a reduction in energy prices

Values shown with more significant figures than is warranted by the method and data so that the viewer can see very small differences between results.



# Summary

- Multiple inputs are important to estimate the potential for hybridization
  - Existing and potential regional hydrogen markets
  - Future electricity market prices
  - Equipment costs and performance especially when operated flexibly (high temperature steam electrolyzers)
- Business structures and cases inform key metrics and potential for investments
  - Variations in structures will inform technique for optimizing the scale and operating strategy of hybrid production systems
- Analysis can
  - Identify key parameters for making hybrid nuclear power plants profitable for utility owners
  - Identify key performance parameters where additional R&D is needed for these technologies to be profitable

# Thank You

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[www.nrel.gov](http://www.nrel.gov)

NREL/PR-6A20-81122

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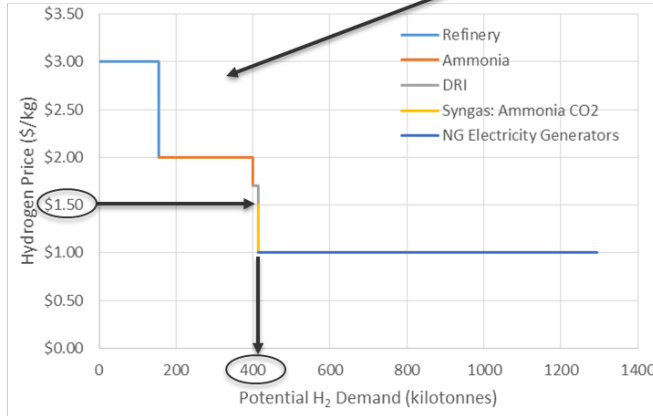
# Technical Backup and Additional Information

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# Approach

## Developed a Unique Iterative Methodology for Hybrid System Optimization with Varying Electricity Prices

1. Initial H2 price estimate (let's assume \$1.5/kg here)

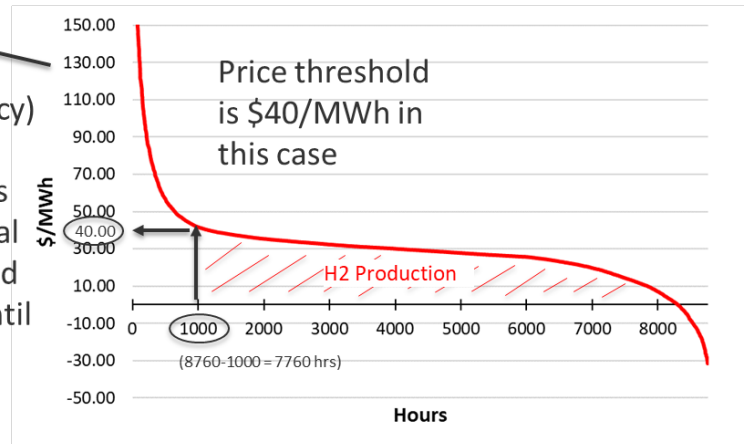


2. That gives us a H2 demand (~410 kilotonnes here)

3. Using the HTE efficiency (kWh<sub>e</sub>/kg-H<sub>2</sub>), back out the # of hours that yield this demand

5. Calculate the H2 prices at that electricity price (using HTE efficiency)

If the H2 price does not match the initial estimate, adjust and repeat steps 2-5 until it does.



4. Back out the electricity price that corresponds to this # of hours