

A Comparison of Generator Technologies for Offshore Wind Turbines

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The Fine Print

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Design Matrix

- Generator technologies
 - Interior permanent-magnet direct drive (IPM)
 - Low temperature superconducting (LTS)
 - Medium-speed geared configuration (gear ratio 120) with surface-mounted permanent-magnet generator (MS-PMSG)
- Ratings of 15/17/20/22/25 megawatts (MW)
- Floating and fixed bottom
- Design and optimization supported by the Wind-Plant Integrated System Design and Engineering Model (WISDEM[®]) and Wind Energy with Integrated Servo control (WEIS).

Wind Turbine Configurations

٠	Specific power International
	Energy Agency (IEA) 15 MW 325
	W/m ²

• Max blade tip speed of 95 m/s

		\mathbf{Nam}	eplate (Power	(MW)	
Parameter	\mathbf{Units}	15	17	20	22	25
Rotor Diameter	m	242.2	257.9	279.7	293.36	312.7
Blade Length	m	117.2	124.7	135.3	141.78	151.2
Hub Diameter	m	7.9	8.4	9.2	9.8	10.4
Rotor Overhang	m	12.0	13.0	14.0	15.0	16.0
Rated Rotor Speed	rpm	7.5	7.0	6.5	6.2	5.8
Rated Shaft Torque	MNm	20.1	24.3	31.0	35.8	43.3

rpm: revolutions per minute

	Generator architecture								
Parameter	\mathbf{Units}	DD-LTSG	DD-IPMSG	MS-PMSG					
Rotor-stator config		Inner rotor	Outer rotor	Inner rotor					
Gear ratio		1:1	1:1	1:120					
Target efficiency	%	97	95	96					
Rated terminal voltage	kV	3.3	3.3	3.3					

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Cost Model

- Bill of materials scaled by unit cost of materials and electricity consumption
 - Includes "buy-to-fly" multipliers
 - U.S. average cost of electricity for industry in 2022 = \$0.078 per kilowatt-hour (kWh)
- Cost and mass of cooling system scales by generator rating and diameter
 - Cooling cost multiplier = \$124 per kilogram (kg)
- Bureau of Labor Statistics manufacturing estimates final cost is 18.9% capital, 61.9% materials, 19.3% labor, so our materials estimate is scaled by 1/0.619 to obtain final cost.

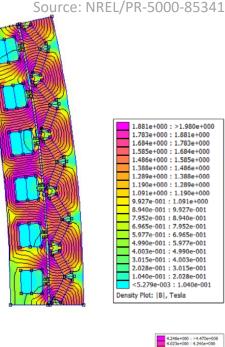
Material	\$/kg	Buy to fly	kWh/kg
Copper	7.30	1.26	96.2
Steel	1.56	1.21	15.9
Elec Steel	Elec Steel 4.44		26.9
NdFeB	66.72	1.0	79.0
NbTi	45.43	1.0	79.0

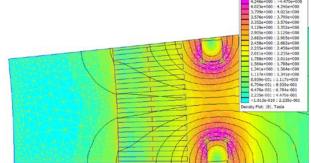
Cooling Mass

Rating (MW)	LTS (t)	IPM (t)	MS-PMSG (t)
15	1().6	1.3
17	12	2.0	1.5
20	14	1.9	1.8
22	16	5.4	2.0
25	18	3.7	2.3

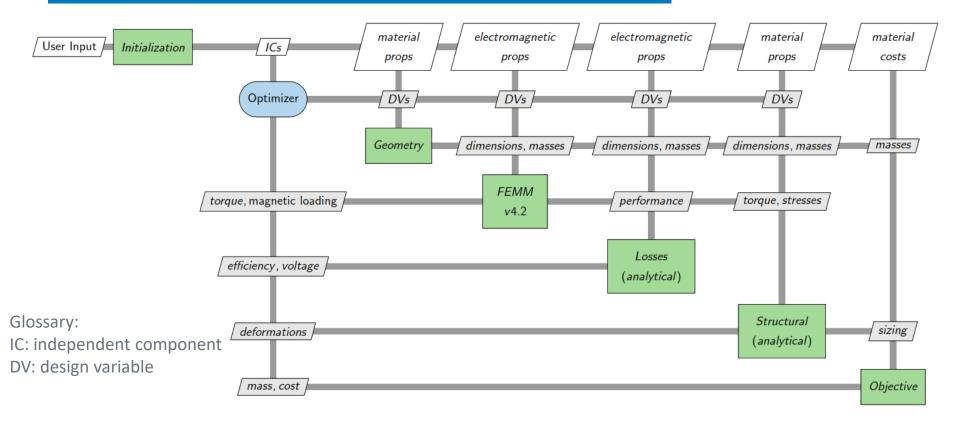
Comparison of Generator Technologies

- Design optimization used finite element method magnetics (FEMM) models of generator sections; particularly important for permanent-magnet designs
- Code is publicly available at <u>https://github.com/WISDEM/GeneratorSE/</u>
- Cost vs. mass minimizations
 - We moved ahead with the minimum-cost designs.
 - Results are very sensitive to the unit costs of the materials.





