

# Photovoltaic Cable Connectors: A Comparative Assessment of the Present State of the Industry

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\*Updated from UL-NIST 2023, PVRW 2024 workshops

DuraMAT webinar  
Monday, 2024/5/13, 1:00-200 MT  
<https://www.duramat.org/news-and-events/webinars>

# Today's Presentation

**Background** (motivation, PVQAT survey on industry)

**Experimental details** (samples, failure analysis protocol, methods examples)

**Results:**

Field degraded connectors: *primary*, metallic & polymeric components)

Accelerated aged connectors: *secondary*, metallic & polymeric components)

**Wrapping up** (solutions, summary, acknowledgements)

*Questions and comments welcome, e.g., end of each section.*

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# Motivation

- BoS components include: **cable connectors**, cables, branch connectors, fuses (discrete & blocks), RSD's.
- Quantifiable ( $\leq x \% \cdot y^{-1}$ ) replacement rate for  $t < 30y$ ! *50y use TBD*.  
-2 DOE projects presently examining: components, occurrence, cost.  
(CPS/N: 38524 @ NREL; 38531 @SNL). References: see PVRW 2024.
- Consequences of degradation and failure include:  
offline-modules, -strings, -inverters;  
system shutdown; arc fault; and fire!!!
- Concerns: *availability, safety, and technology adoption*.



Example of PV fires in Italy.  
Fiorentini et. al., PVRW 2020.  
<https://www.nrel.gov/docs/fy21osti/80055.pdf>





# Fielded Connectors: Common Degradation Modes and Scorched Metal Pins

Q: “What degradation modes dominate PV cable connectors in today’s industry?”

A: PVQAT (*survey & specific meetings*): **incompatible makes, improper assembly, uncapped ends**, ... also ... incomplete connection, improper sizing, and improper mechanical fastening.

- Featured today: **incomplete connection**, **incompatible makes**, **scorched plug & socket**.
  - **Scorched metal pins**: majority of field samples, unexpected, remains to be reconciled.

Field degraded & failed cable connectors:

- Nondestructive failure analysis.
- Destructive failure analysis.
  - Metallic  and polymeric  components.

# PVQAT Survey: Dominant Degradation/Failure Modes

- **Connector incompatibility**: plug and socket are cross-mated between different manufacturers and/or models. Present preventative NEC, IEC standards initiatives.
- **Improper assembly**: not built correctly. Often field assembly @ home run, including: stripping jacket, crimp tool, fitting of parts, torquing to specification.
- **Uncapped ends**: ends left open to the environment. Separate mechanical and electrical installation steps common. Contamination and corrosion suspected.
- **Incomplete connection**: connector not properly engaged, but visible seem fitted.
- **Improper sizing of connector to cable**: compromised seal against H<sub>2</sub>O.
- **Improper mechanical fastening to system**: (1) connectors cantilevered from the cable. May void the manufacturer's warranty. (2) cable ties crush the connector.
- **Live disconnection**: active connector separated, then reconnected for continued use.

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# The Degraded Connector Specimens Used in Forensics Examination

## Highlights:

- Samples obtained from new and prior collaborators, including PVQAT TG10.

-Detailed forensics: >50/118 samples.

- Mostly two manufacturers (a & b).

-Market share (quantity).

-Design (straight spring)?

- Mostly *warm* climates.

-Donated specimens, not targeted locations.

-Desert and monsoon/savanna climates missing.

- Compare to accelerated tests.

LOCATION	QUANTITY SUPPLIED	CLIMATE: class (description)	MANUFACTURER(S)
Baltimore, MD	8	Cfa (subtropical)	a
Dallas, TX	22	Cfa (subtropical)	b
Dallas, TX	2	Cfa (subtropical)	b
Davis, CA	6	Csa (Mediterranean)	c
Fredericksburg, VA	2	Cfa (subtropical)	c
Golden, CO	5	BSk (steppe)	b, d, e
Los Angeles, CA	5	Csb (Mediterranean)	a
Prince Edward Island (PEI), CAN	21	Dfb (continental)	b, d
Sacramento, CA	35	Csa (Mediterranean)	a
<i>accelerated tests</i>	6	<i>IEC 61215</i>	b
	6	<i>C-AST</i>	b, e
<b>TOTAL</b>	<b>118</b>	<b>5 + 4</b>	<b>5</b>



# Forensic Examination in This Study

- A protocol for nondestructive then destructive failure analyses was developed from this project.

Nondestructive: keep plug/socket connected, as-received.

Destructive: iterative.

Highlights:

- ⇒ Custom R-I sweep all connectors, including short leads.
- XCT allows metal pins and crimp to be examined without cutting the specimen.
- Traditional epoxy potting and polishing is useful.
- Unconventional*- methods applied here (milling plastic, extracting convolute spring for greater area of examination, and hot melt wax for ease of specimen handling).

Field selection:  
tripped inverter/thermography/visual inspection



Nondestructive failure analysis:  
Optical photography  
R-I sweep (*low through high current*)  
Wet HiPot  
XCT  
-*metal pins*  
-*crimps (pin to cable)*

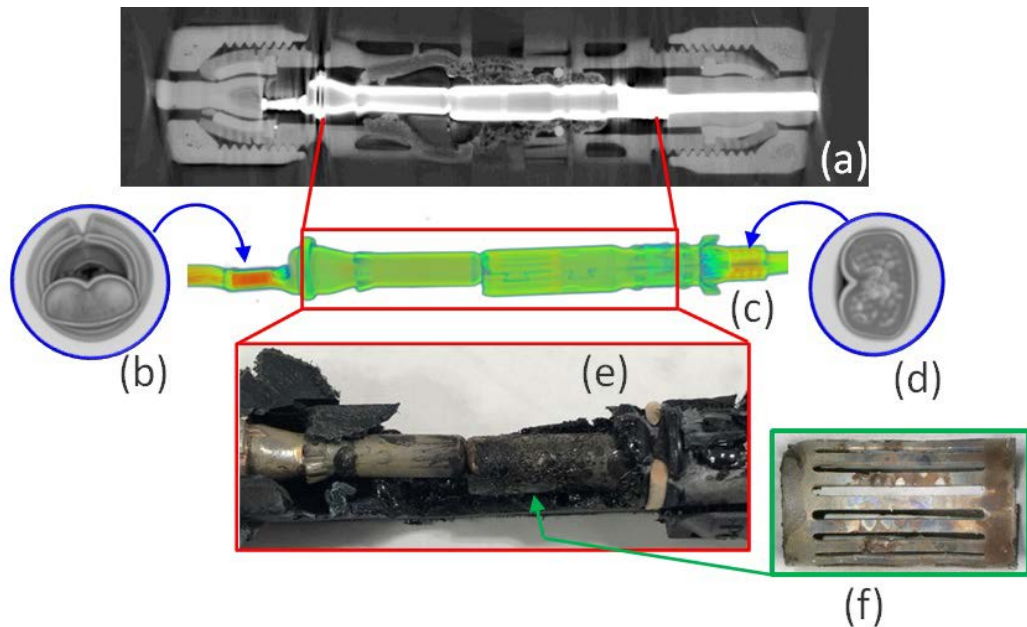


Destructive failure analysis:

1. Remove exterior plastic  
Optical photography  
FTIR, TGA, DSC
2. Extract convolute spring  
Optical microscopy
3. Cross-section and polish metals  
SEM morphology  
EDS composition

# An Early Specimen Motivated R-I Characterization

- Outward blister (mm's) on plastic socket.
- Externally: plug and socket fit together without physical separation.
- R of 90 m $\Omega$  in 2-wire measurement.
- Crimped metal folded over, no extruding wire strands, no extra space inside crimp.

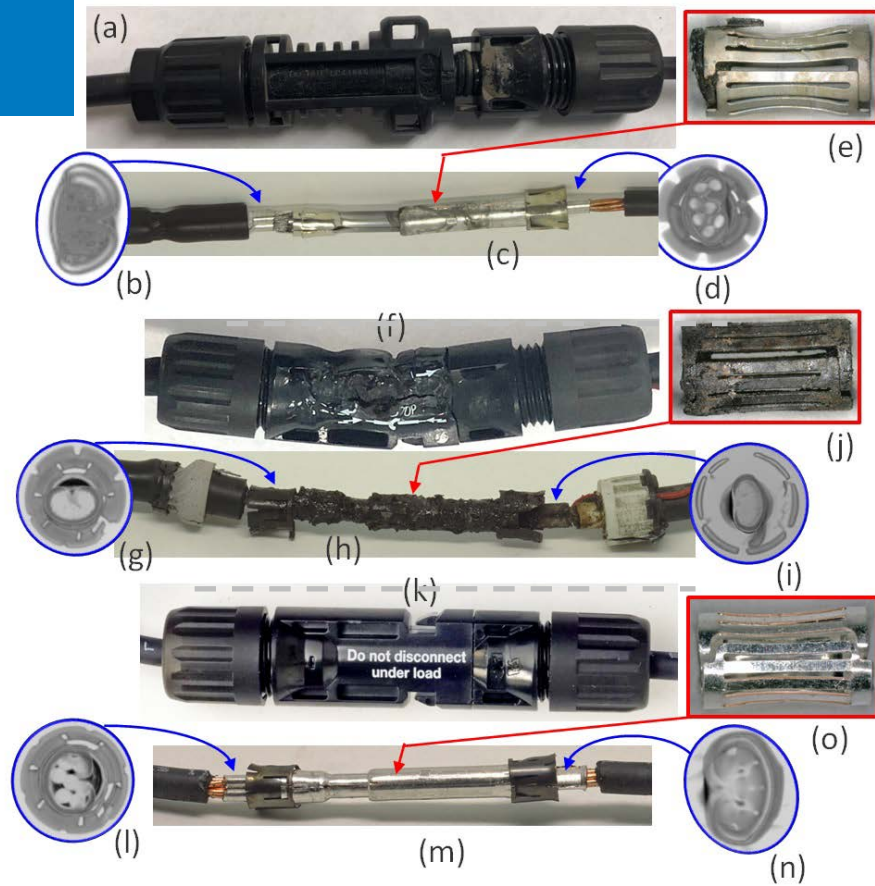


*A field-degraded connector: (e) photograph of deconstructed pin and socket as well as XCT cross-sections of: (a) the entire connector; (c) the detail of the metal pin and socket; (b) and (d) crimp site on the metal pins; and (f) the convolute spring.*

- "Incomplete connection".
- Field assembly suspected – metal pin(s) not seated correctly/inactive alignment features.
- Primary damage occurred between metal pins rather than in the crimps.
- Early basis for R-I sweep (10's of A as in PV system, rather than 1 mA test current).

