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Droop Control-Based Dispatch of an Islanded Microgrid With Multiple Grid-Forming Sources

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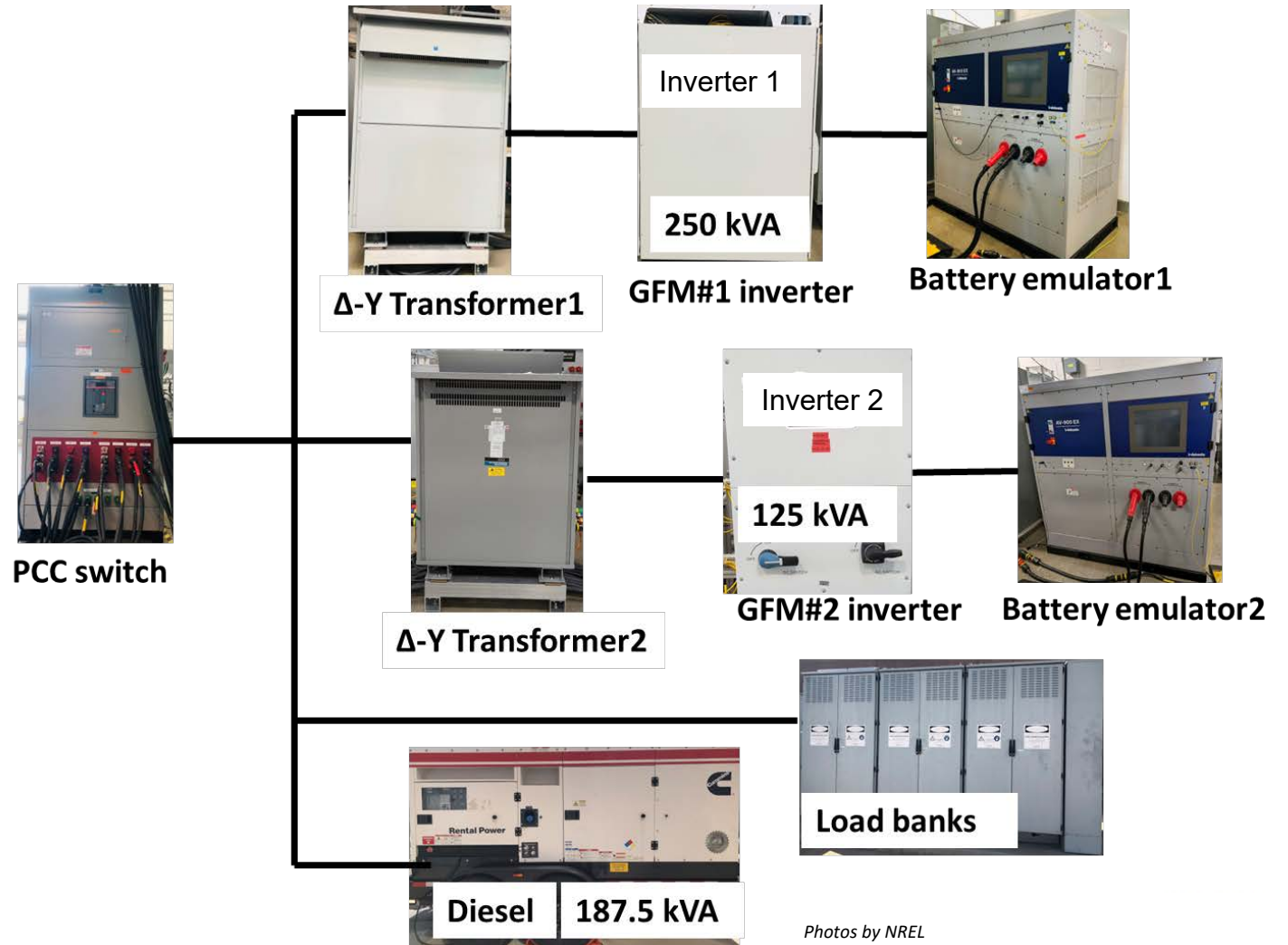
Background & Objectives