Generator Design Optimization



LTS Design

- Optimal design parameters generally avoid extremes
- Good cost and consistent efficiency across power

h _{yss} h _{ys}	
< <u>− ra</u> stator	20
$rotor \stackrel{\bullet}{\leftarrow} h_s \stackrel{\bullet}{\rightarrow} h_{sc} \stackrel{\bullet}{\rightarrow} h_{yrs}$	t hsc

			Βοι	inds
Symbol	Description	\mathbf{Units}	Lower	Upper
r_a	Stator radius	m	3	4.75
h_s	Winding height	$\mathbf{m}\mathbf{m}$	50	400
l_s	Axial length	m	0.75	1.75
h_{sc}	Field coil height	$\mathbf{m}\mathbf{m}$	30	250
N_{sc}	Field coil turns	-	1500	3500
h_{yr}	Rotor yoke thickness	$\mathbf{m}\mathbf{m}$	150	300
pp	Pole pairs	-	15	40
N_c	Stator turns per coil	-	1	7
dlpha	Wire width	deg	0.2	0.6
h_{ss}	Stator support rim thickness	$\mathbf{m}\mathbf{m}$	25	600
h_{sr}	Rotor support rim thickness	$\mathbf{m}\mathbf{m}$	25	500
t_r	Rotor disc thickness	$\mathbf{m}\mathbf{m}$	25	500
t_s	Stator disc thickness	$\mathbf{m}\mathbf{m}$	25	500

	Nameplate Power (MW)							
\mathbf{Symbol}	Description	\mathbf{Units}	15	17	20	22	25	
r_a	Stator radius	m	4.5	4.5	4.75	4.75	4.75	
h_s	Winding height	$\mathbf{m}\mathbf{m}$	148	166	180	220	263	
l_s	Axial length	m	1.0	1.0	1.0	1.0	1.0	
h_{sc}	Field coil height	$\mathbf{m}\mathbf{m}$	40	30	35	45	73	
N_{sc}	Field coil turns	-	1504	1506	1606	1806	2102	
I_{sc-op}	Field current	А	451.67	527.86	516.47	500.21	514.73	
h_{yr}	Rotor yoke thickness	$\mathbf{m}\mathbf{m}$	150	150	150	150	150	
pp	Pole pairs	-	38	37	39	39	39	
N_c	Stator turns per coil	-	1	1	1	1	1	
dlpha	Field coil width	deg	0.749	1.316	1.258	1.258	1.310	
T_{ratio}	Torque ratio	-	1.02	1.08	0.98	1.02	1.02	
Ep_{ratio}	Terminal voltage ratio	-	0.98	0.80	0.84	0.86	0.82	
η^{-}	Efficiency	-	98.4	98.4	98.5	98.4	98.4	
M_{gen}	Total mass	t	192.1	192.9	207.8	217.3	228.6	
C_{gen}	Total cost	k	4944.4	5270.5	6078.9	6631.5	7369.8	

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IPM	Design

Description

Stator radius

Tooth height

Axial length

Pole pairs

Turns per coil Tooth width

Magnet thickness

Rotor yoke thickness

Stator yoke thickness

Winding current density

Rotor disc thickness

Stator disc thickness

Stator support rim thickness

Rotor support rim thickness

Vertex to rotor inner radius

Symbol

 r_a

 h_t

 l_s

 d_{mag}

 h_m

 h_{yr}

 h_{ys}

 $pp \\ N_c$

 b_t

 J_s

 h_{ss}

 h_{sr}

 t_r

• Difficulty maintaining efficiency target at high power

Units

 \mathbf{m}

 $\mathbf{m}\mathbf{m}$

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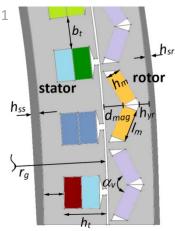
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Mass and cost increase with increasing power than LTS design

