



Evaluating the Durability of Balance of Systems Components Using C-AST

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The Motivation for the BoS Study

- BoS components include: connectors, cables, **branch connectors**, fuses (discrete), fuse blocks.
- Durability of BoS components has very limited research examination.
- Quantifiable replacement rate for $t < 25y$! 50y: TBD.
-2 DOE AOP projects presently examining: components, occurrence, cost.
- Consequences of degradation and failure:
module offline, string offline, tripped inverter,
system shutdown, arc fault, fire!!!
- With limited publicity, latter consequences are BoS-centric.



Example of PV fires in Italy.
Fiorentini et. al., PVRW 2020.



Goals of the C-AST Project



C-AST chamber during operation (MiMo test sites).

General:

C-AST typically used with MiMos, so:

- Develop characterization methods.
- Identify degradation modes.
- Demonstrate ability to distinguish known bad components using C-AST.

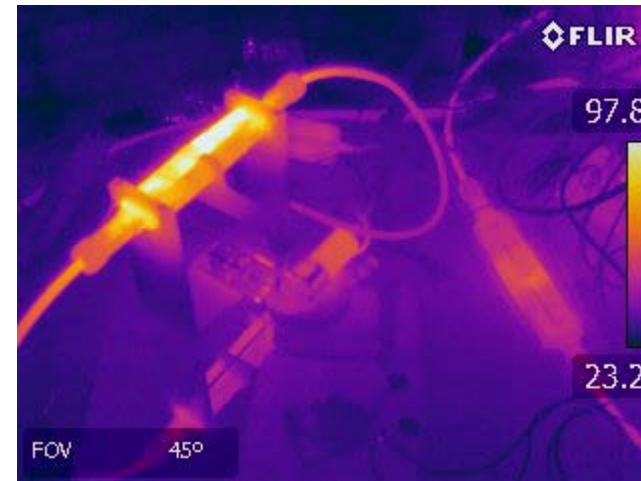
Specific:

- Identify most damaging stressors (environments, from C-AST sequences).
- Can static load or mechanical vibration contribute to failure?

Look For in This Presentation

-External mechanical actuation greatly affected the result.-

- How is examination implemented?
- What component(s) are affected?
- How to further validate the result?



Optional encore slides on j-box adhesives & pottants.

Branch Connectors: The Scenario



- Utility provider experiencing ~30% failure rate in their power transfer chain, attributed to branch connectors.
 - “Failure” means overheating, softening, physical distortion.
 - Observable ΔT in thermographic imaging.
 - Worst consequence: broken circuit, arc, fire.
- Component makes & models kept confidential in this presentation.



