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Transient Stability Study of a Real-World Microgrid with 100% Renewables

Yaswanth Nag Velaga¹, Jing Wang¹, Annabelle Pratt¹, Laurence Abcede²,
Nagadev Shamukh²

¹ National Renewable Energy Laboratory

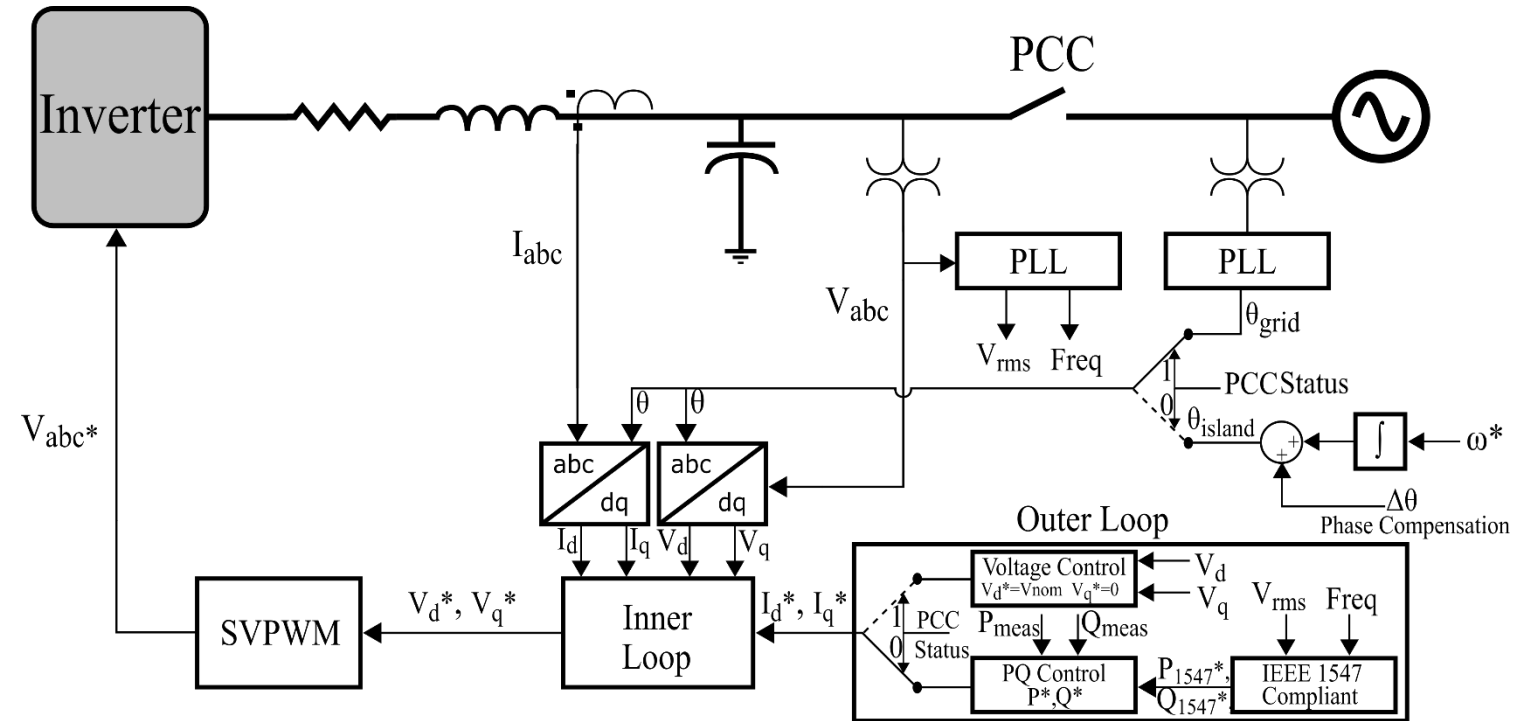
² San Diego Gas & Electric



- Transient stability of multiple grid-forming and grid-following inverters in a 100% renewable microgrid is not studied.
- High-fidelity electromagnetic transient (EMT) model of a real-world microgrid is required.
- Inverter models need to match field deployed studies.
- Different dynamic operating conditions are required to study inverter model response.
- Outcome of the study will assist the field deployment.

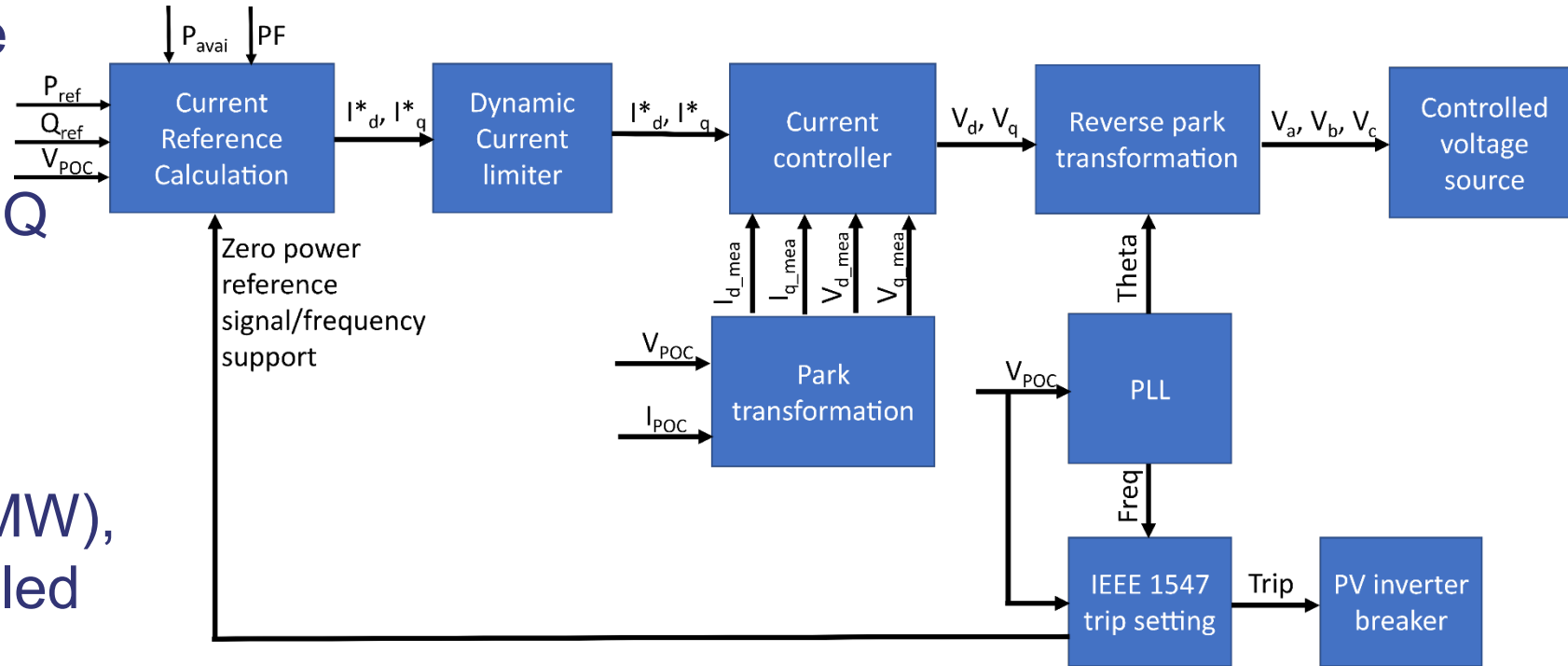
GRID FORMING INVERTER (GFM)