# Features Observed in Field Degraded Connectors

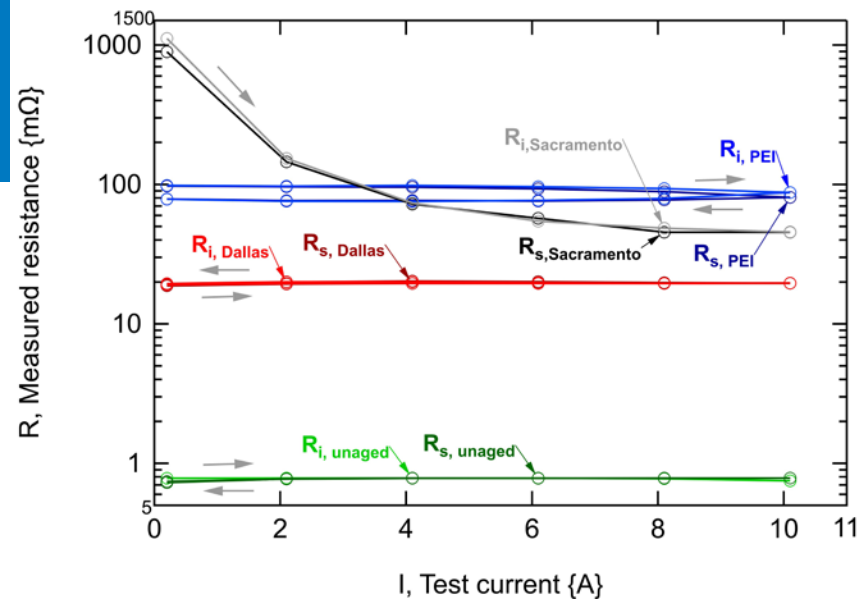
- (a)-(e): incompatible end, compromised electrical connection.
- (f)-(j): cracks and vias extend into plastic body. Failure identified visually; not identifiable from module I-V and power history!
- (a) and (f): loose end nut on the right.
- (k) and (n): unaged (reference).
- Other specimens: vaporized end (plug or socket), large blister(s), locking pins no longer fully seated, change in plastic surface gloss.



*Photos of connectors, including external appearance and springs after deconstruction.*

# R-I Sweep May Be Used to Diagnose Degraded Connectors

- $R_{\text{unaged}}$ : 0.73 m $\Omega$  at 0.2 A, 0.78 m $\Omega$  at 10 A.
- Elevated R (10's of m $\Omega$ ) observed for field degraded samples.
- PEI: hysteresis from high to low R.
- PEI, Dallas, other specimens: measurable difference between initial and stabilized (1 min) R.



*Resistance-current sweeps for field and unaged specimens of the same model. The results are shown for initial and stabilized readings at each measured current.*

- $2 \leq \Delta R \leq 4$  m $\Omega$  criteria for accelerated aging in standards.
- 6%  $\Delta R$  consistent with 4 $^{\circ}$ C temperature rise for bulk Cu.
- R anticipated to increase with current, e.g., from Joule heating.
- $\downarrow R$  for PEI ... from thermal depletion of surface oxide or improved of contact (CTE misfit)?
- Examples show usefulness of 4-wire R-I sweeps as damage quantification & diagnostic tool.

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Field degraded connectors: *primary*, metallic & polymeric components)

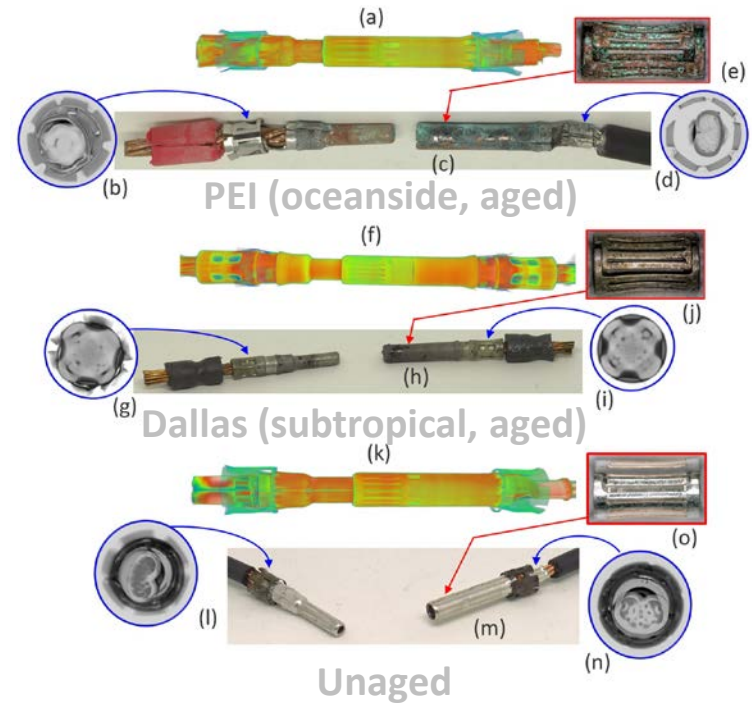
Accelerated aged connectors: *secondary*, metallic & polymeric components)

**Wrapping up** (solutions, summary, acknowledgements)

*Questions and comments welcome, e.g., end of each section.*

# Failure Analysis of Fielded Cable Connectors

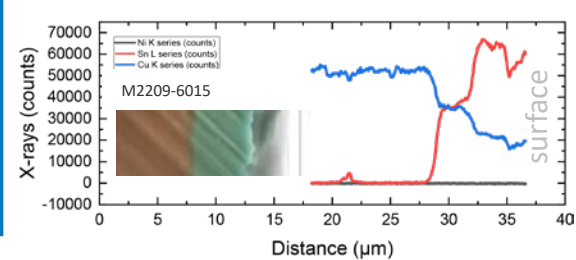
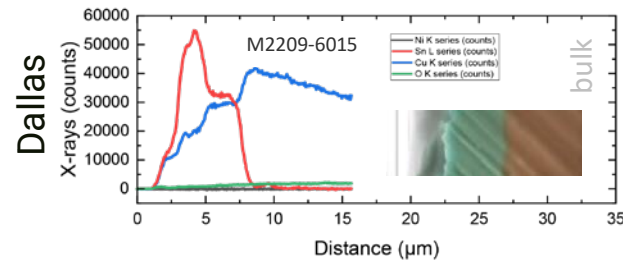
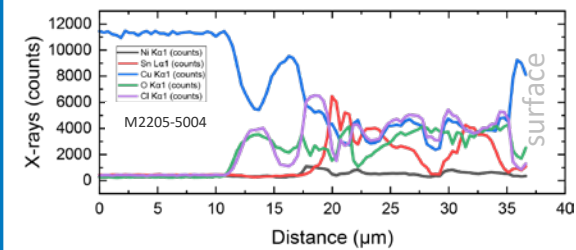
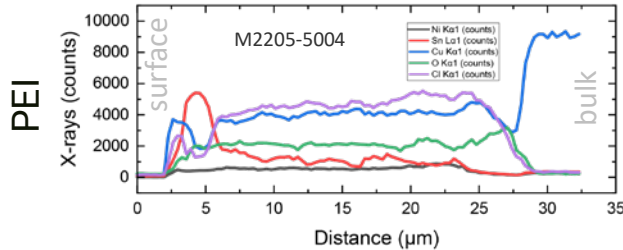
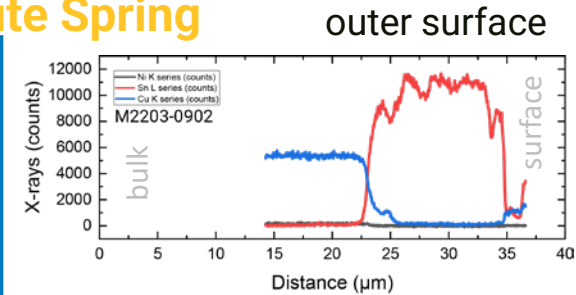
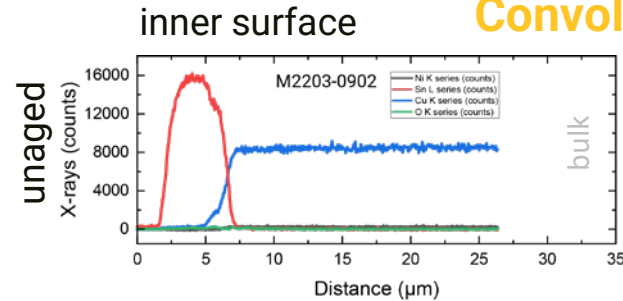
- Study of three connectors through destructive failure analysis.
- ~1y field use (where applicable).
- Metallic and polymeric components examined separately.
- Journal manuscript on F/A protocol and field degraded connectors in review.
- PEI: Incompatible connectors.  
Hermeticity compromised; corroded metal pins.
- Dallas: Scorched metal pins (common).
- We suspect improper field assembly (crimp, sizing, uncapped) is out there, but seldom identified in our specimens.





# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

## Convolute Spring



- Unaged reference (M2203-0902)

- 10 µm outer coating layer of Sn
- 5 µm inner coating layer of Sn
- little mixing between layers
- Z of Be too low for EDS detection

- PEI, oceanside, aged (M2205-5004)

- thick (25 µm) scale layer, inside & out
- mixed Ni/Sn/Cu as well as heavy O and Cl traces
- Ni may be transferred at elevated T

- Dallas, subtropical, aged (M2209-6015)