- Grid-forming (GFM) inverters are expected to parallel synchronous generators (SGs) before rotating, fossil fuel-based SGs are phased out.
- Primary droop control allows GFM inverters to share power without communications; however, it is necessary to dispatch GFM inverters and/or SGs with the desired output power for better energy management.
- **Goal of this work**: Develop an analytic approach to dispatching GFM inverters and SGs with the desired output power.
 - Shift the droop intercept up/down while maintaining the same frequency operating point to improve transient stability.

This concept is demonstrated through a pure hardware setup with two commercial inverters and one diesel generator.

Microgrid System Under Study

- Universal Interoperability for Grid-forming Inverters (UNIFI) Consortium is conducting multi-vendor testing to ensure that GFM inverters work together
- UNIFI 1-MW multi-vendor GFM inverter test bed:
 - A microgrid system to demonstrate the concept
 - PCC switch
 - Two commercial GFM inverters and one diesel generator
 - Each GFM inverter connected to a Δ -Y transformer
 - Load banks (RLC load).

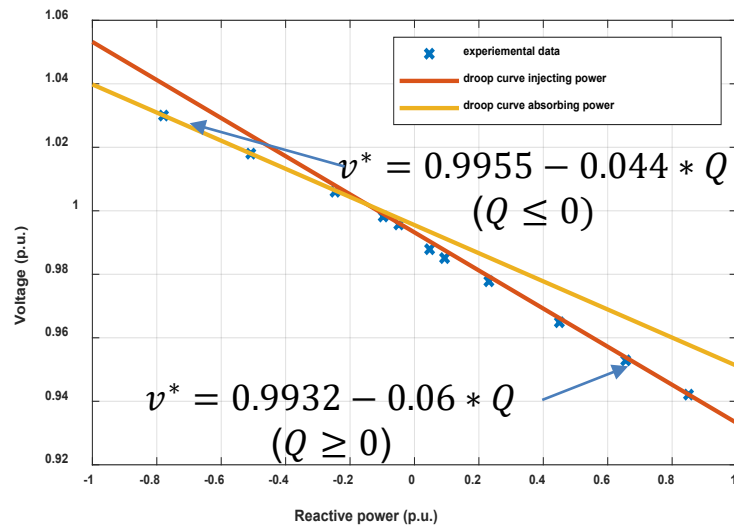


Photos by NREL

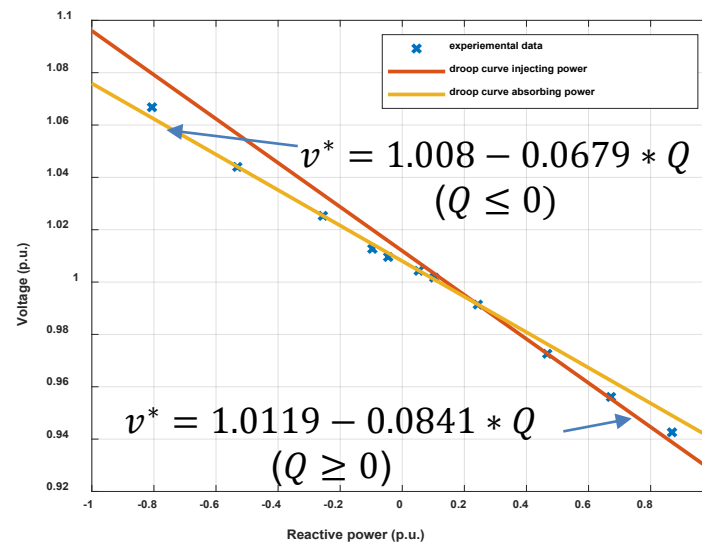
Droop Characterization of the GFM Sources

- The frequency droop matched the settings without adjustments.
- The voltage droop was off and needed to be characterized.
 - Steady-state test: 5%, 10%, 25%, 50%, 75%, 100%, PF=1, 0.8 lagging and leading, pure inductive and capacitive loads of the inverter capacity.