- Average switch model with DC/AC inverter dynamics.
- Operational modes:
 - VF control (startup)
 - PQ control (grid-connected)
 - VF control islanding master (islanded mode)
- IEEE 1547-2018 compliant in PQ control mode.
- Smooth islanding transition is possible by adding the phase angle difference between grid and self generated phase angle to GFM phase angle.
- Grid supporting functions: 1) Real/reactive power priority 2) Ride-through mode.
- SES1 and 2 (BESS) are modeled as GFM inverters.



GRID FOLLOWING INVERTER (GFL)

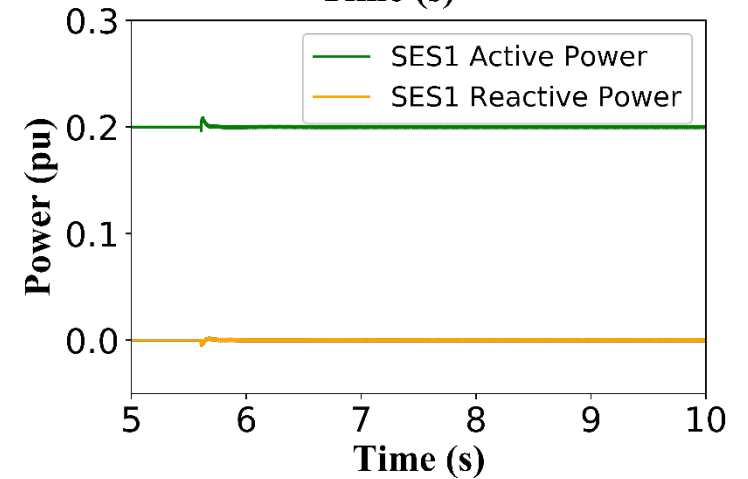
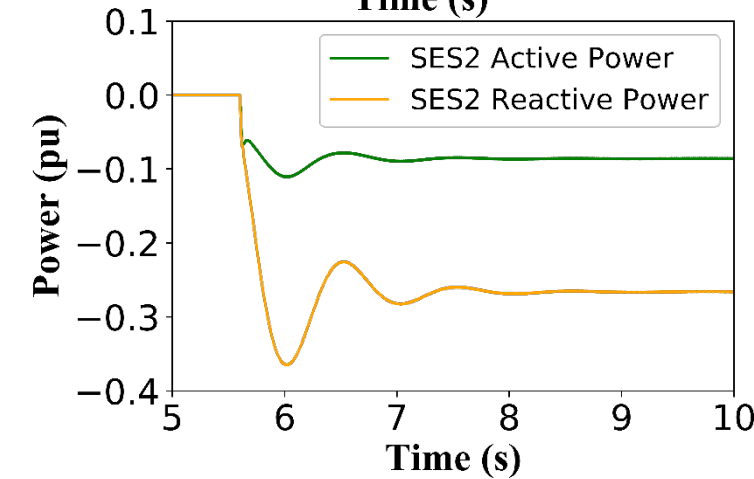
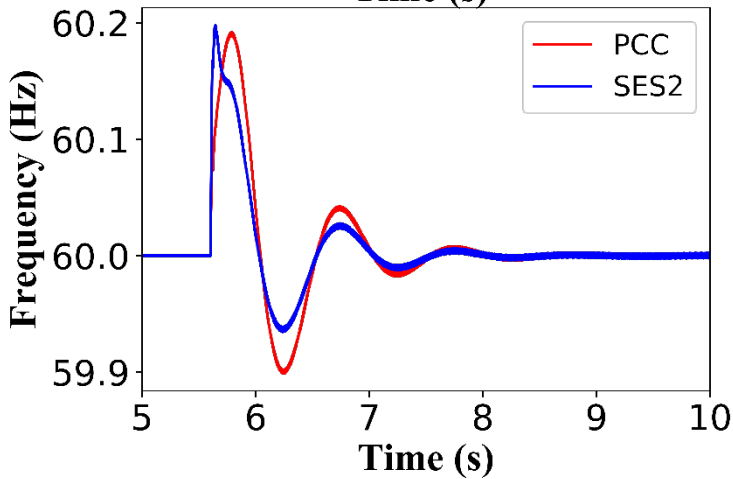
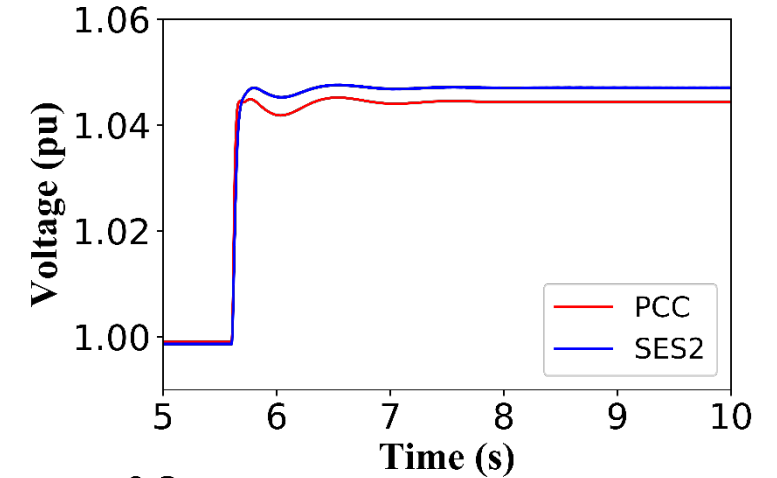
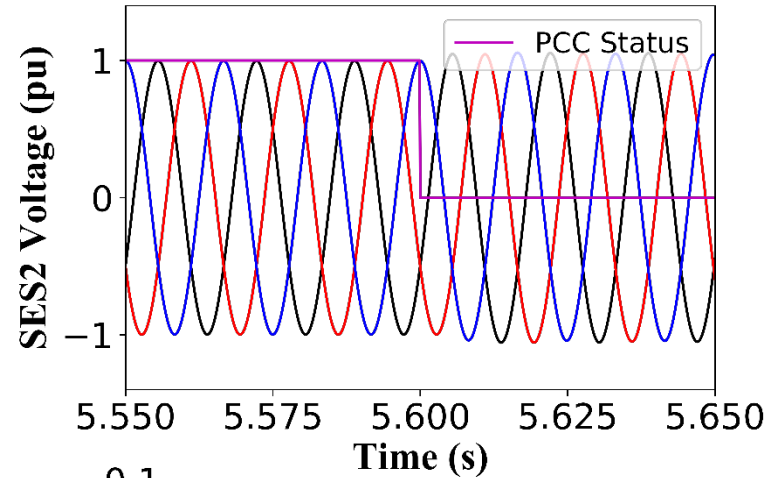
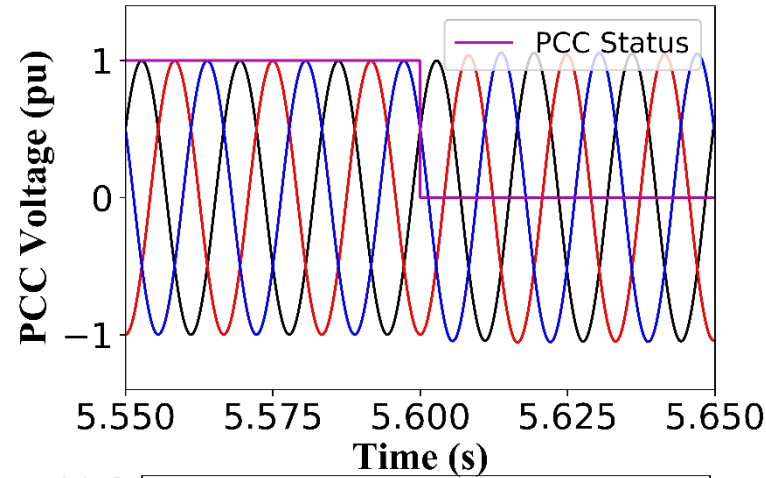
- Voltage controlled source average model.
- GFL model can work in PQ control or smart inverter function (volt-var with var priority).
- PV1 (26 MW), PV2 (6.5 MW), and rooftop PV are modeled as GFL inverters.
- PV1 is IEEE 1547-2018 compliant and rooftop PV are IEEE 1547-2003 compliant.
- PV1 is aggregated and modeled using 20 GFL inverters of 1.3 MW each.
- Rooftop PV is aggregated as 82 inverters of different ratings and locations.