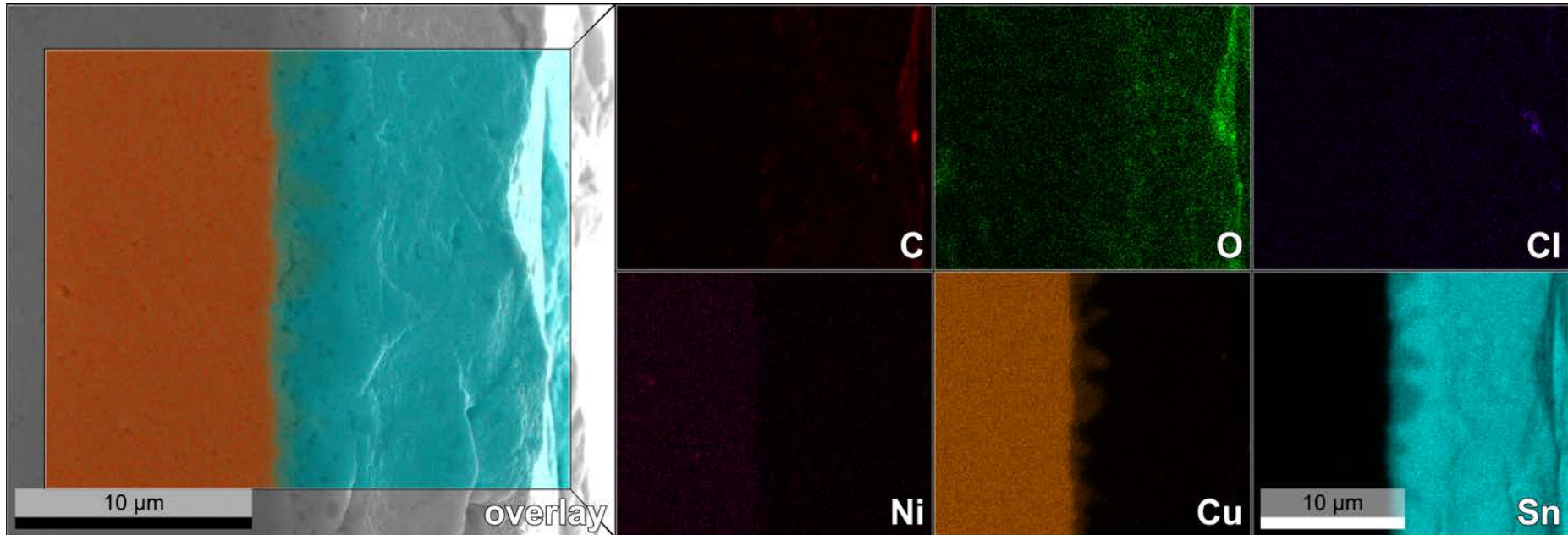
- ca. 7 µm Sn on surface, concentration gradient
- equimolar Cu mixed-phase 3-4 µm at -Sn/Cu interface, inside & out
- -23.6±0.1 % at. Sn intermetallic ε phase gradient mixed-phase: Sn/Cu ratio decreases after 3-4 µm plateau toward surface



# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

## Convolute Spring

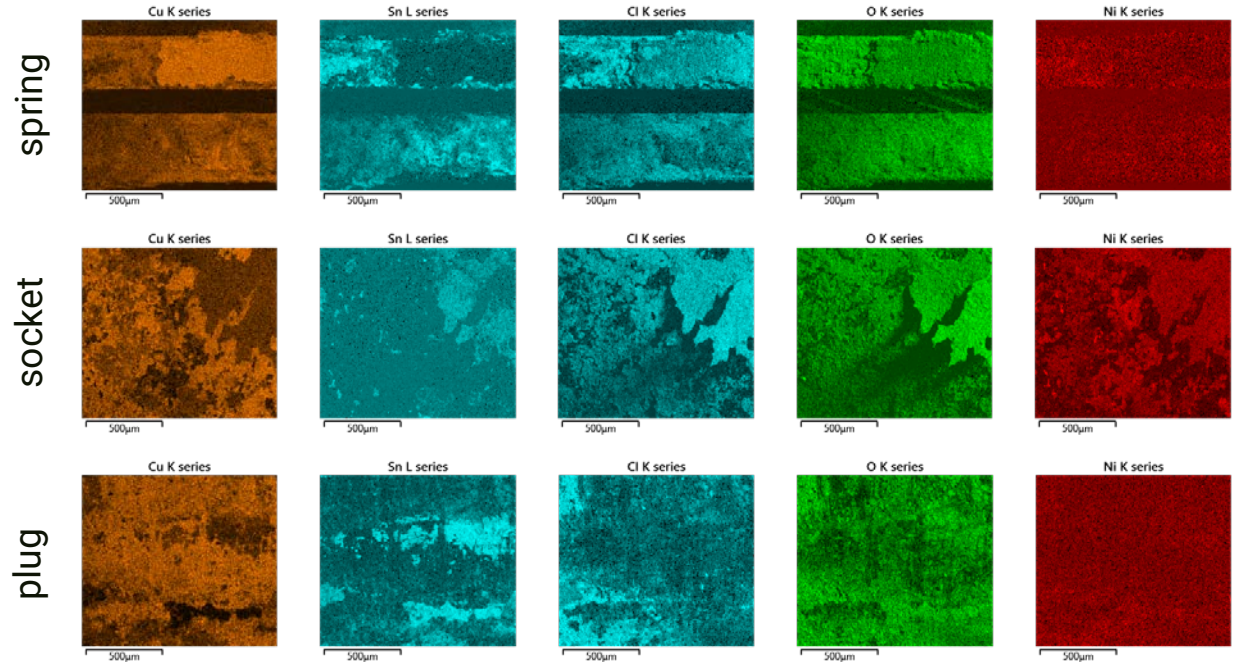
Unaged reference (M2203-0902)



# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

## Elemental mapping confirms scale compositions

- PEI, oceanside, aged (M2205-5004)
  - Cl signal colocalized with both Cu and Sn regions
  - O signal everywhere Cl is present
  - Ni also detectable from surface



# Cable Connectors: Key Characteristics of Polymeric Components

- Components examined: sealing o-ring & bushing; structure end nut & body.
- Goal: seal against H<sub>2</sub>O, prevent corrosion of metals.

## Typical in-use concerns:

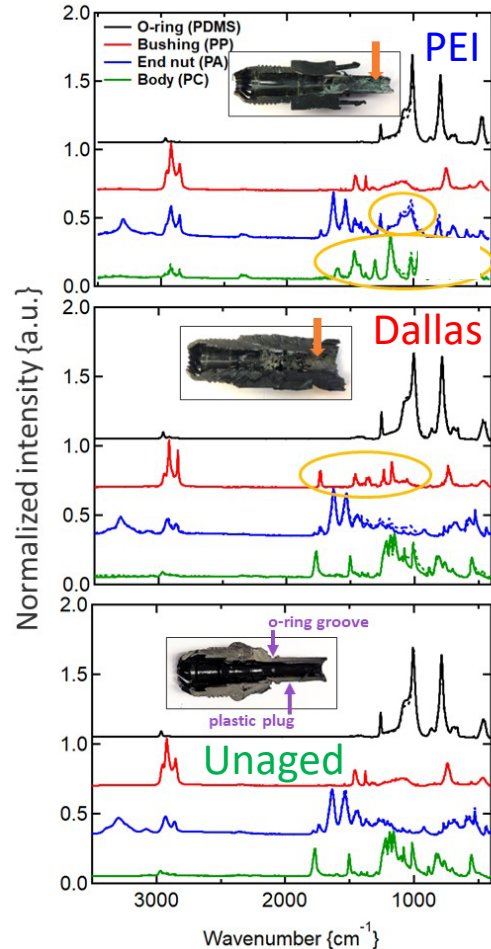
- Dimensional stability... material, type, glass & melt transitions. *\*primarily PA6/6.*

## Adverse operation concerns:

- Thermal decomposition. Here @ 2% mass loss, >T<sub>application</sub>\*

POLYMER MATERIAL	POLYMER STRUCTURE	POLYMER TYPE	O-RING	BUSHING	END NUT	BODY	T <sub>g</sub> , GLASS TRANSITION {°C}	T <sub>m</sub> , MELT TEMPERATURE {°C}	T <sub>d</sub> , DECOMPOSITION TEMPERATURE {°C}
silicone (PDMS)	semicrystalline	thermoset, elastomer	a, b, e	a, b, e	N/A	N/A	<-90	-45	400
polypropylene (PP)	semicrystalline	thermoplastic	N/A	b	N/A	N/A	-5	155	260
polyamide (PA)*	semicrystalline	thermoplastic	N/A	N/A	a, b	b	60	260	380
polycarbonate (PC)	amorphous	thermoplastic	N/A	N/A	N/A	a, b	145	N/A	450
polyphenylene ether and polystyrene	amorphous	thermoplastic copolymer	N/A	N/A	e	e	140/90	N/A	360

# The Damaged Components and Connector Failure Modes From Polymer Forensics



- **PEI:** PC body degraded, blue-green deposit from metal pin.
- **Dallas:** PP bushing degraded (lowest  $T_d$  polymer), gray discoloration, deformation of PC body from over-heating,  $T_d$  450 °C.
- Both: silicone O-ring not affected by field use.
- Damage to polymeric components is secondary, occurring from overheating after metal pins compromised near their connection.

*FTIR spectra for the polymeric components from the connectors: PEI, Dallas, and unaged. Notable differences in the spectra signature is identified with a circle. The cut connector body is shown in the insets.*

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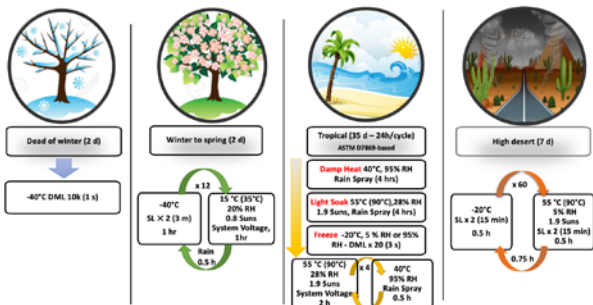
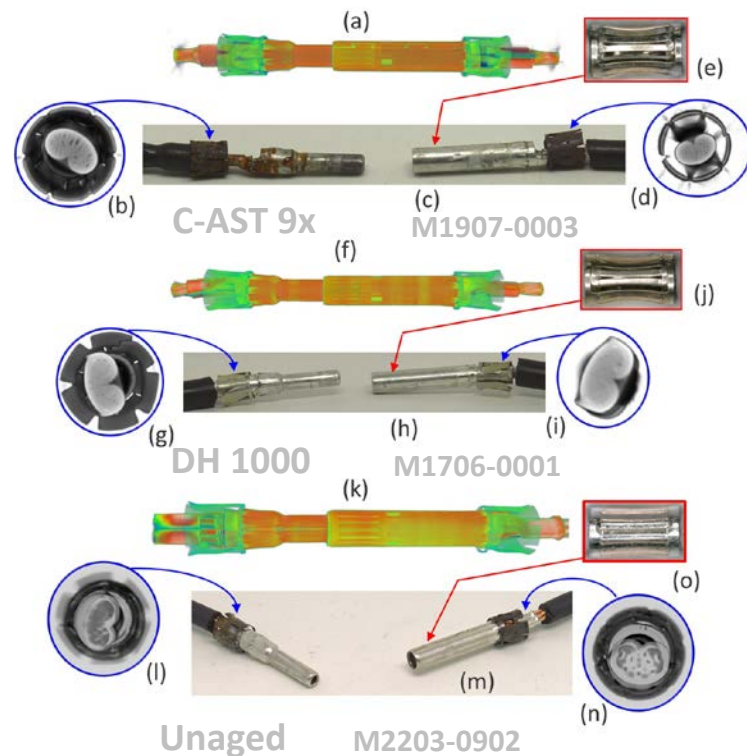
**Wrapping up** (solutions, summary, acknowledgements)

*Questions and comments welcome, e.g., end of each section.*

# Failure Analysis of Cable Connectors After Accelerated Aging

## Tests:

- **C-AST** (below)
- **Damp Heat** (85°C/85%RH, steady state @  $V_{oc}$ ).