Branch Connectors: The Approach

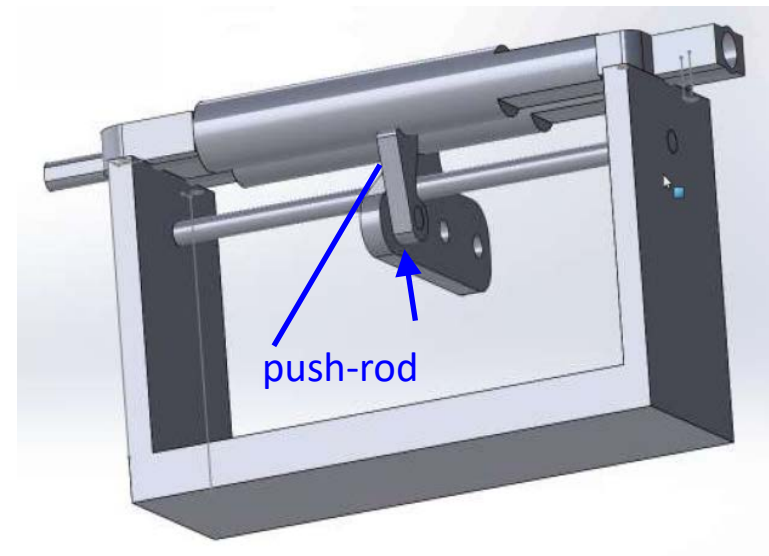
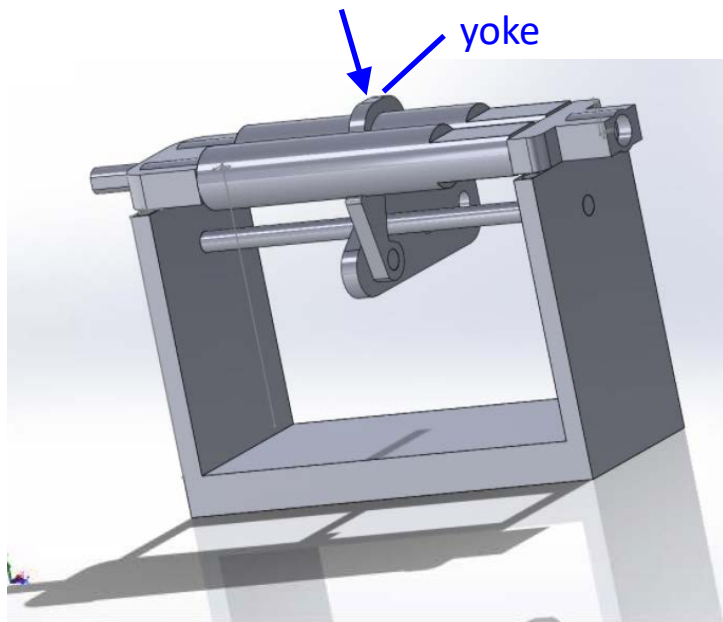


- Compare **C-AST** to UL standard tests.
- # and contribution of bad components unknown.
Evaluate proximate system components: cable connectors, fuse, branch connectors.
- **Develop fixture and software using benchtop experiments (1 replicate).**
- Use custom C-AST fixture for mechanical actuation (6 replicates).



A BENCHTOP, SAMPLE INTEGRATED PUSH/PULL MECHANICAL FIXTURE WAS USED

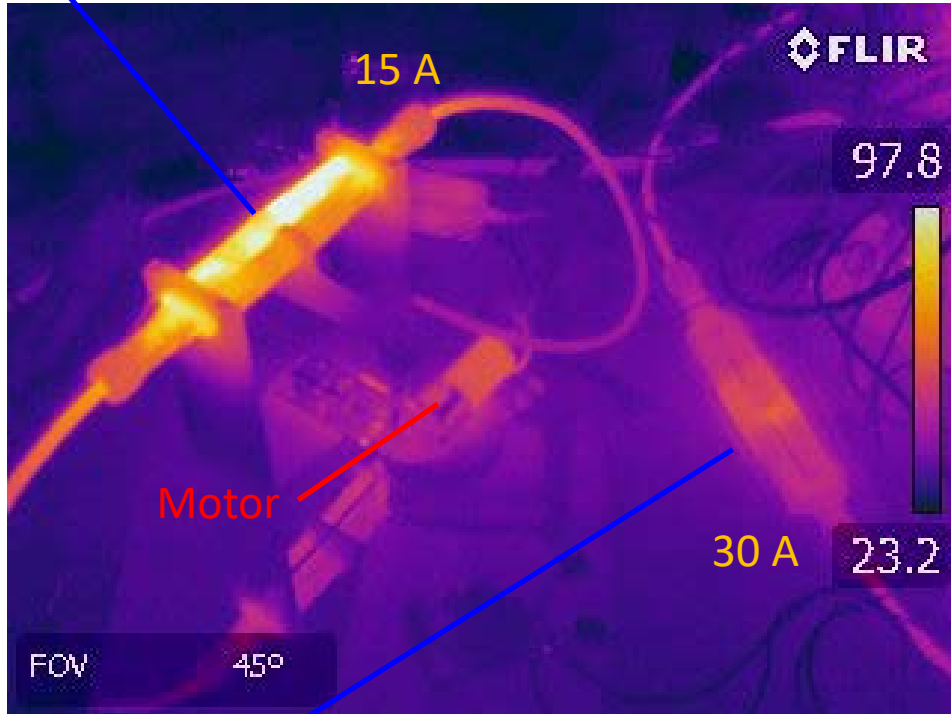
- “Yoke and push-rod” concept design concept was selected. (vs. “wedge”).
- Specimen assembly is part of the actuation mechanism.
- Deflection used: 3 mm (initial) → 1 mm → 0.5 mm (C-AST).
- Benchtop version run with 16 rpm DC motor.
- C-AST version uses hydraulic actuators, 1/8 – 10 Hz.