SIMULATION SETUP AND TEST SCENARIOS

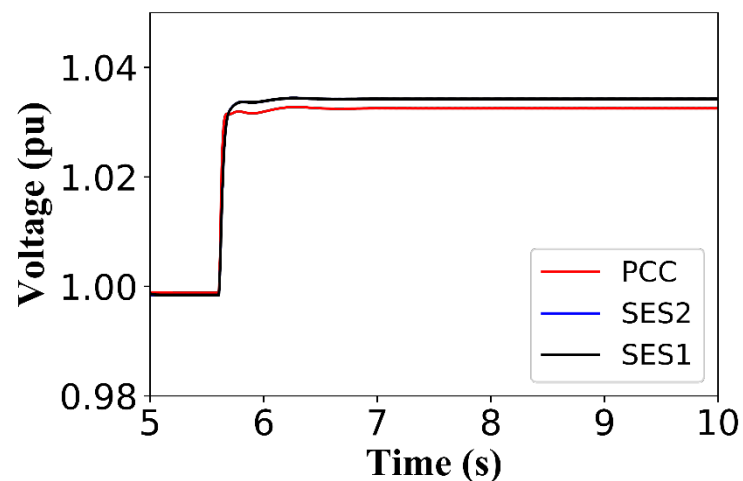
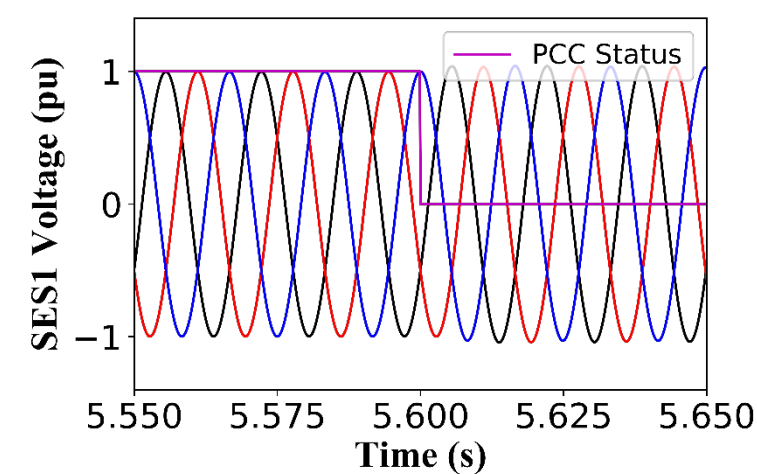
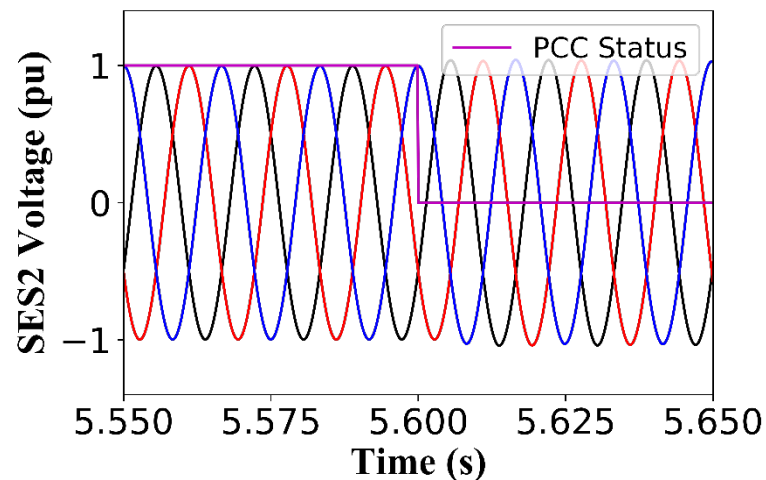
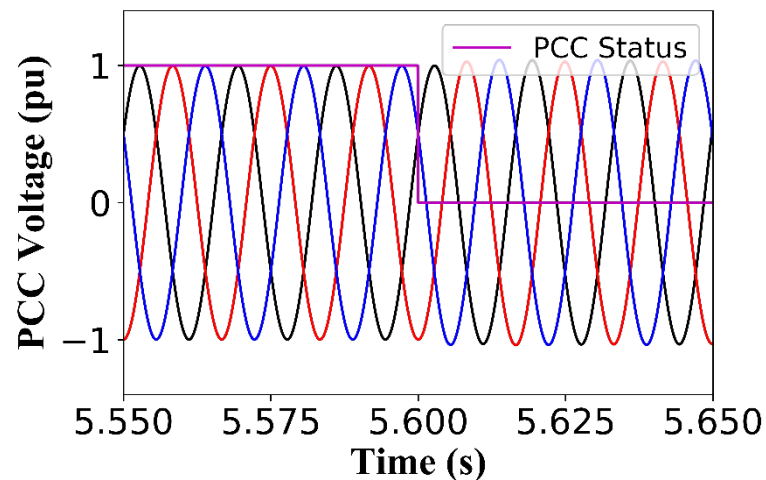
- High-fidelity PSCAD model has 106 inverters including SES1, 2 & 3.
- Borrego model is split into three networks using Bergeron model; 1) transmission, Ckt1 with rooftop, SES1, 2 and PV1; 2) Ckt2 with rooftop, PV2; 3) Ckt3 with rooftop.
- Due to the limitation of traveling wave time, simulation time step is fixed at 25 μ s.
- PV1 is not included in the test scenarios due to light loading conditions.
- Morning load and solar data from SDG&E are used for the test scenarios.
- Different dynamic test scenarios are simulated to evaluate the stability and reliability of 100% renewable microgrid.
 - Scenario #1: Unplanned islanding with SES1 in GFL and SES2 in GFM
 - Scenario #2: Unplanned islanding with SES1 & 2 in GFM (Isochronous mode)
 - Scenario #3: Unplanned islanding with SES1 & 2 in GFM (droop mode)
 - Scenario #4: Black start of Ckt1

SCENARIO #1: SES1 (GFL) AND SES2 (GFM)