Summary of the C-AST sequences  
(+1000 V, at MiMo current)

# Failure Analysis of Cable Connectors After Accelerated Aging: Case Study of Metallic Components

## Unaged (M2203-0902)

- Reference sample

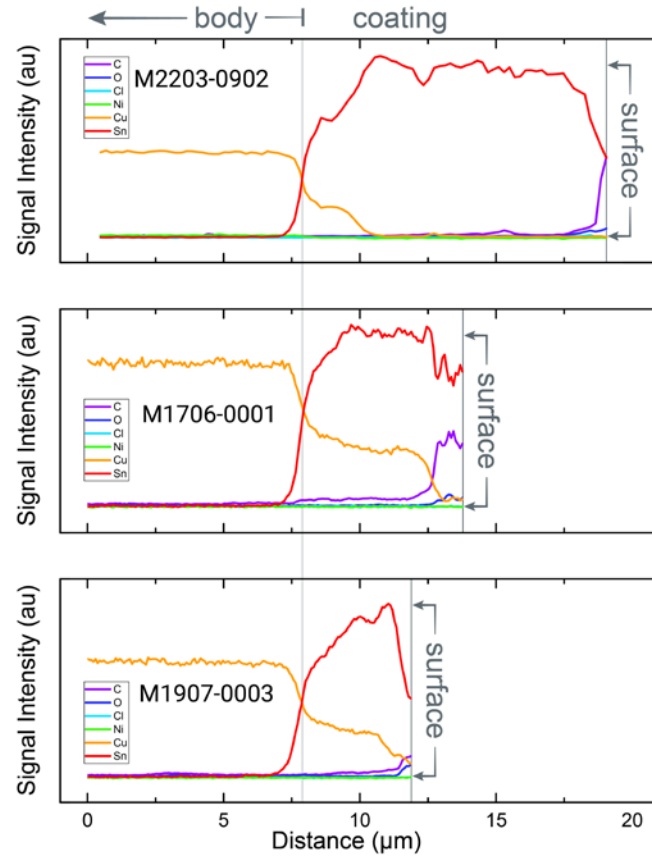
## DH 1000 (M1706-0001)

- Diffusion of Cu bulk into Sn surface layer.
- 12  $\mu\text{m}$   $\rightarrow$  8  $\mu\text{m}$  thick Sn surface layer.

## C-AST 9x (M1907-0003)

- Diffusion of Cu bulk into Sn surface layer
- 12  $\mu\text{m}$   $\rightarrow$  6  $\mu\text{m}$  thick Sn surface layer.

## Convolute Spring

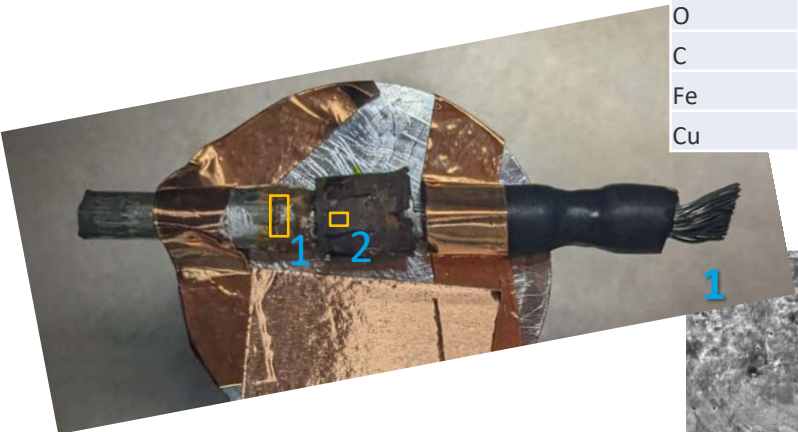




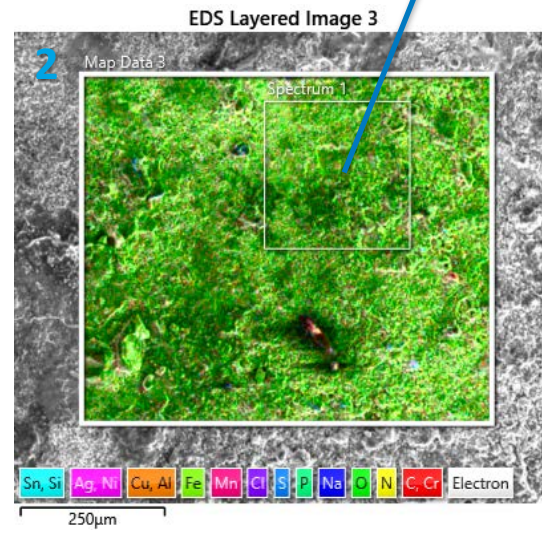
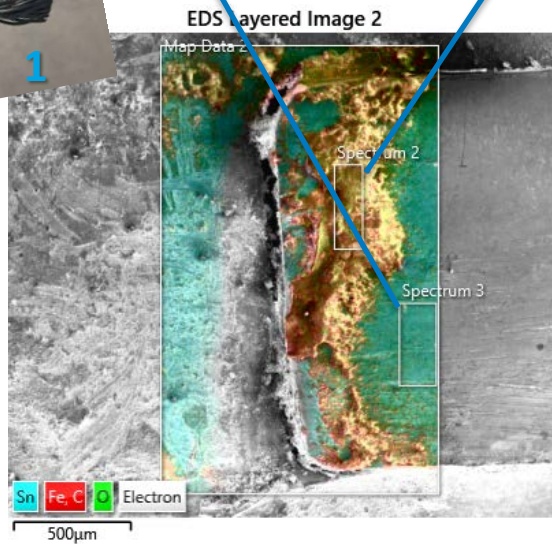
# Failure Analysis of Cable Connectors After Accelerated Aging: Case Study of Metallic Components

- C-AST 9x (M1907-0003):  
What Is Corroding?

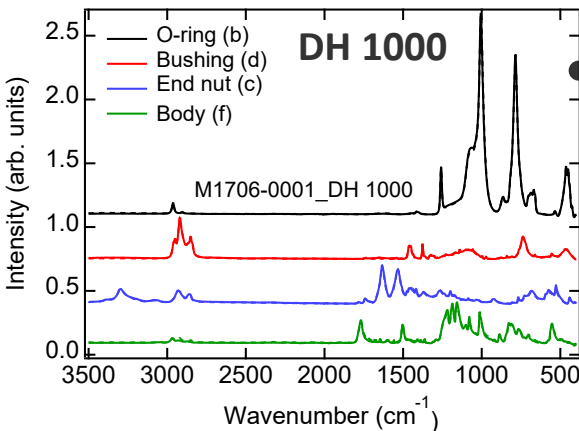
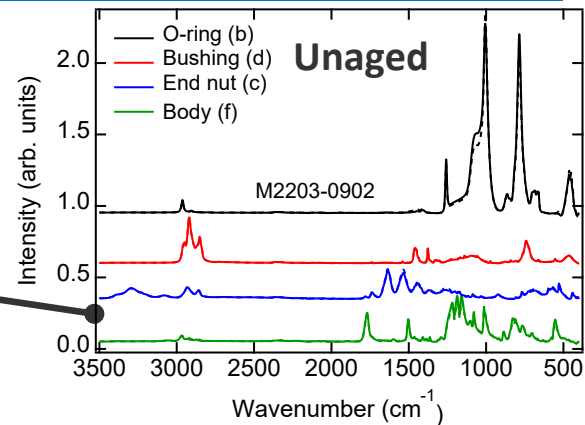
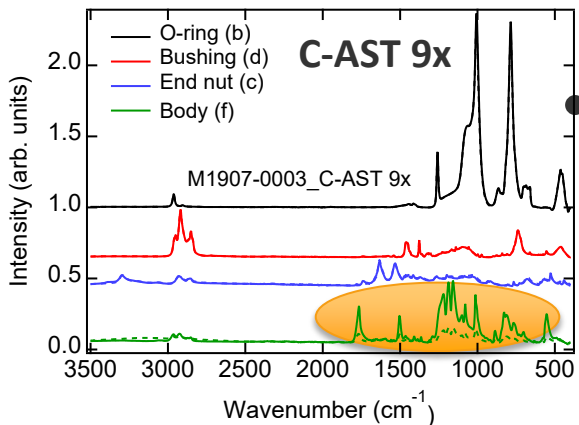
Element	Weight %	$\sigma$	Element	Weight %	$\sigma$	Element	Weight %	$\sigma$
Sn	62.47	0.24	Fe	45.71	0.23	Fe	62.87	0.12
O	25.94	0.23	O	35.65	0.22	O	27.48	0.08
C	5.52	0.12	C	17.82	0.28	C	8.65	0.14
Fe	4.62	0.08				Mn	0.37	0.02
Cu	0.93	0.08				Si	0.23	0.01
						Cl	0.14	0.01



- Fe is from retainer spring near connector end nut/cable.



# Failure Analysis of Cable Connectors After Accelerated Aging: Case Study of Polymeric Components



## C-AST 9x:

- Degradation of the connector PC body, suspect from heating following metal pin corrosion. Initial mechanical/hermeticity failure (not bulk degradation polymer) suspected.

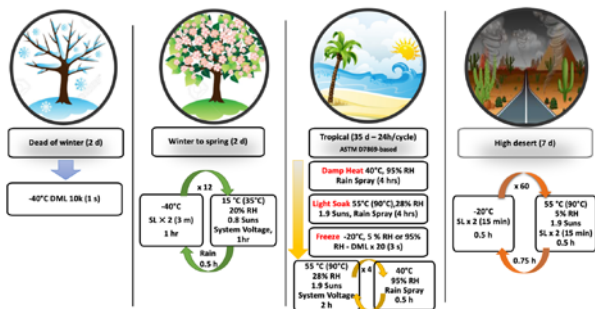
## All:

- Silicone O-ring and PP bushing not chemically affected.