Bounds			Nameplate Power (MV							
Lower	Upper	Symbol	Description	\mathbf{Units}	15	17	20	22	25	
3	4.75	r_a	Stator radius	m	4.5	4.5	4.75	4.75	4.75	
40	4.70 350	l_s	Axial length	m	2.5	2.5	2.5	2.5	2.5	
		h_t	Tooth height	$\mathbf{m}\mathbf{m}$	107	120	137	149	214	
0.75	2.5	b_t	Tooth width	$\mathbf{m}\mathbf{m}$	34.5	32.6	32.5	28.7	33.5	
50	250	d_{mag}	Vertex to rotor inner radius	$\mathbf{m}\mathbf{m}$	50	50	50	50	50	
5	60	h_m	Magnet thickness	$\mathbf{m}\mathbf{m}$	16.3	22.0	30.8	48.3	47.3	
20	300	h_{yr}	Rotor yoke thickness	$\mathbf{m}\mathbf{m}$	30	97	94	74	81	
20	300	h_{ys}	Stator yoke thickness	$\mathbf{m}\mathbf{m}$	61.2	48.0	53.8	62.5	115.2	
50	200	pp	Pole pairs	-	60	65	60	55	55	
2	10	N_c	Turns per coil	-	4	4	4	4	4	
20	100	J_s	Winding current density	A/mm^2	6	6	6	6	6	
3	6	T_{ratio}	Torque ratio	-	1.05	1.01	1.05	1.06	1.05	
40	200	Ep_{ratio}	Terminal voltage ratio	-	0.81	0.91	0.89	0.82	0.80	
40	200	η^{-}	Efficiency	-	94.7	94.6	94.7	94.9	93.8	
50	300	M_{gen}	Total mass	t	314.0	382.9	445.9	460.6	507.5	
50	300	C_{gen}	Total cost	\mathbf{k}	6298.5	7516.0	9334.5	10708.2	11819.7	



Source: NREL/PR-5000-85341

MS-PMSG Design

- Consistent efficiency across power
- Greater mass and cost increase with increasing power than LTS design

Source: NREL/PR-5000-85341	5
hyr hs	
hrs hm	
NdEaP magnat	stator
rotor	

			Bo	unds			Nameplate Power				er (MV	N)
Symbol	Description	\mathbf{Units}	Lower	Upper	\mathbf{Symbol}	Symbol Description		15	17	20	22	
	Electric machine design variable	es			r_q	Air-gap radius	m	0.5	0.5	0.5	0.5	0
r_g	Air-gap radius	\mathbf{m}	0.5	2.0	l_s	Axial length	\mathbf{m}	0.59	0.60	0.66	0.69	0.
l_s	Axial length	\mathbf{m}	0.5	2.5	h_s	Slot height	$\mathbf{m}\mathbf{m}$	25	25	26	26	
h_s	Slot height	$\mathbf{m}\mathbf{m}$	25	100	g	Air-gap length	$\mathbf{m}\mathbf{m}$	9	9	9	9	
g	Air-gap length	$\mathbf{m}\mathbf{m}$	6	9	\tilde{h}_m	Magnet height	$\mathbf{m}\mathbf{m}$	12	14	18	28	
h_m	Magnet height	$\mathbf{m}\mathbf{m}$	5	75	pp	Pole pairs	-	10	10	10	10	
pp	Pole pairs	-	4	10	ratio	Ratio of pole width to pole pitch	-	0.83	0.83	0.85	0.85	0
ratio	Ratio of pole width to pole pitch	-	0.7	0.85	N_c	Stator turns per coil	-	2	2	2	2	
N_c	Stator turns per coil	-	2	12	I_s	Stator current	А	6000	6000	6000	6000	6
I_s	Stator current	Α	500	6000	h_{yr}	Rotor yoke thickness	mm	96	81	44	38	
h_{yr}/h_{ys}	Rotor/Stator yoke thickness	$\mathbf{m}\mathbf{m}$	10	100	h_{ys}	Stator yoke thickness	mm	26	28	35	41	
	Structural design variables				Tratio	Torque ratio	-	1.02	0.99	1.00	0.99	0
h_{sr}/h_{ss}	Rotor/Stator support rim thickness	$\mathbf{m}\mathbf{m}$	45	250		Terminal voltage ratio		1.02 1.09	1.07	$1.00 \\ 1.10$	1.10	1
n_r/n_s	Number of rotor/stator spokes	-	5	15	Ep_{ratio}	Efficiency	-	0.968	0.972	0.975	0.977	0.9
b_r/b_s	Rotor/Stator circumferential arm dimension	\mathbf{m}	0.1	1.5	-η	Enterency	-	0.908	0.972	0.975	0.911	0.3
d_r/d_s	Rotor/Stator arm depth	\mathbf{m}	0.1	1.5	M_{gen}	Total mass	\mathbf{t}	5.116	5.382	6.094	6.810	7.7
t_{wr}/t_{ws}	Rotor/Stator arm thickness	$\mathbf{m}\mathbf{m}$	1	200	C_{gen}	Total cost	\mathbf{k}	325.2	366.1	436.8	499.1	57