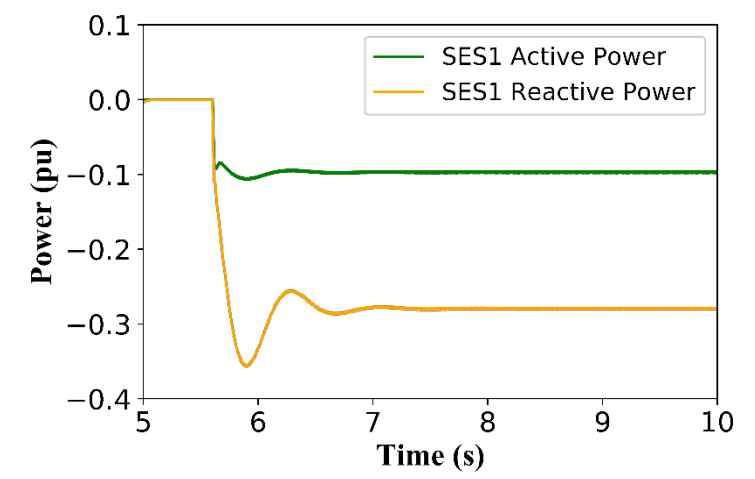
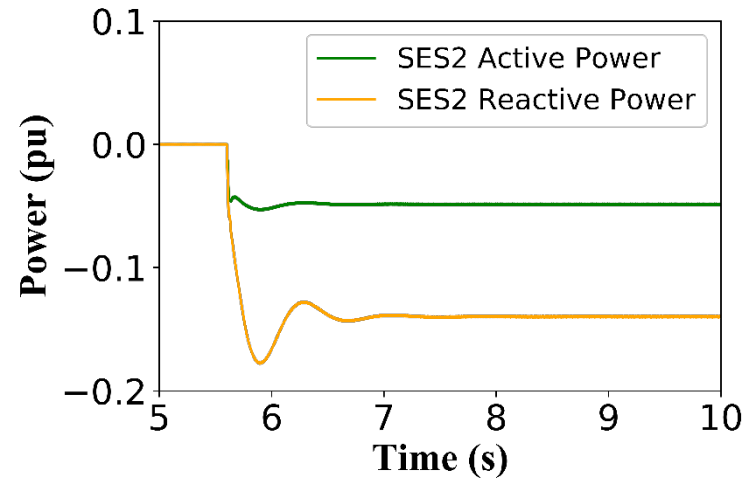
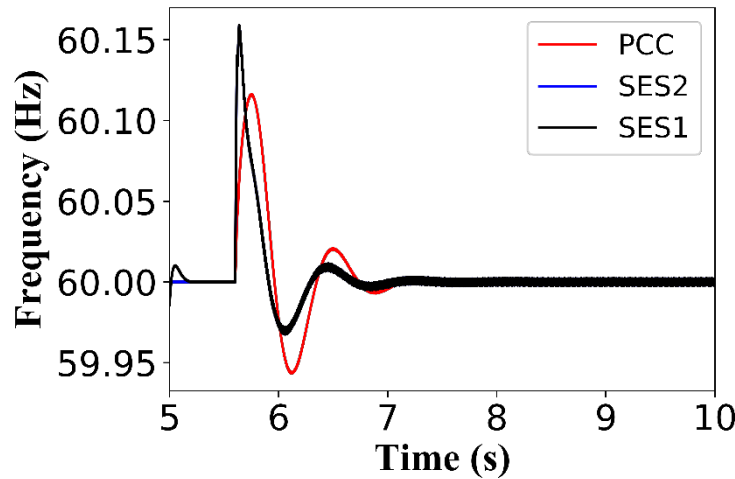
- Microgrid frequency overshoots by 0.2 Hz and dampens within 3 sec.
- SES2 power measurements show the settling time of 2 sec.

SCENARIO #2: SES1 AND SES2 (GFM VF CONTROL, ISOCHRONOUS MODE)



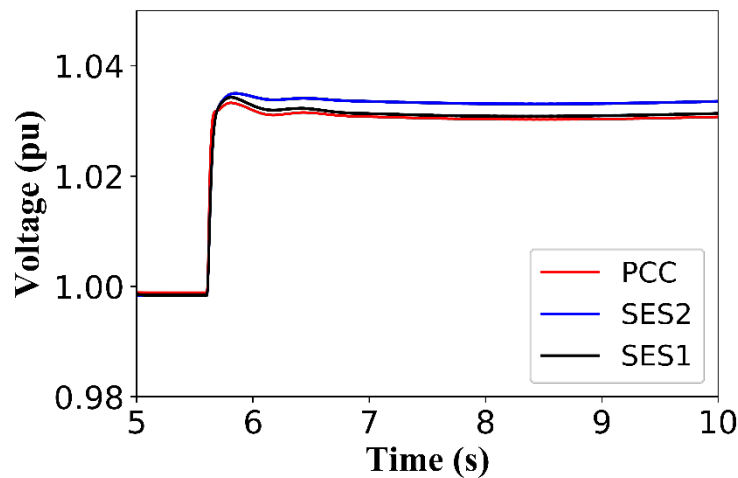