GFM#1 voltage droop characterization



GFM#2 voltage droop characterization

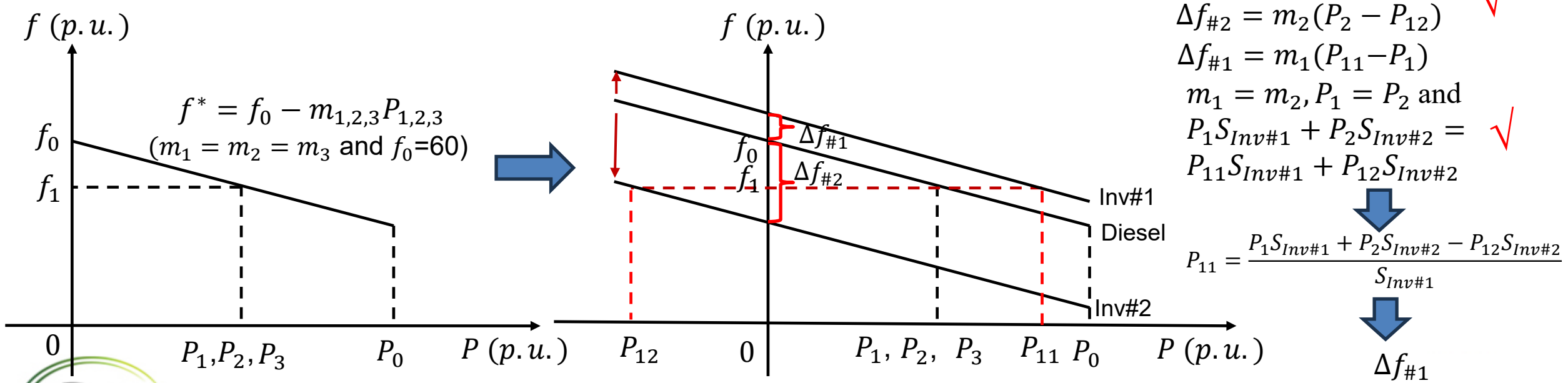


Diesel generator droop characteristics

- The frequency droop is 0.6% with a bias of -0.36 Hz representing the droop intercept of 60 Hz.
- The voltage droop is 3.7% with a zero bias representing the droop intercept of “1” p.u. voltage.