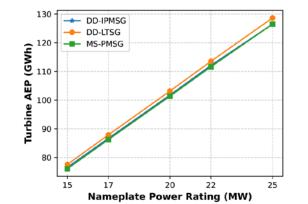
Mass and Cost Trends

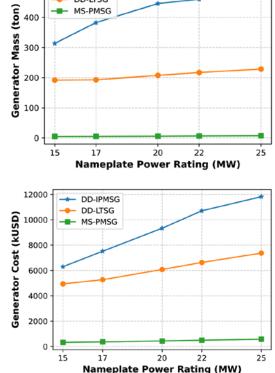
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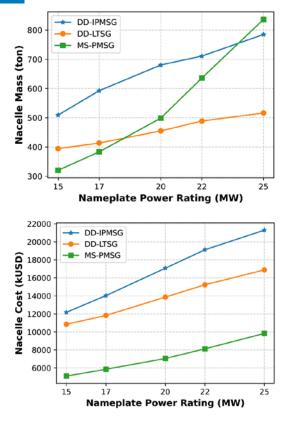
DD-IPMSG

DD-LTSG

Bounds on armature diameter limit growth of mass, not of cost, and IPMSG design at 25 MW does not meet efficiency requirement.

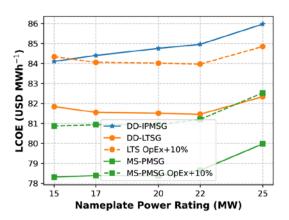


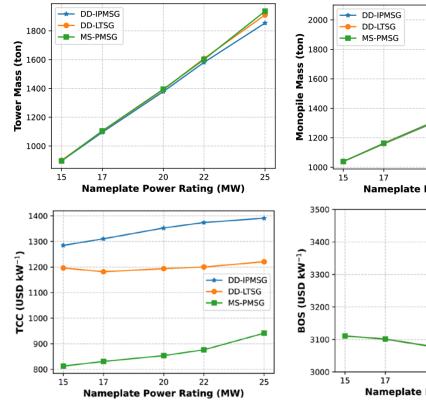


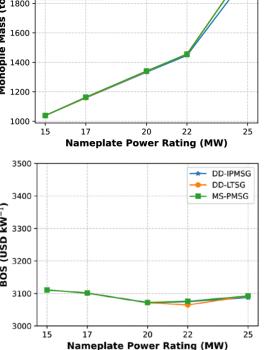


Fixed Bottom Designs

- Operational expenditure (OpEx) costs of 110 \$/kW/yr.
- LCOE results are very sensitive to this number, see LTS and MS-PMSG results for OpEx costs increased by 10%.

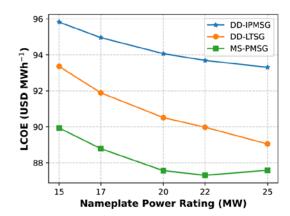


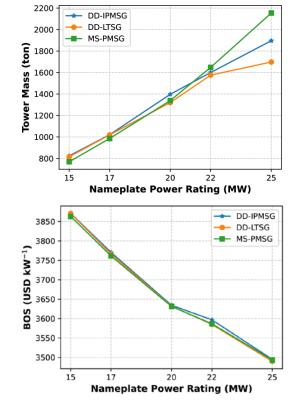


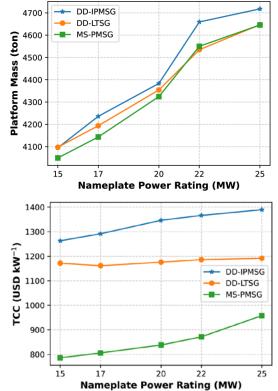


Floating Designs

- Similar platform masses and BOS costs across generator technologies.
- At 25 MW, MS-PMSG and LTS are closer.









- Three drivetrain technologies (IPM, MS-PMSG, and LTS) at five ratings (15, 17, 20, 22, and 25 MW), fixed-bottom and floating evaluated in WISDEM and WEIS
- IPM efficiency struggles at higher power; could indicate topology limitations.
- LTS efficiency suggests no limitation over power; less sensitive to cost and efficiency change with power.
- MS-PMSG shows improving efficiency with power level, but higher rate of cost increase than LTS.
- Results are sensitive to models (material properties, costs, operations and maintenance), so focus on trends rather than specific numbers.

Summary

- LTS reduces LCOE by 2%–3% compared to IPM, which struggles especially at higher ratings.
- Despite the lower drivetrain efficiency, MS-PMSG shows the lowest cost of energy. However, we did not model operations and maintenance costs, which might increase with a gearbox or new technology, and results are very sensitive to OpEx.
- LCOE decreases with increasing rating for floating. For fixed bottom, it stays flat from 15–20 MW, and increases at 25 MW.

Q&A





NREL/PR-5000-85341