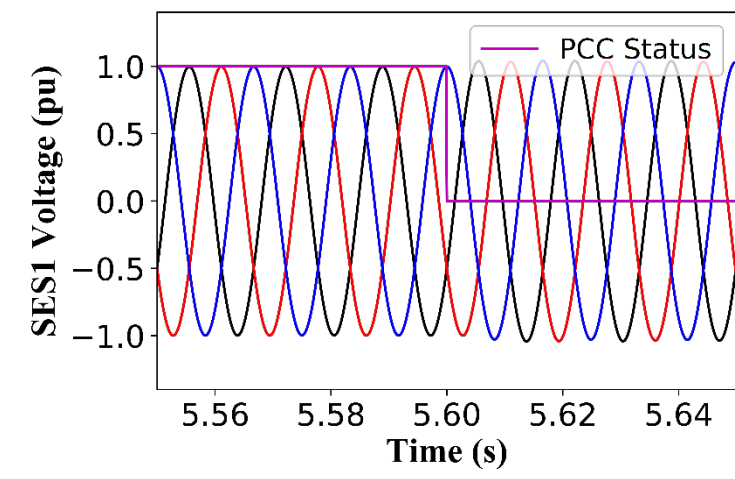
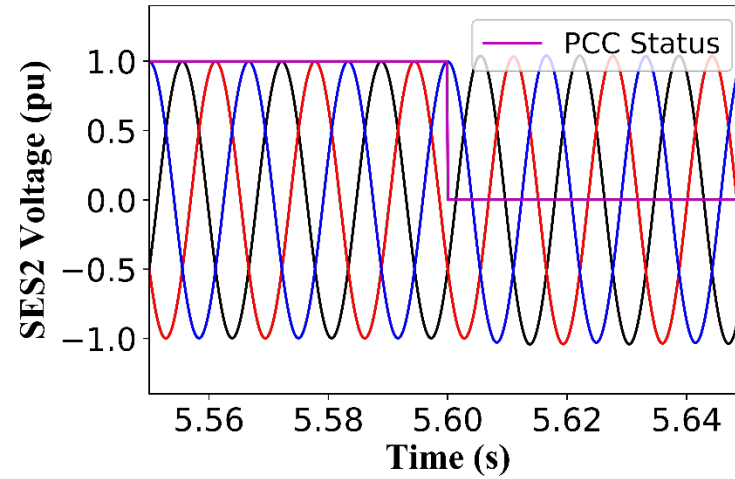
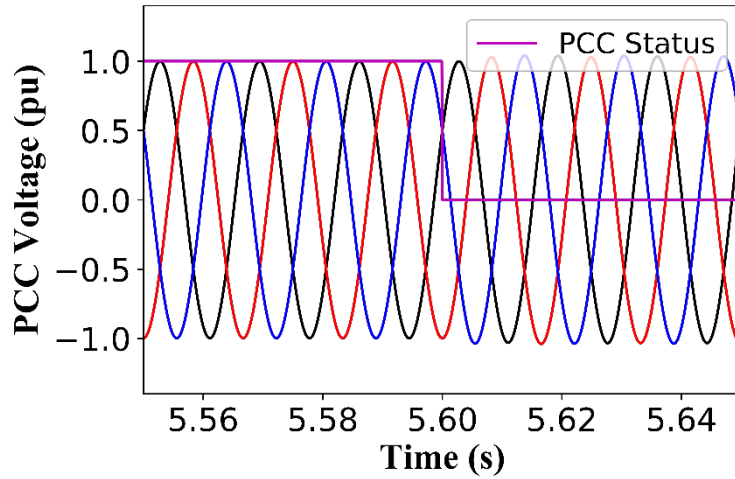
- Instantaneous voltage of PCC, SES1, and 2 show the smooth transition from grid-connected to islanded.
- SES1 and 2 terminal voltage rises to 1.03 p.u. due to excess reactive power in the microgrid.