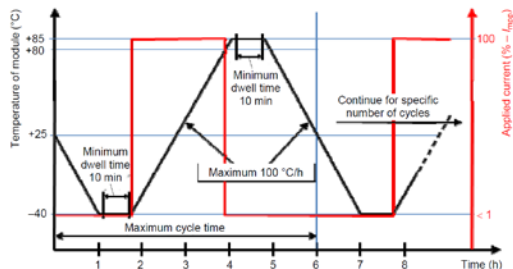
# Failure Analysis of Cable Connectors After Accelerated Aging

## Tests:

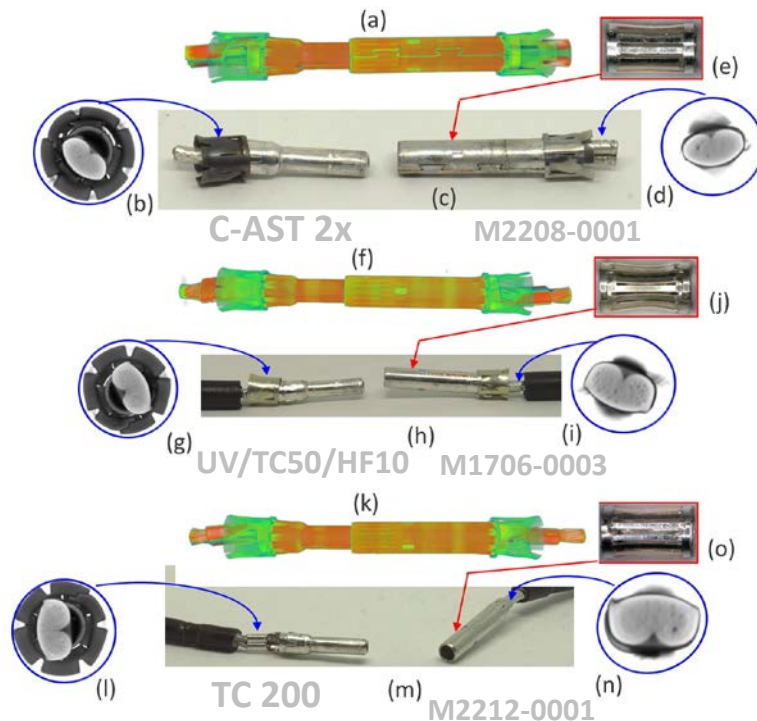
- **C-AST** (below)
- **Thermal Cycle** (below),
- **UV conditioning/Thermal Cycle (below)/Humidity Freeze** (starting from 85°C/85%RH).



Summary of the C-AST sequences



The Humidity Freeze test is similar (with 85 °C/85% RH) to the Thermal Cycle test (from IEC 61215-2)



# Failure Analysis of Cable Connectors After Accelerated Aging: Case Study of Metallic Components

## TC200 (M2212-0001)

- 9  $\mu\text{m}$  Sn surface layer
- Negligible Intermetallic layer mixing (similar profile to unaged)

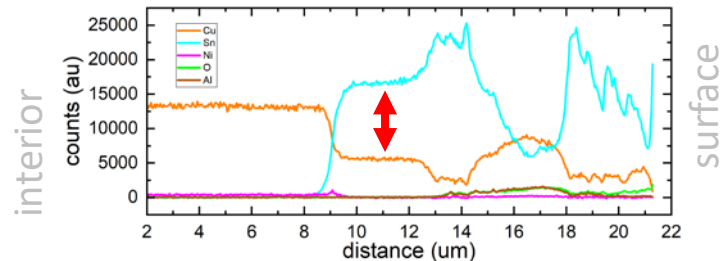
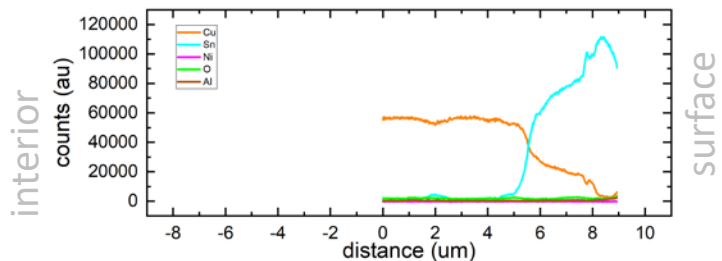
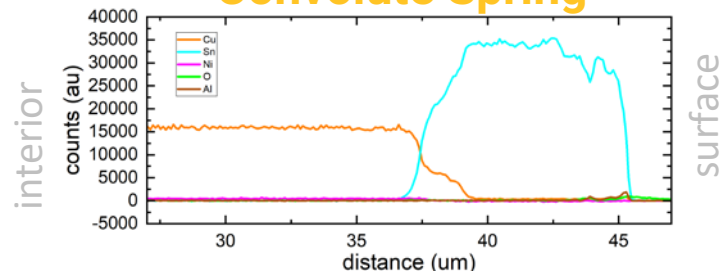
## UV/TC50/HF10 (M1706-0004)

- 4  $\mu\text{m}$  Sn surface layer
- Intermetallic layer mixing
- Localized damage
- Surface oxidation. From HF10? (compare to -0001)

## C-AST 2x (M2208-0001)

- 12  $\mu\text{m}$  mixed-metal surface layer
- Extensive metallic mixing past interface;  
61.5 Sn (%at) is not an intermetallic phase.
- Now more vulnerable to corrosion

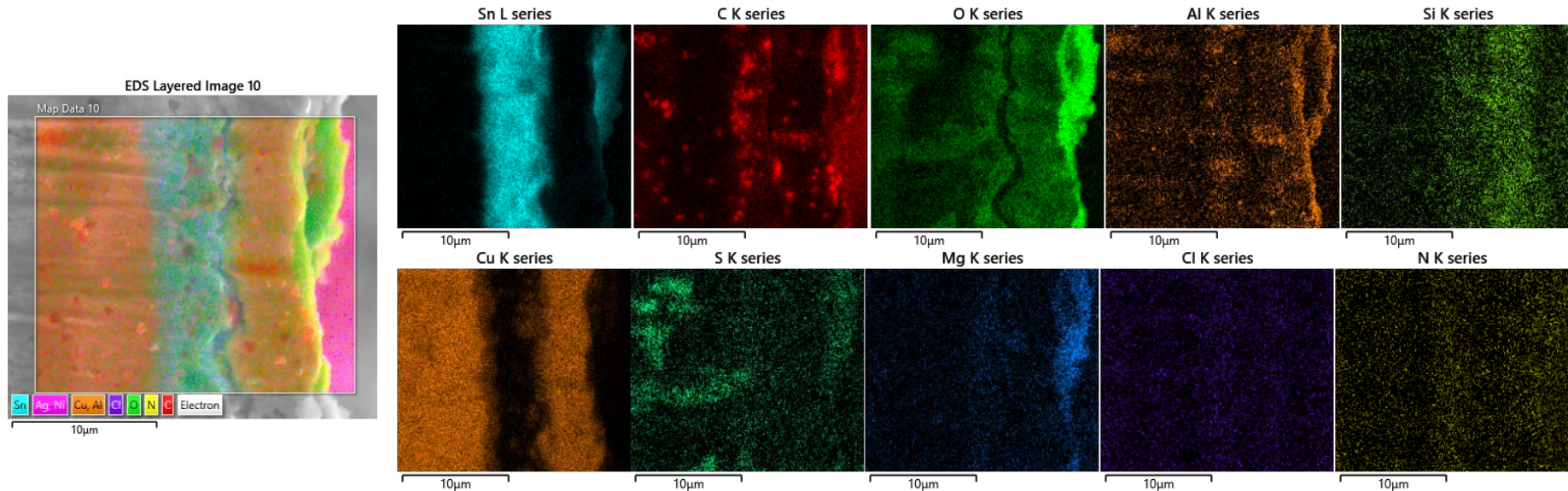
### Convolute Spring





# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

- Cross-section of the metal socket on M1706-0006 (TC 200)

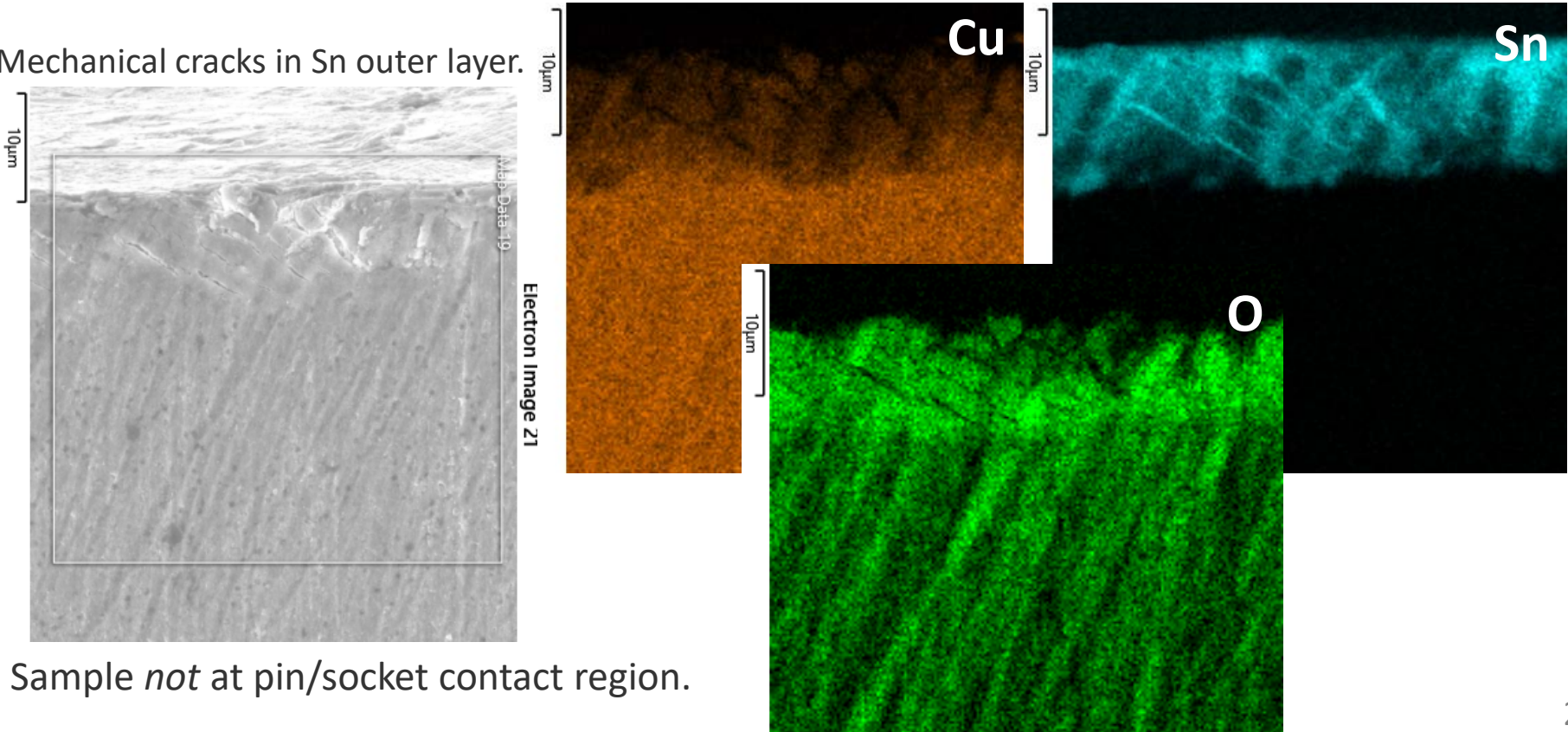


- Sn surface layer is structurally compromised.
- Oxidized Cu (?@ pin/socket contact?), contaminated with Mg, present on top of Sn.
- Sulfur signal in body; C inclusions.

# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

- Cross-section of the metal socket on M1706-0006 (TC 200)

- Mechanical cracks in Sn outer layer.



- Sample *not* at pin/socket contact region.

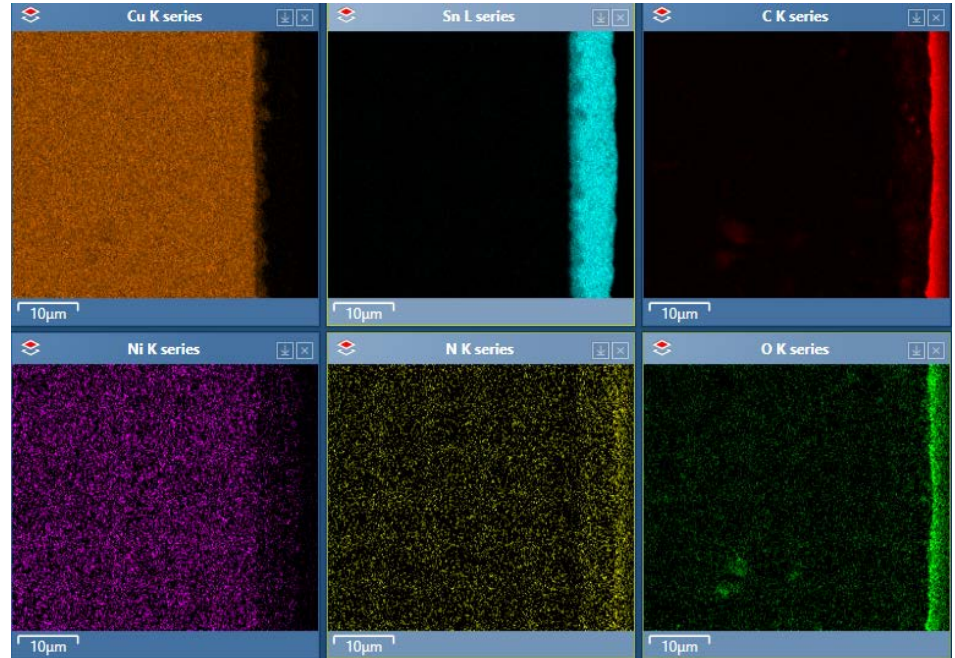
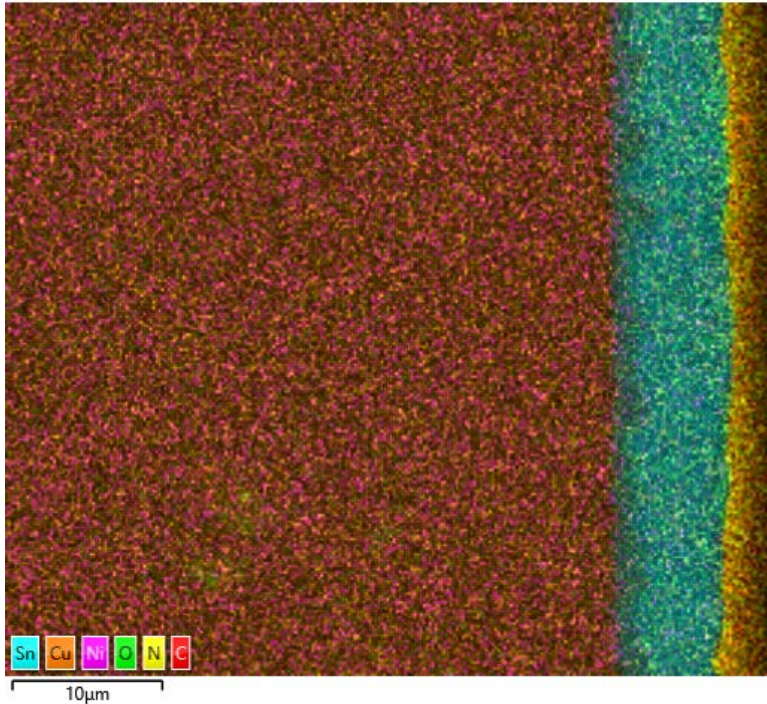


# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

## Convolute Spring

TC200 (M2212-0001)

EDS Layered Image 1



*Nickel in bulk Cu, not Cu/Sn interface (some manufacturers)  
Ni:Cu is 2.6 for M2208-0001, M2212-0001, M2203-0902. < 10% at. as in strengthened Cupronickel alloy*

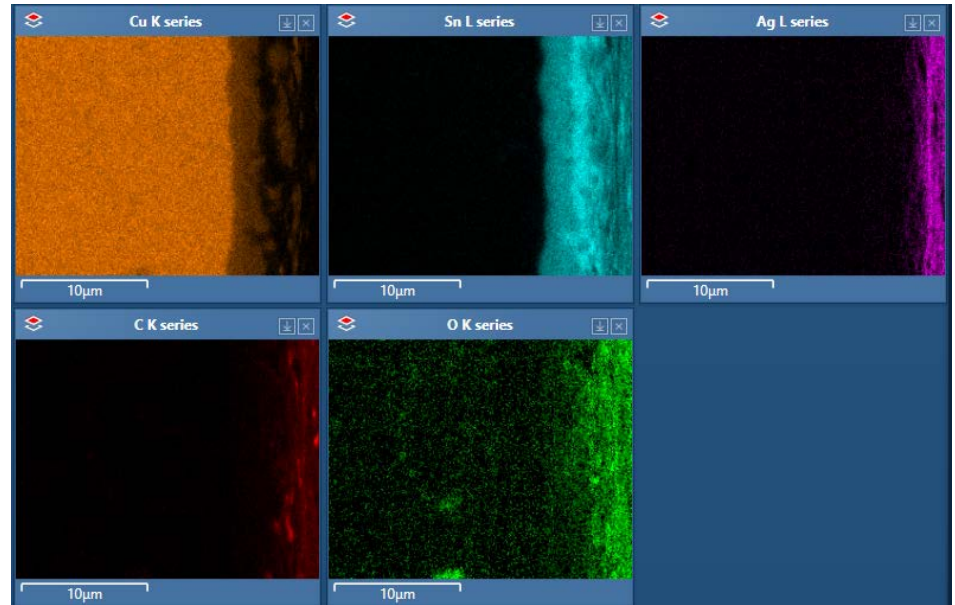
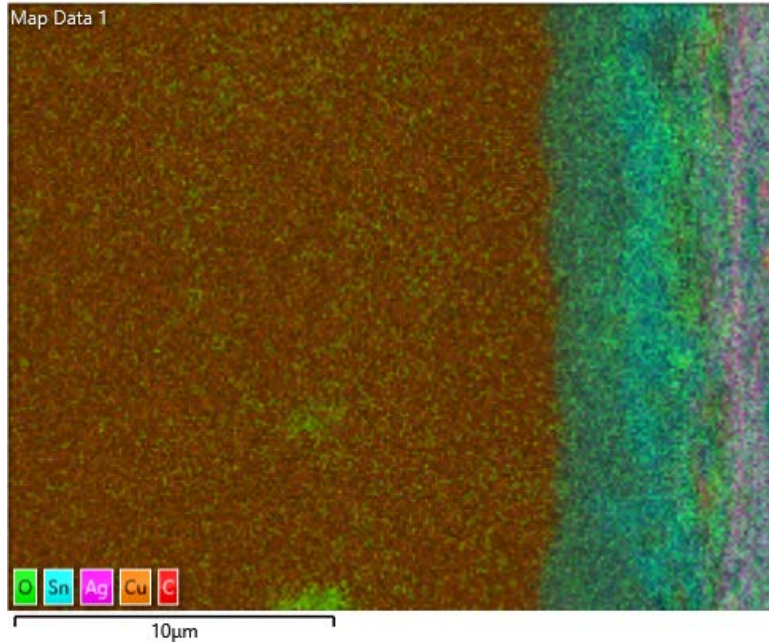


# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

## Convolute Spring

UV/TC50/HF10 (M1706-0004)