SolidWorks model of mechanical fixture

Mechanical Actuation Readily Affected Test Results

Dynamic (actuated) sample assembly



Static (unactuated) assembly

Operation:

- Start at 10 A / 20 A applied DC current.
- Current incremented 1 A each day to failure.

Observed limits:

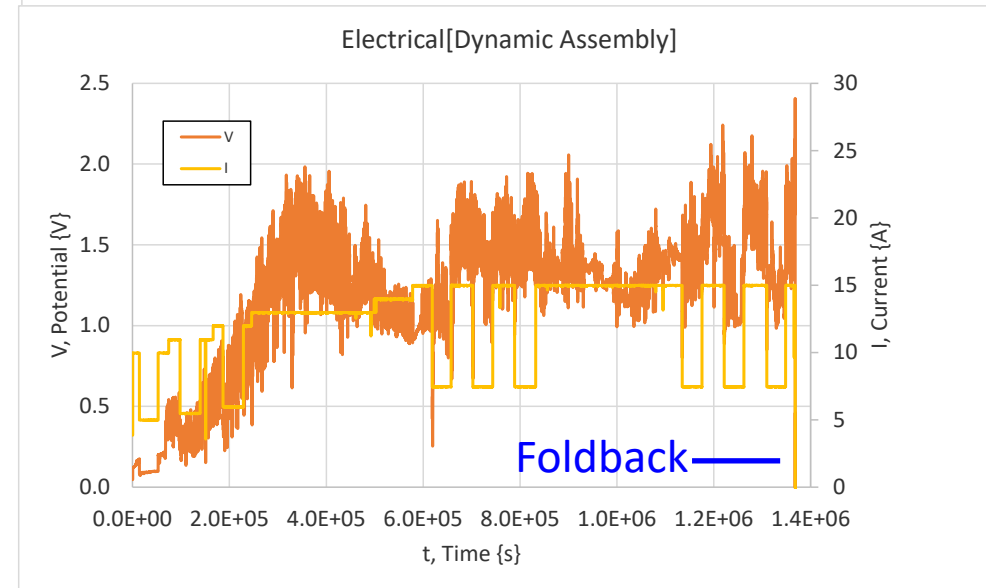
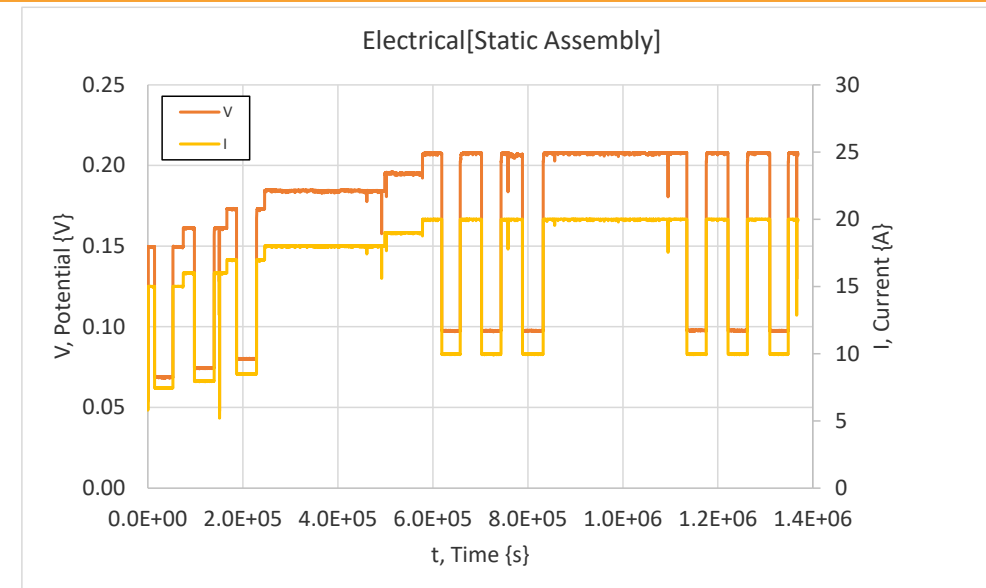
- Static assembly: fails at 35 A (equiv. labels for 30 A).
- Dynamic assembly: fails at 15 A. $T_{\text{external}} > 130^{\circ}\text{C}$.
- UL connector test: no failure BC @ 37.5 A. $T_{\text{external}} 44^{\circ}\text{C}$.