SCENARIO #2: SES1 AND SES2 (GFM VF CONTROL, ISOCHRONOUS MODE)



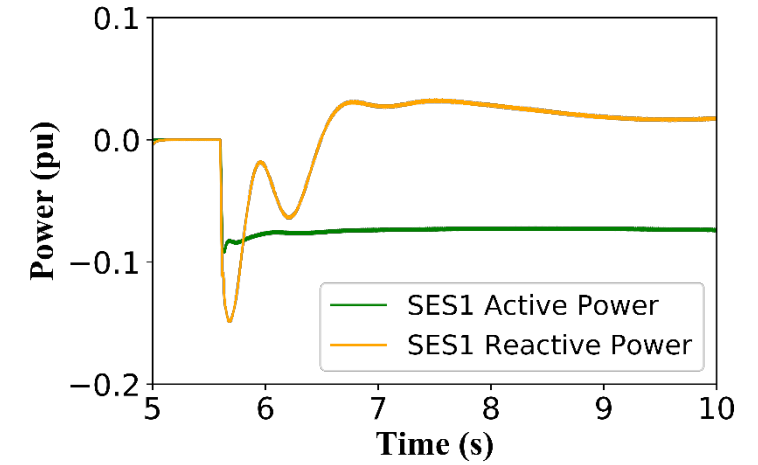
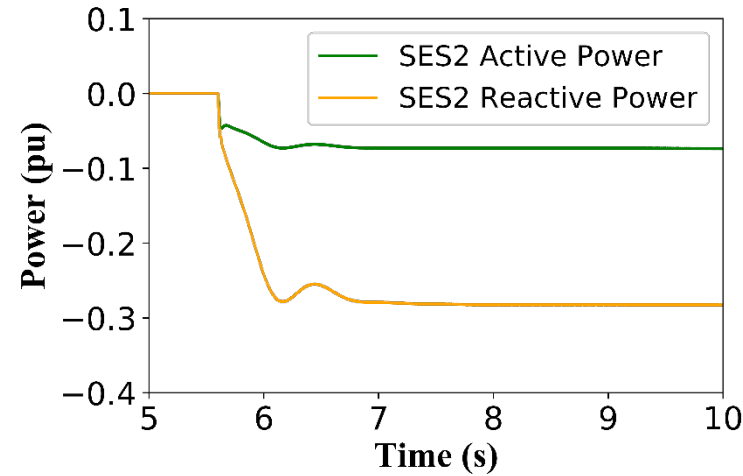
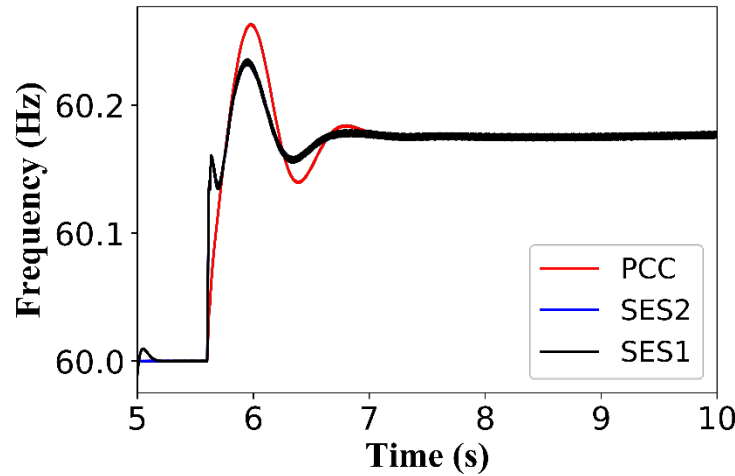
- Frequency result show the maximum overshoot of 0.15 Hz.
- Damped frequency oscillations settling time is 1.5 sec.
- SES3 is not required to inject any power because frequency is within deadband limit.
- Results show that scenario #2 provides better transient response than scenario #1.

SCENARIO #3: SES1 AND SES2 (GFM VF CONTROL, DROOP MODE)



- SES1 & 2 droop constants are set to 4%.
- PI control in outer loop is changed to PD control for stability.