EDS Layered Image 1

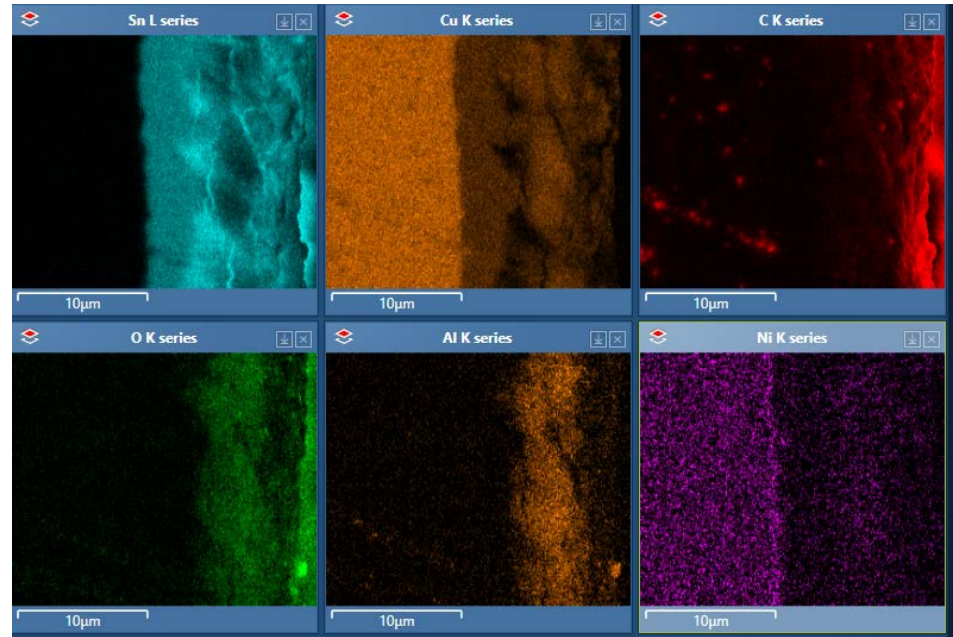
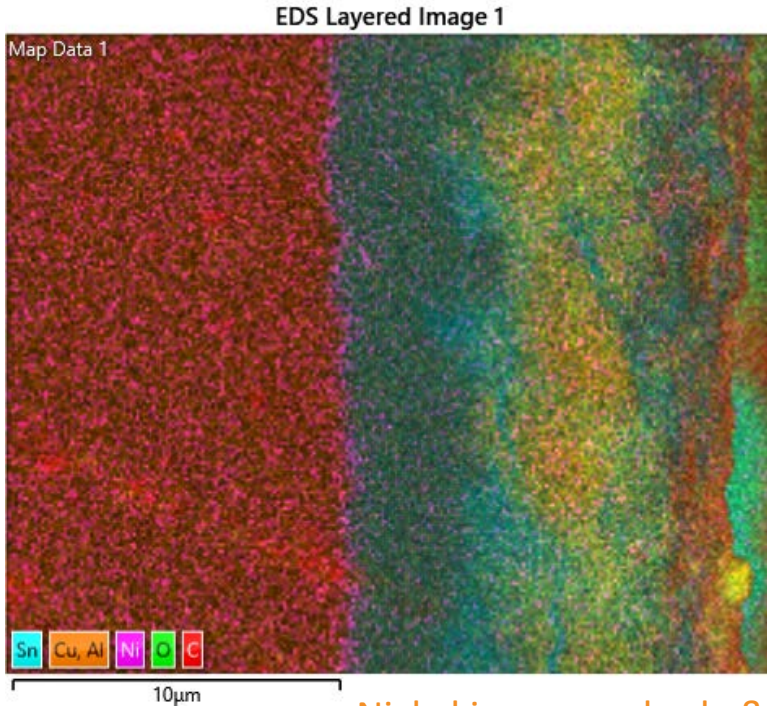


No nickel detected

# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

## Convolute Spring

C-AST 2x (M2208-0001)



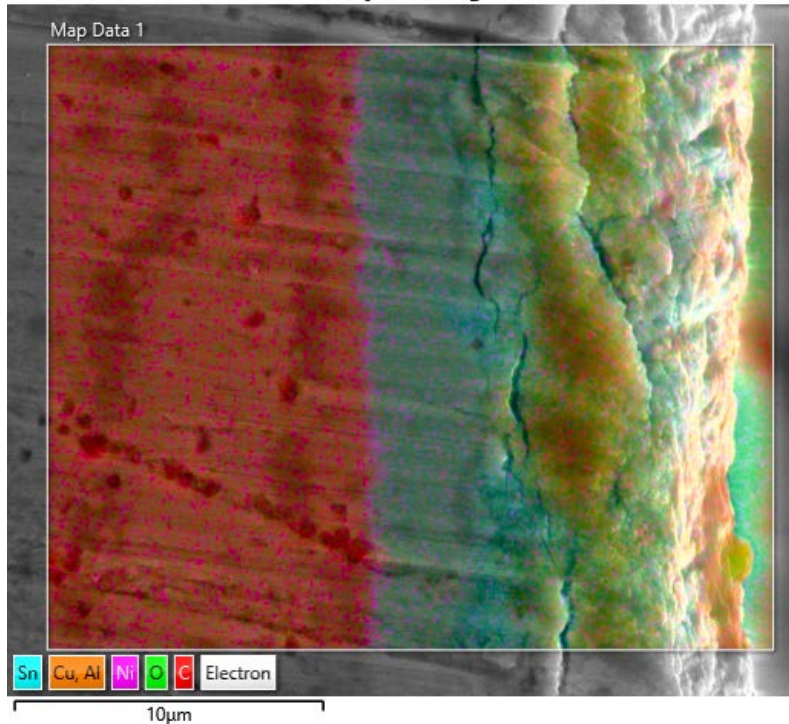
Nickel in copper body & spike at interface | Extensive scale present  
Al, C may be sample preparation artifact (polishing grit)



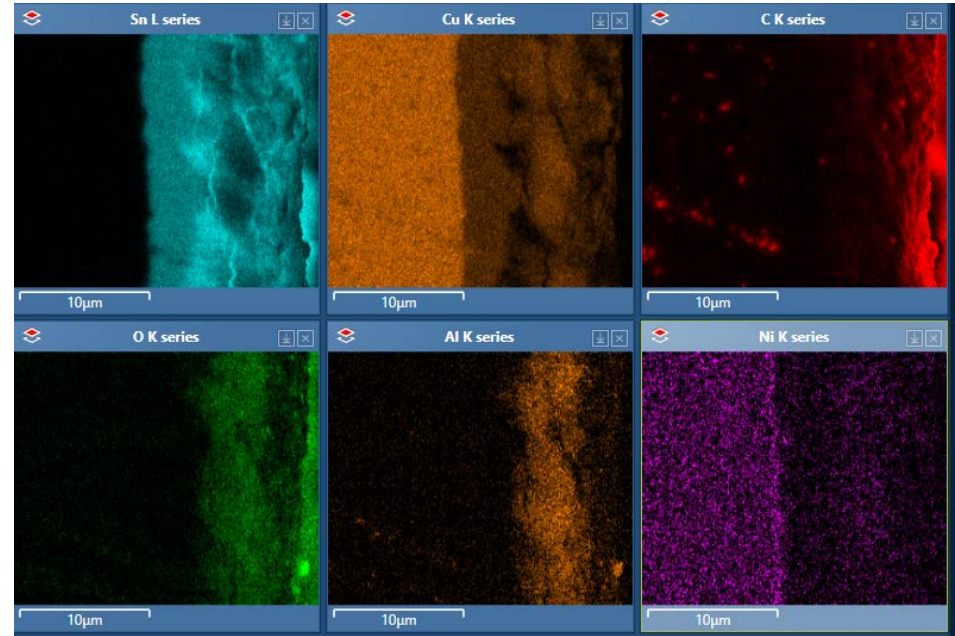
# Failure Analysis of Fielded Cable Connectors: Case Study of Metallic Components

## Convolute Spring

EDS Layered Image 1

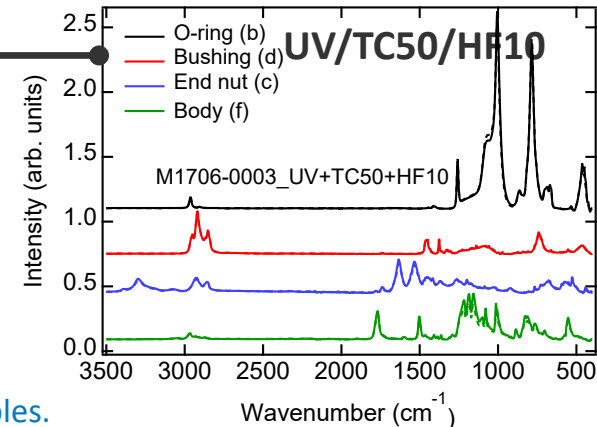
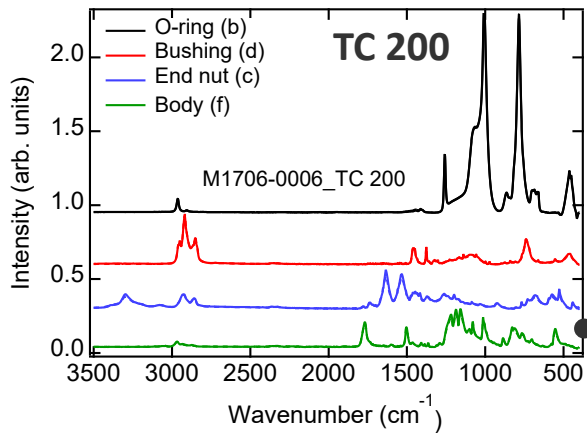
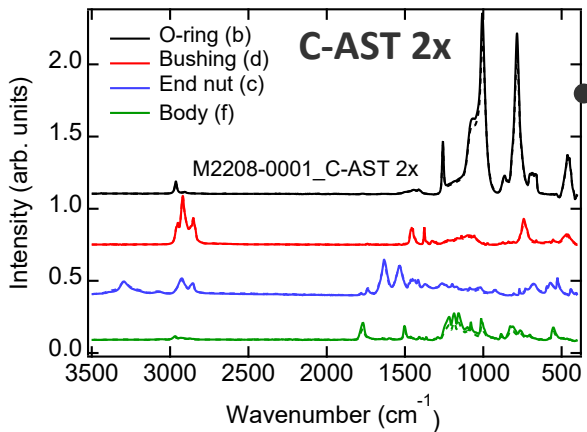


C-AST 2x (M2208-0001)



Nickel in copper body not consistent between samples.  
Multiple material vendors? (Specific Cu alloys observed in other models/components, e.g., aluminum bronze).

# Failure Analysis of Cable Connectors After Accelerated Aging: Case Study of Polymeric Components



- No visual degradation of polymer, these samples.
- No chemical changes detected here in FTIR.

# Today's Presentation

**Background** (motivation, PVQAT survey on industry)

**Experimental details** (samples, failure analysis protocol, methods examples)

**Results:**

Field degraded connectors: *primary*, metallic & polymeric components)

Accelerated aged connectors: *secondary*, metallic & polymeric components)

**Wrapping up** (solutions, summary, acknowledgements)

*Questions and comments welcome, e.g., end of each section.*

# Prevention of Common Degradation/Failure Modes

Please say solutions that come to mind.

- Connector incompatibility: Model-specific jumper presently required, greater # connectors. NEMA, IEC Universal Plug & Socket standards.
- Improper assembly: Training, certification, informative outreach. NABCEP CE Conference. IRA apprenticeship.
- Uncapped ends: In standards, require caps to be shipped with connectors. Verify and inform (NREL experiment). Training, certification, informative outreach.
- Improper sizing of connector:cable: Certify cable/connector combinations (few present uses). Training, certification, informative outreach.
- Improper mechanical fastening to system: Training, certification, informative outreach. DETRIMENTAL mechanical perturbation identified in separate experiments (NREL).
- Live disconnection: Training, certification, informative outreach.
- Incomplete connection: ???

# Fielded Connectors: Common Degradation Modes and Scorched Metal Pins

- Degradation modes from PVQAT: **incompatible makes, uncapped ends, improper assembly** ...incomplete connection, improper sizing, and improper mechanical fastening.
- Examples today: **incomplete connection, incompatible makes, scorched plug & socket.**
  - **Scorched metal pins:** majority of field samples (not accelerated), unexpected, may result from: design, manufacturing, uncapped ends, vibration/bending, CTE/abrasion, live disconnection, ...
  - Other modes *may exist*, e.g., corrosion or fracture of polymers.
- Takeways from forensics:
  - Use 4-wire R-I sweep to quantify, diagnose degraded connectors (vs. low current, 2-wire).
  - Mass transport with intermediate  $\epsilon$  phase Sn:Cu alloy; surface scale formation (maritime);
  - Secondary damage to polymers (body & bushing).