Failure modes:

- Static assembly: fails at fuse (open circuit).
- Dynamic assembly: fails at fuse/branch.
 - Local arcing suspected from: smoke, local melting of plastic, discolored metal pins, increased fuse resistance.

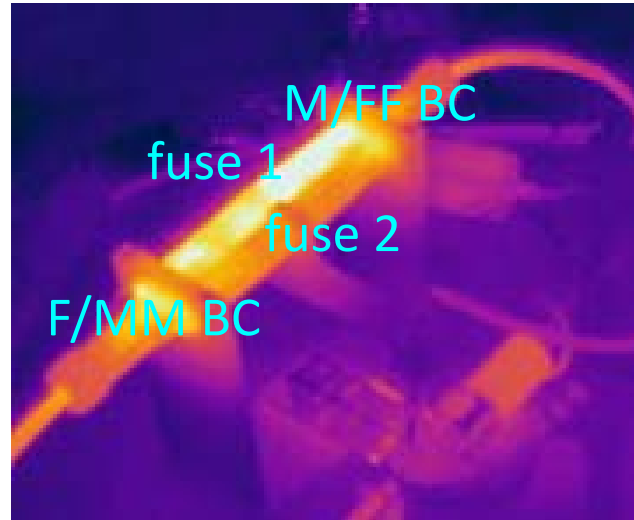
I-V: Mechanical Actuation Gave an Immediate, On-going Affect

- LabView software for C-AST developed in benchtop experiments.
 - I, V are logged per sample assembly.
 - Data binned & analyzed in 1 minute intervals.
 - Optional “burst” mode to log @ 100 kHz.
-
- Example ($\delta=1$ mm) compares I, V for static & dynamic assemblies.
 - I, V scales (y-axis) are different, static vs. dynamic.
 - V quickly becomes more variable for dynamic.
-
- Foldback protection ($> V_{fb}$) was extended from 1 to 5 to 25 s.
 - Q: what would you use to simulate an inverter?