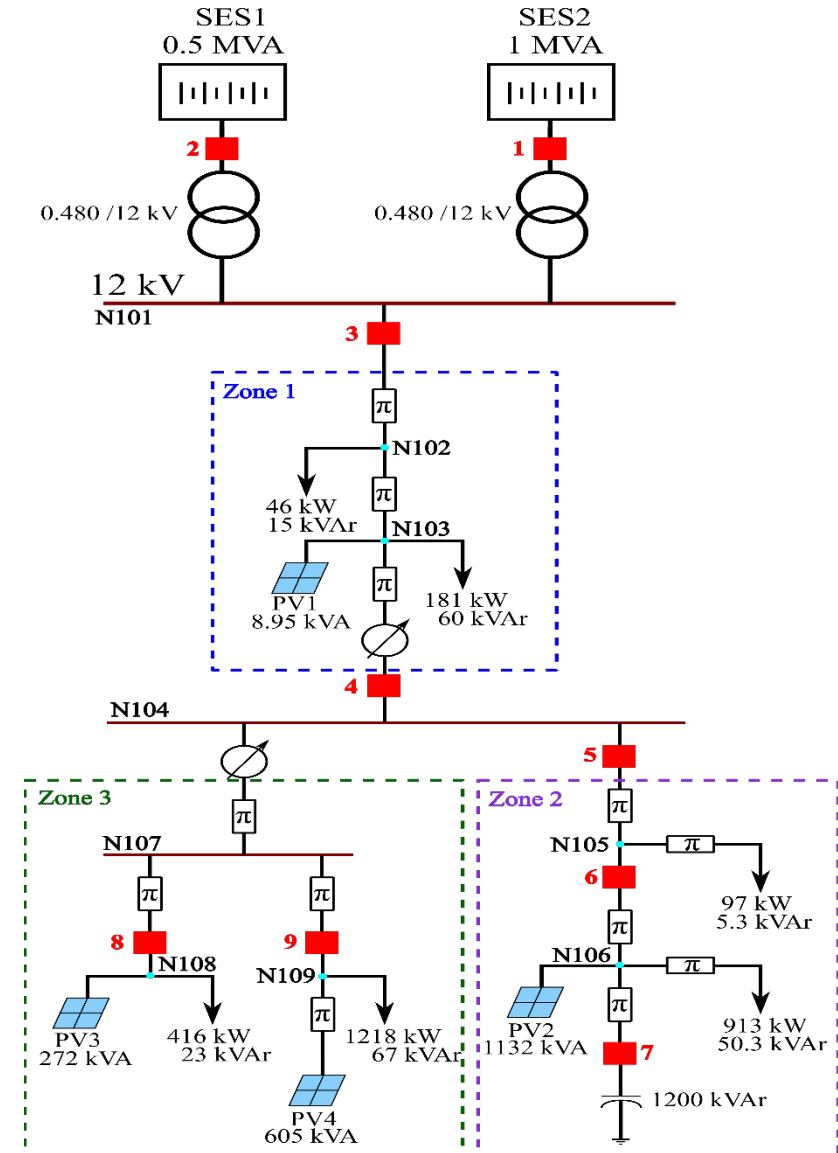
SCENARIO #3: SES1 AND SES2 (GFM VF CONTROL, DROOP MODE)



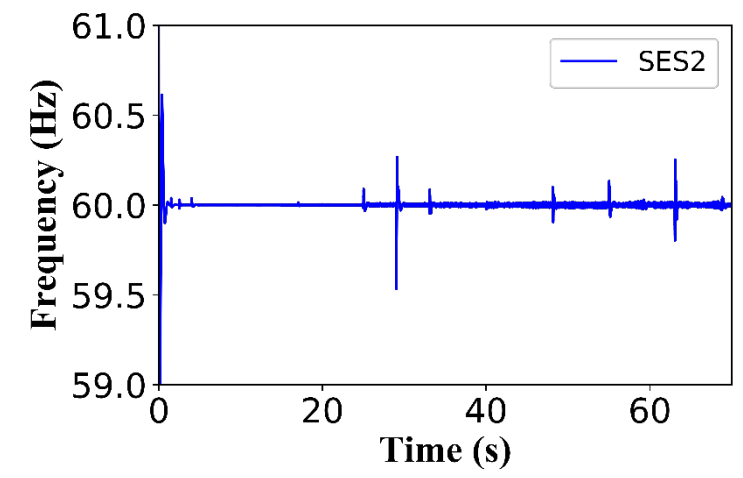
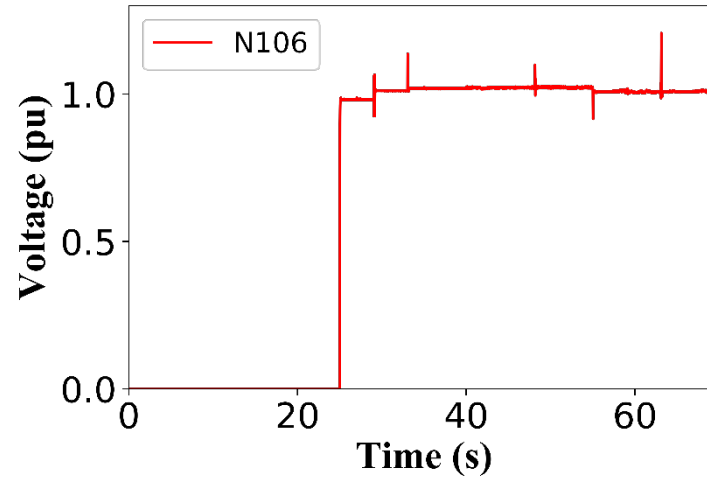
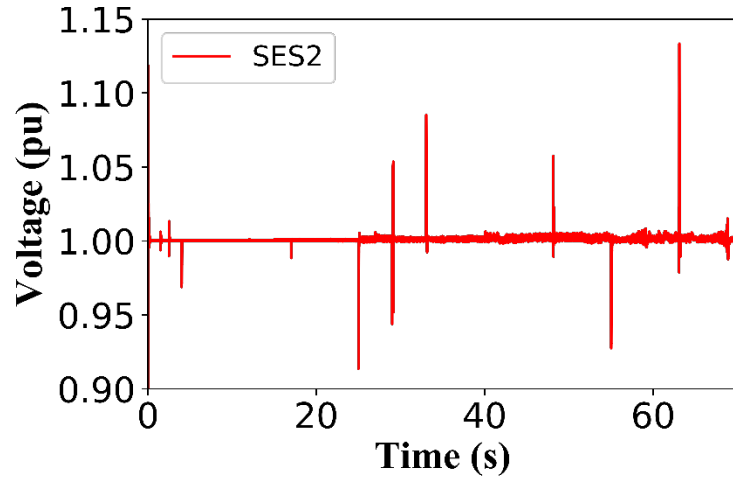
- Microgrid frequency settles above 60 Hz due to droop mode.
- Frequency and damped oscillations show similar settling time compared to scenario #2.
- More challenging scenarios like load steps and generation loss are required to determine the GFM operating mode (isochronous, droop).