- There are separate 3-year AOP projects at NREL, Sandia about BoS components, including: connectors, cables, cable ties, ...

- Monthly PVQAT TG10 web group meetings covering the state of the industry as well as feedback on testing and results.

- Collaborators needed for on-site PV installation inspections.

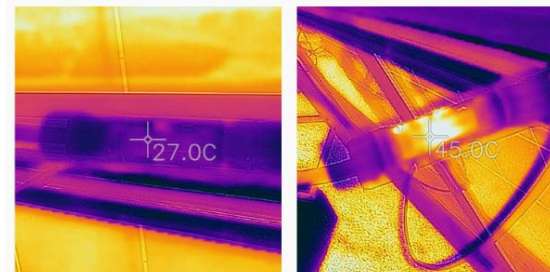
- Collaborators needed for degraded/failed specimens.

Next meeting: 2024/5/21 RE: Failure analysis of cable connectors

- All participants welcome!

Please inquire to: Laurie BURNHAM [lburnha@sandia.gov](mailto:lburnha@sandia.gov); David MILLER [David.Miller@nrel.gov](mailto:David.Miller@nrel.gov)

Also: <https://energy.sandia.gov/programs/renewable-energy/photovoltaics/pv-systems-and-reliability/pv-connectors/>



*Infrared inspection of intact (left) and degraded (right) cable*



*Cracking of tracker cable at the controller box.*

# Acknowledgements

👉 Thanks to:

- Dr. Michael Kempe and Bill Sekulic of NREL.
- Numerous collaborators for field specimens (confidential).
- PVQAT TG10 (~200 recent followers).

CPS 38524/ Agreement 38524 DOE SETO.

This work was authored in part by the National Renewable Energy Laboratory, operated by Alliance for Sustainable Energy, LLC, for the U.S. Department of Energy (DOE) under Contract No. DE-AC36-08GO28308. Funding provided by U.S. Department of Energy's Office of Energy Efficiency and Renewable Energy (EERE) under the Solar Energy Technologies Office (SETO) The views expressed in the article do not necessarily represent the views of the DOE or the U.S. Government. The U.S. Government retains and the publisher, by accepting the article for publication, acknowledges that the U.S. Government retains a nonexclusive, paid-up, irrevocable, worldwide license to publish or reproduce the published form of this work, or allow others to do so, for U.S. Government purposes.

NREL/PR-5K00-87599



NREL STM campus, Dennis Schroeder

Additional comments & questions: [David.Miller@nrel.gov](mailto:David.Miller@nrel.gov)

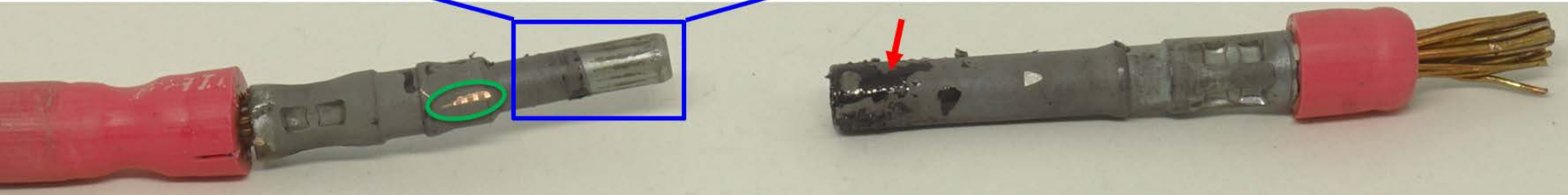
Additional slides  
(reference/supplementary information)

# Morphology Provides Clues for Scorched Pins

- Scorched pins observed on majority of field connectors, this project.
- Residual likeness of convolute spring often observed on metal pin.
- Causes: design, manufacture (plating), contamination, vibration, ?thermal misfit (localized abrasion & wear)?

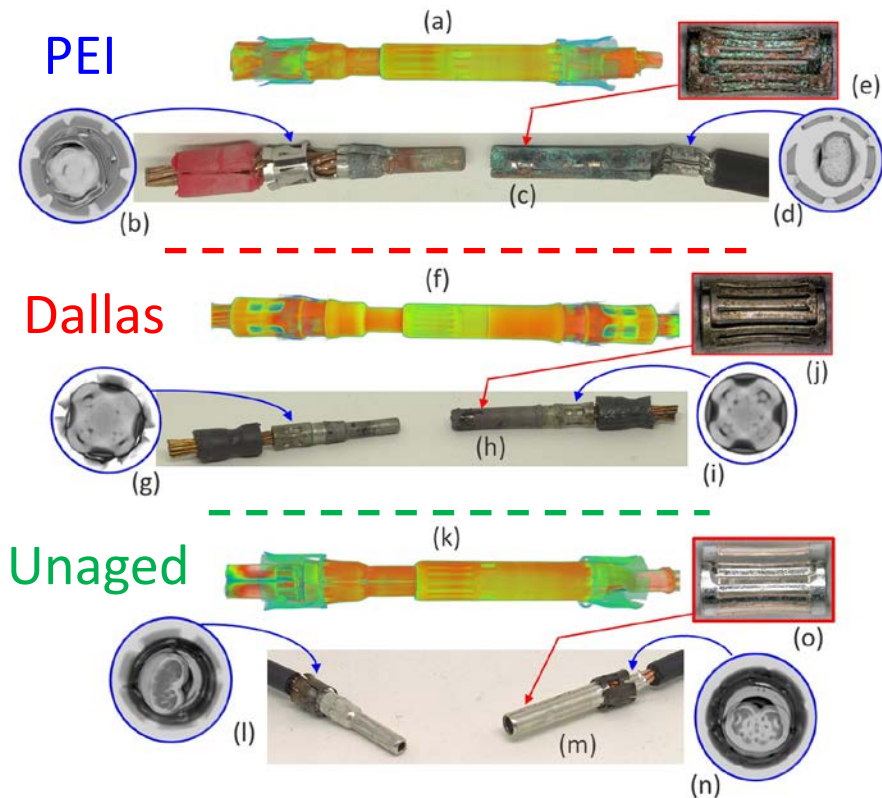


*A field-degraded connector: residual from convolute spring (inset); plastic from the connector body (red); artifact of milling (green)*



# Diagnosing the R-I Specimens Using the Examination Protocol From This Study

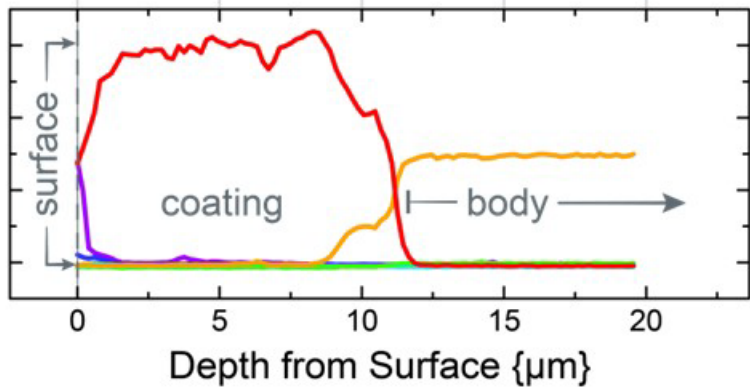
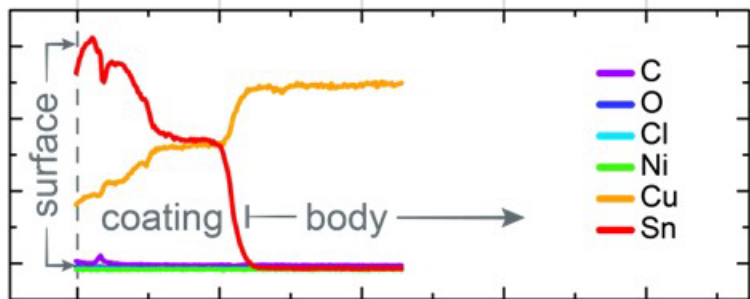
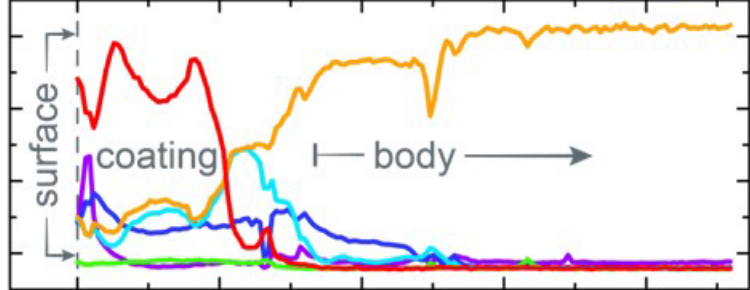
- Incompatible plug & socket compromise mechanical seal of PEI connector.
- Blue-green appearance  $\Leftrightarrow$  ocean side corrosion.
- Mixed gas test ( $H_2S$ ,  $NO_2$ ,  $Cl_2$ , and  $SO_2$ , IEC 62852); fixed gas method ( $H_2O$  and  $SO_2$ , ISO 22479); and stress corrosion test (humid ammonia-air mixture, UL6703) presently assess corrosion.
- Dallas specimen scorched at metal pins and spring, but not at crimps.
- Possibly: design, manufacture (plating), contamination, perturbation, thermal misfit (localized abrasion & wear), live disconnection.
- Barrel style pin (g & i, intended for 7 strand cable, USA); rolled pin (b) intended for higher strand count.



*XCT and external appearance of plug, socket, spring, and crimp after deconstruction.*

# EDS Composition Analysis Readily Distinguishes Connector Metals

Signal Intensity {a.u.}



## PEI (oceanside):

- Greatest concentration of Cl, O.
- 15-25 μm surface scale (corrosion).
- Ni may be artifact of incompatible plug & socket.

## Dallas:

- Temperature → mass transport of Sn & Cu.
- Steady Sn/Cu alloy at  $3 < h < 5 \mu\text{m}$ .
  - $23.6 \pm 0.1 \%$  at. Sn.
  - Intermetallic  $\epsilon$  phase Sn:Cu (23-24 %at.)

## Unaged:

- ~10 μm outer Sn surface layer.
- Rapid Sn → Cu transition at  $8 < h < 11 \mu\text{m}$ .