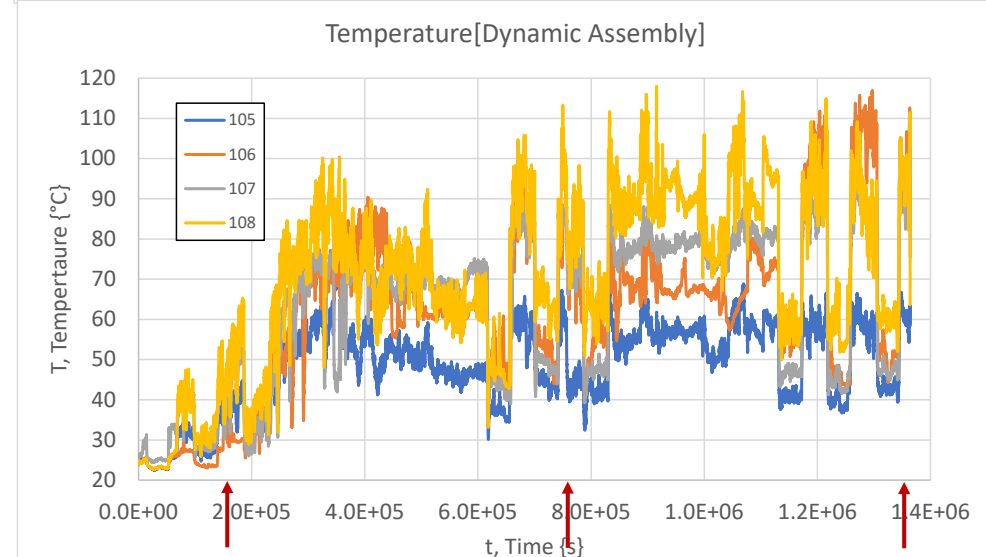
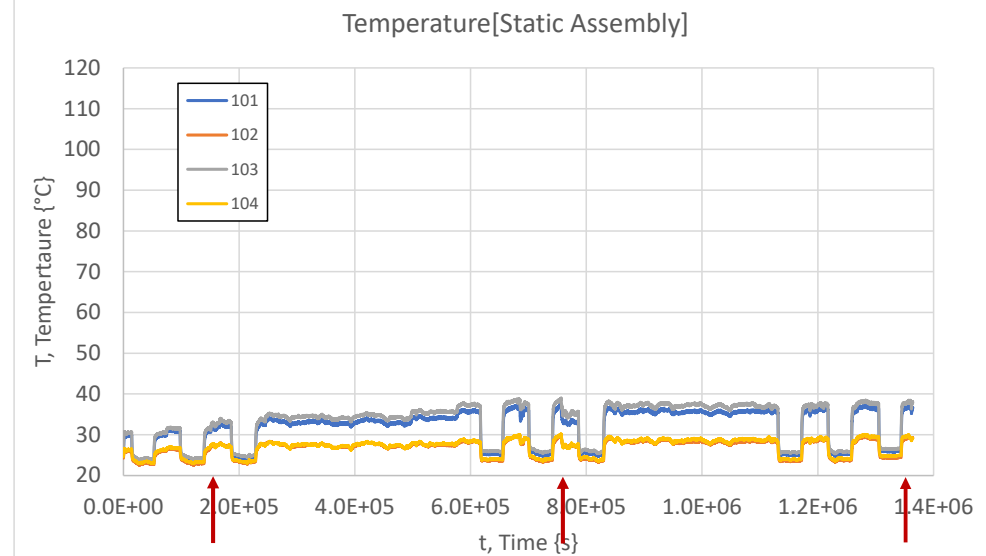


T: Mechanical Actuation Gave an Immediate, On-going Affect

- T is logged per site (F/MM BC, fuse 1, fuse 2, M/FF BC).
 - Discrete T-type thermocouples in sheet package.



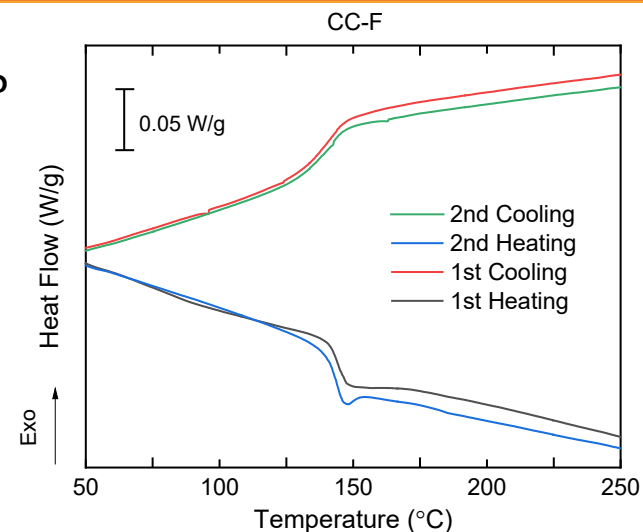
- Example ($\delta=1$ mm) compares T for static & dynamic assemblies.
 - Scale (y-axis) same for static & dynamic.
 - FLIR vs. TC: exact hottest spot difficult to predict.
 - Helpful to know: t_{onset} , what components affected.



Data from experiment 4. Red arrows indicate approximate read point for FLIR imaging.