BLACK START OF CKT1

- SES2 is used as GFM to black start ckt1.
- SES1 operates in GFL mode along with rooftop PV.
- Ckt1 has three zones based on utility black start sequence; zone1 has light, and balanced load; zone2 & 3 has heavy unbalanced load.
- Morning load and solar data from SDG&E are used for the ckt1 load and PV generation.
- Rooftop PV comes online 8 sec after the connected bus is energized.
- Accelerated black start is performed to reduce the total time in PSCAD simulation.

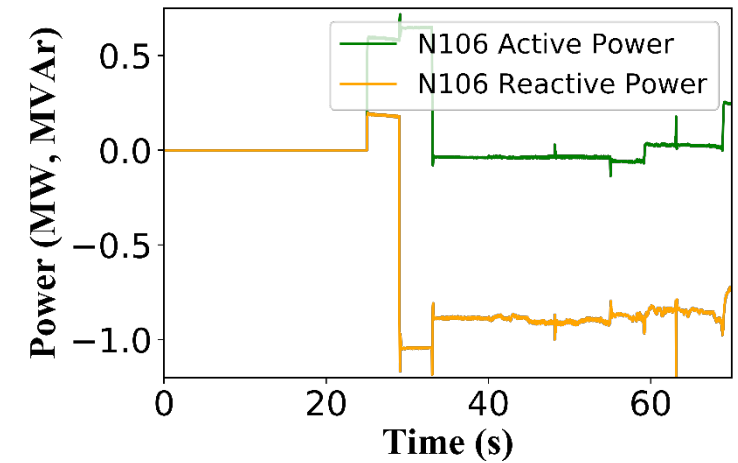
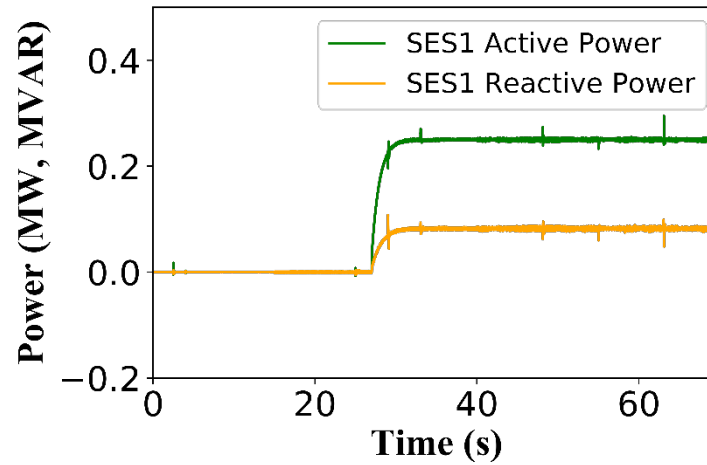
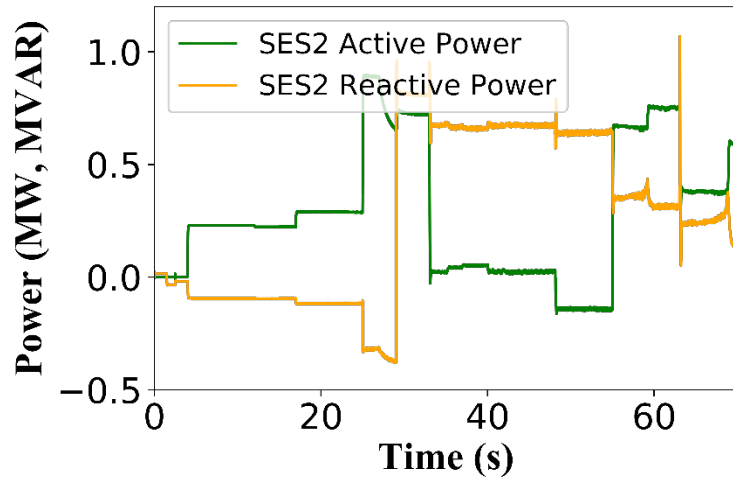


SCENARIO 4: CKT1 BLACK START



- Voltage and frequency measurements show the transients which are caused by cap bank and rooftop energization.
- Notch filter tuned to second harmonic is used to suppress noise caused by unbalanced load after 27 sec.
- Third and fourth harmonics makes the measurement noisy with each unbalanced load.

SCENARIO #4: CKT1 BLACK START



- SES2 power measurements show that BESS rating is not exceeded.
- SES1 is required to achieve the load and generation balance during zone2 & 3 load switching.

CONCLUSION

- High-fidelity PSCAD model with 86 inverters is simulated under unplanned islanding and black start scenarios.
- Unplanned islanding scenario results show the smooth transition between grid-connected and islanded mode.
- Two GFM inverters in islanded mode showed better transient response but droop mode required the PD control in outer loop.
- More test scenarios are required to determine optimal mode (Isochronous or droop).
- Ckt1 black start is successful with SES2 as GFM source.
- Positive sequence dq0 control can only control fundamental components.
- Negative-sequence control or harmonic compensation control is required to eliminate the noise in the measurements.

Thank You

Email: yaswanthnag.velaga@nrel.gov

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