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Emergency Asset Positioning for Resilient Transmission Grid Operation

Ignas Satkauskas* , Jonathan Maack* , Matthew Reynolds* , Devon Sigler* , Kinshuk Panda* , and Wes Jones* *National Renewable Energy Lab

Introduction

In this paper we study a problem of hurricane emergency preparedness via placement of emergency storage assets prior to its strike. We present a two-stage stochastic model for choosing locations and quantities of emergency storage to help support the power grid through a hurricane event. The expectation of losses in our twostage model is estimated using the sample average approximation. We construct damage scenarios for sample average approximation using WIND Toolkit meteorological data and fragility curves of various electric grid components. We demonstrate the efficacy of our twostage planning model by simulating operations during Hurricane Dolly on the 2000-bus transmission test system. Our model, coupled with our scenario selection strategy, is effective at mitigating loss of load when compared to a model without emergency storage assets placed prior to an extreme event.

Problem formulation

A two-stage stochastic program can be defined as follows:

$$
\min_{\mathbf{x}} f(\mathbf{x}) + \mathbb{E}_{\gamma} \left[L(\mathbf{x}, \gamma) \right] \quad \text{s.t.} \quad \mathbf{g}(\mathbf{x}) \leq 0 \tag{1}
$$

where

 \mathbf{r}

$$
L(\boldsymbol{x},\boldsymbol{\gamma}) = \min_{\boldsymbol{x}} l(\boldsymbol{x},\boldsymbol{y},\boldsymbol{\gamma}) \quad \text{s.t.} \quad \boldsymbol{g}_{\boldsymbol{\gamma}}(\boldsymbol{x},\boldsymbol{y}) \leq 0. \tag{2}
$$

First stage of our model is given by:

$$
\min_{S} \sum_{i \in \phi} C_{i} S_{i} + \mathbb{E}_{\gamma} \left[L \left(S, \gamma \right) \right] \tag{3}
$$
\n
$$
\text{s. t. } S_{i}^{\min} < S_{i} < S_{i}^{\max} \quad \forall \, i \in \phi, \tag{4}
$$

Second stage of our model is given by:

 \overline{I}

$$
\begin{array}{llll} \displaystyle \sum_{(s,\boldsymbol{\gamma}) = \min\limits_{g \in G, t \in T} c_g x_g^t + \sum\limits_{w \in W, t \in T} c_w \omega_w^t & \\ & + \sum\limits_{i \in \phi, t \in T} \left(c_i^+ y_i^{t,+} + c_i^- y_i^{t,-} \right) & \end{array}
$$

 (5)

such that

$$
x_{g}^{min} \leq x_{g}^{t} \leq x_{g}^{max} \quad \forall g \in G, t \in T
$$
\n(6)
\n
$$
R_{g}^{down} \leq x_{g}^{t} - x_{g}^{t-1} \leq R_{g}^{up} \quad \forall g \in G, t \in T
$$
\n(7)
\n
$$
0 \leq s_{i}^{t} \leq S_{i} \quad \forall i \in \phi, t \in T
$$
\n(8)
\n
$$
s_{i}^{t} = s_{i}^{t-1} - \frac{\Delta p_{i}^{t}}{\eta_{i}} \quad \forall i \in \phi, t \in T
$$
\n(9)
\n
$$
0 \leq p_{i}^{t} \leq p_{i}^{max} \quad \forall i \in \phi, t \in T
$$
\n(10)
\n
$$
0 \leq y_{i}^{t+1} \quad \forall i \in \phi, t \in T
$$
\n(11)
\n
$$
0 \leq \omega_{w}^{t} \leq \gamma_{w}^{t} \omega_{w}^{t}.f^{cst} \quad \forall w \in W, t \in T
$$
\n(12)
\n
$$
p_{i}^{t} + \sum_{w \in W_{i}} \omega_{w}^{t} + \sum_{g \in G_{i}} x_{g}^{t}
$$
\n(13)
\n
$$
+ \sum_{e \in \mathcal{E}_{in}(i)} f_{e}^{t} - \sum_{e \in \mathcal{E}_{out}(i)} f_{e}^{t}
$$
\n
$$
= \gamma_{i}^{t} d_{i}^{t} + y_{i}^{t+1} - y_{i}^{t-1} \quad \forall i \in \phi, t \in T
$$
\n
$$
\gamma_{e}^{t} \leq F_{e} \leq f_{e}^{t} \leq \gamma_{e}^{t} \overline{F}_{e} \quad \forall e \in \mathcal{E}
$$
\n(14)
\n
$$
\gamma_{e}^{t} (B_{e} (\theta_{i}^{t} - \theta_{j}^{t}) - f_{e}^{t}) = 0 \quad \forall e \in \mathcal{E}, t \in T.
$$
\n(15)

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Scenario: Hurricane Dolly

Our working example includes the path of the Hurricane Dolly (Fig 1-2) over a week in July of 2008 and synthetic ACTIVSg 2000-bus grid [1]. Using NREL's WIND Toolkit data [2] and fragility curve methodology [3,4] we generate damage scenarios to transmission lines (Fig 3), substations (Fig 4), and wind plants (Fig 5). Most of the damages occur within the first 8 hours of hurricane landing.

Figure 2: Landing and overland period: July 23, 00:00 – July 25, 00:00 Most damage occurs during 8-hour period: July 23, 18:00 – July 24, 02:00

Figure 1: Path of the Hurricane Dolly (July 20 -27) and synthetic
ACTIVSg 2000 bus transmission grid. Size of the blue circles
corresponds to hurricane's radii and their color intensity correspond to maximum wind speed.

Figure 3: Realization when max number of ches were damaged. Damaged lines (red lines) and damaged poles (black dots)

Figure 4: A realization when max number of substations (6) were number c
damaged

Asset placement and operation

Table 1: Summary of elements damaged and load lost in the sin for each scenario. Branch column gives the total number of branches damaged, while substation and islanded bus columns show bus numbers (names) given in the network description.

caused by the hurricane. Future work includes extending formulation to include other emergency assets, using larger uncertainty sets, and applying our method to other

emergencies (e.g., flood or polar vortex).

References

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2. WIND (Wind Integration Nower Systems, vol. 32, no. 4, pp. 3258–3265, 20
- **Penetrations of Wind Polynomy Orleans, LA. USA,**

Using two different uncertainty sets results
in different batterv in different battery
placement decisions placement

ne (black dots).

Damage scenarios 6-10
result in battery hattery placement shown in Fig 5, while scenarios 1-5 result in placement decisions shown in Fig 6.

 $12.\overline{00} \qquad 15.00 \qquad 18.00 \qquad 21.00 \qquad 00.00 \qquad 03.00 \qquad 06.00 \qquad 09.00 \qquad 12.00$ **Figure 7:** Loss of load without batteries in each of the 10 scenarios **Figure 8:** State of charge of large case emergency batteries in operation simulation under each of 10 scenarios.

> In our experiments, we chose a planning horizon of 4 hours broken into 8 half-hour steps. This horizon is chosen to cover the time window of maximum damage caused by Dolly's landfall. Ten scenarios represent the uncertainty for the planning problem (Table 1). Loss of load without batteries is shown in Fig 7 and battery discharge is shown in Fig 8. Simulated transmission grid operations with planned storage show reduced amounts of load lost due to infrastructure damage