DSC & FTIR Identify Connector Ends Are Polycarbonate

Q: What is the phase transition temperature, what material is implied for black deformed plastic?
→DSC and FTIR examination of unaged samples.

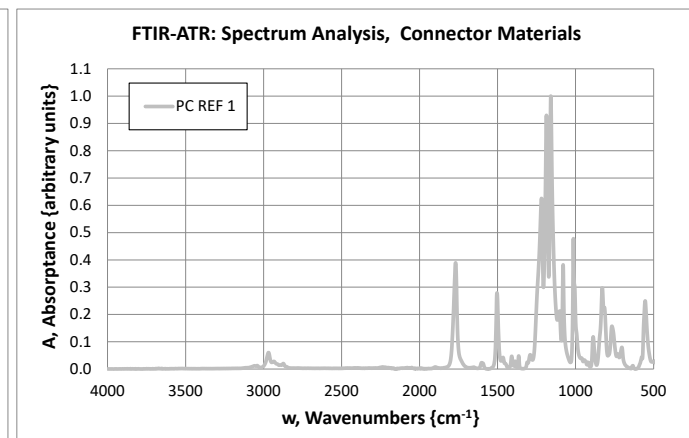
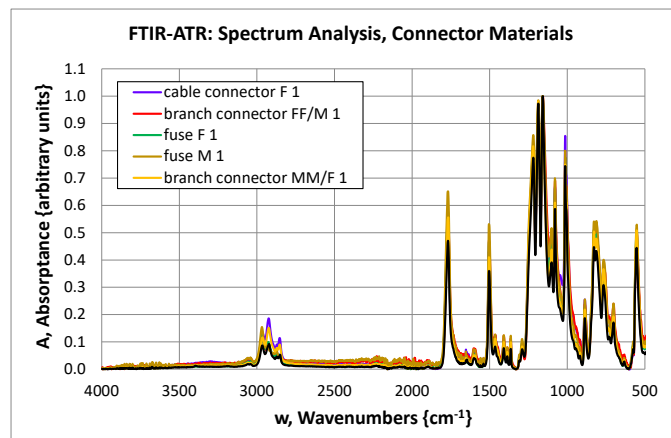


DSC for cable connector, female end (plastic).

- Suspect hard structural polymer (PC, ABS, etc) from handling samples.
- T_{glass} of $142 \pm 5^\circ\text{C}$ (AVG \pm 2 S.D.) suggests material is amorphous PC.
- All samples gave similar response (scans from $-90 - 200^\circ\text{C}$), including:
cable connector, branch connector, fuse connector ends.

- Cable-, branch-, fuse- connectors have same FTIR spectra.
 - Similar to polycarbonate reference sample.
 - 2 measurements from separate pieces each component.
 - FTIR spectra verified on both F and M connector ends.

⇒ Suspect PC containing carbon black.



FTIR (left) for all component ends and (right) PC reference.

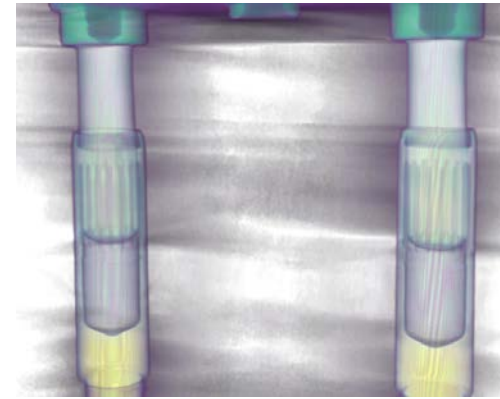
XCT: Different Sample Locations, Temperatures May Dominate Between Field & “C-AST”

- Figures: X-ray Computed Tomography imaging of field- and accelerated tested-samples.
- Field samples show asymmetry not present on unaged samples.
- Accelerated samples: bulge + contrast proximate to solder.

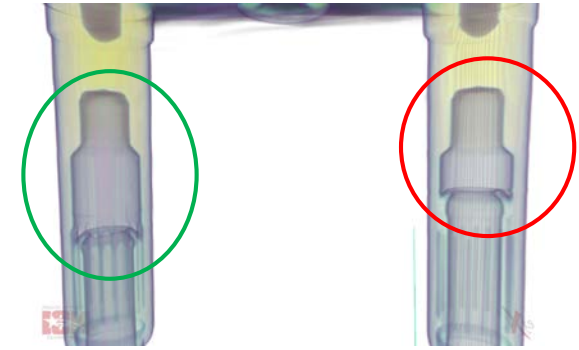
- Convolute spring component shape unchanged.
 - $T_{\text{forge}} \text{ Cu} \sim 900^{\circ}\text{C}$. $T_{\text{melt}} \text{ Cu} 1085^{\circ}\text{C}$.
- Aluminum bronze fuse holder shape unchanged.
 - $T_{\text{softening}} \text{ Al/Cu} \sim 315^{\circ}\text{C}$. $T_{\text{melt}} \text{ Al/Cu} > 550^{\circ}\text{C}$.
- Solder may contribute to failure.
 - $T_{\text{melt}} \text{ Sn/Ag/?Cu?} \sim 220^{\circ}\text{C}$.

plastic $\Rightarrow 142^{\circ}\text{C}$ realized in field.

solder $\Rightarrow 220^{\circ}\text{C}$ realized in accelerated test.



Unaged metal pins, utility provider
(opposite end)



Metal pins, utility provider.



Unaged metal pins, utility provider.



Metal pins, benchtop $\delta = 3 \text{ mm}$.

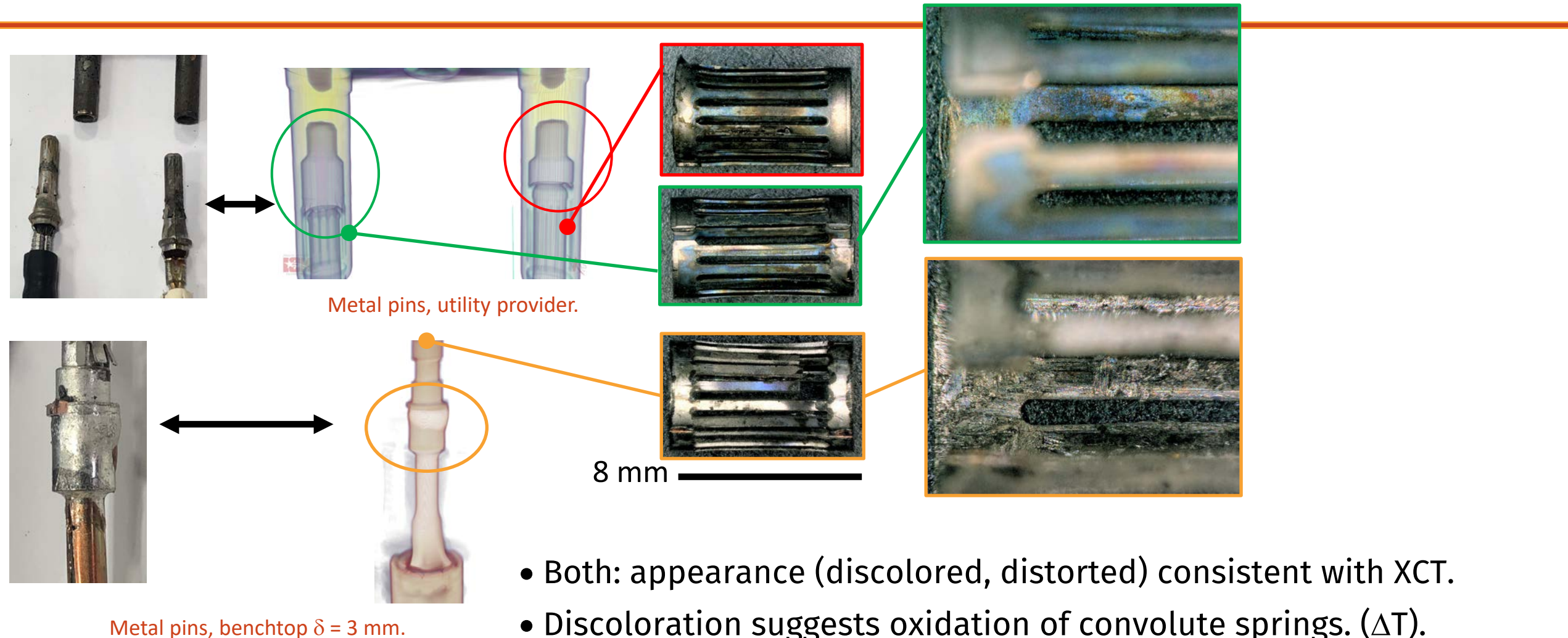
The Destructive Failure Analysis Procedure Following XCT

1. Remove (mill) external plastic.
 - Retain plastic for F/A (FTIR, DSC).
 - Inspect internal metal components relative to XCT.
 - Methods: camera, optical microscopy, SEM/EDX.
2. Extract (cut, unfold) convolute spring from F metal pins.
 - Inspection, methods as above.

convolute spring, extracted from unaged metal pin



Optical Microscopy: Oxidation of Spring, with Mechanical Wear for $\delta = 3$ mm



- Both: appearance (discolored, distorted) consistent with XCT.
- Discoloration suggests oxidation of convolute springs. (ΔT).
 - More localized discoloration in benchtop specimen.
- Scuff marks (ends, interior) suggest wear during accelerated test.

Present Status

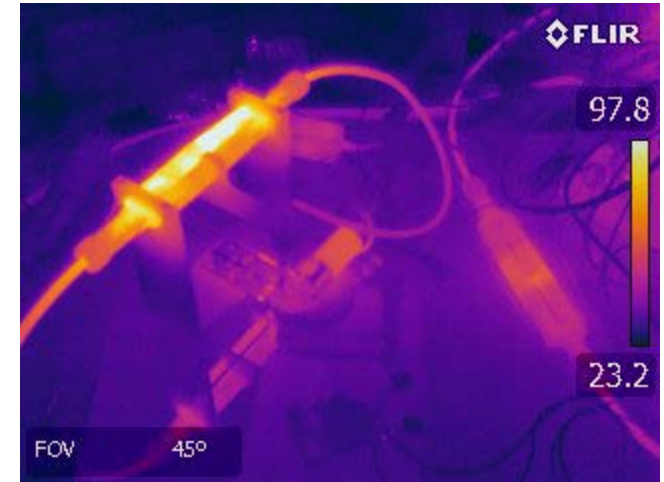
Branch Connectors:

- On-going failure analysis: solder vs. spring, $\delta = 1$ mm.
 - Do we still see wear?
- Static assembly branch connectors through round 1 of C-AST (10 A).
- Dynamic C-AST branch connector assembly pending.
 - Will effect of mechanical actuation be observed as in benchtop experiments?
 - Will effect of weathering be observed?
- May apply second round of C-AST (increased current).
- Final comparison at IEEE PVSC 2022.

Remember From This Presentation

-External mechanical actuation greatly affected the result.-

- How is examination implemented?
 - sample integrated push/pull mechanical fixture*
- What component(s) are affected?
 - static: fuse (internal).*
 - with actuation: BC/fuse (observed for field).*
- How to further validate the result?
 - mechanical wear observed for $\delta = 3\text{mm}$.*
 - pending C-AST @ $\delta = 0.5\text{mm}$.*



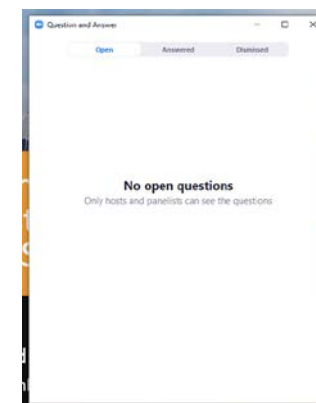
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👉 Please add to the "Questions and Answers" or contact: David.Miller@nrel.gov

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