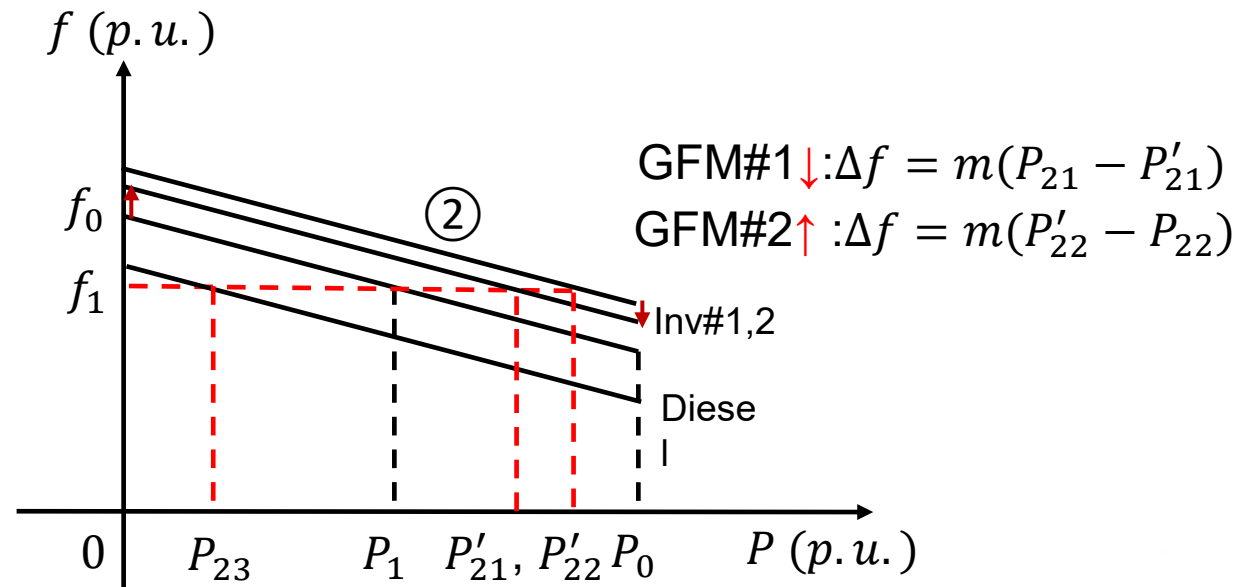
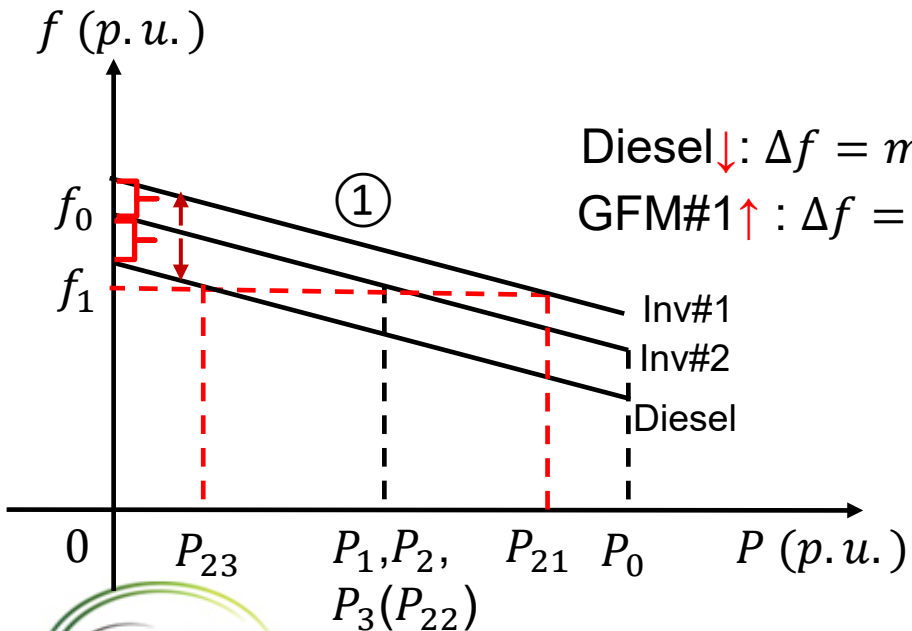
Drop-Based Real-Time Dispatch—Scenario #1

- Charge one GFM inverter with other GFM sources supplying the loads:
 - Start from equal power sharing (left figure).
 - Dispatch GFM#2 to charge the battery due to low SOC with the target power (right figure).
 - Strategy: Shift the frequency droop intercept of GFM#2 ↓ and GFM#1 ↑, and keep the diesel at the same operating point for better stability.



Drop-Based Real-Time Dispatch—Scenario #2

- Reduce the diesel output and let the two GFM's equally share power (start from equal power sharing):
 - Step 1: Shift the frequency droop intercept of diesel ↓ and GFM#1 ↑, and keep GFM#2 at the same operating point for better stability.
 - Step 2: Shift the frequency droop intercept of GFM#1 ↓ and GFM#2 ↑ for equal power sharing, and keep the diesel at the same operating point for better stability.



Experiment Setup

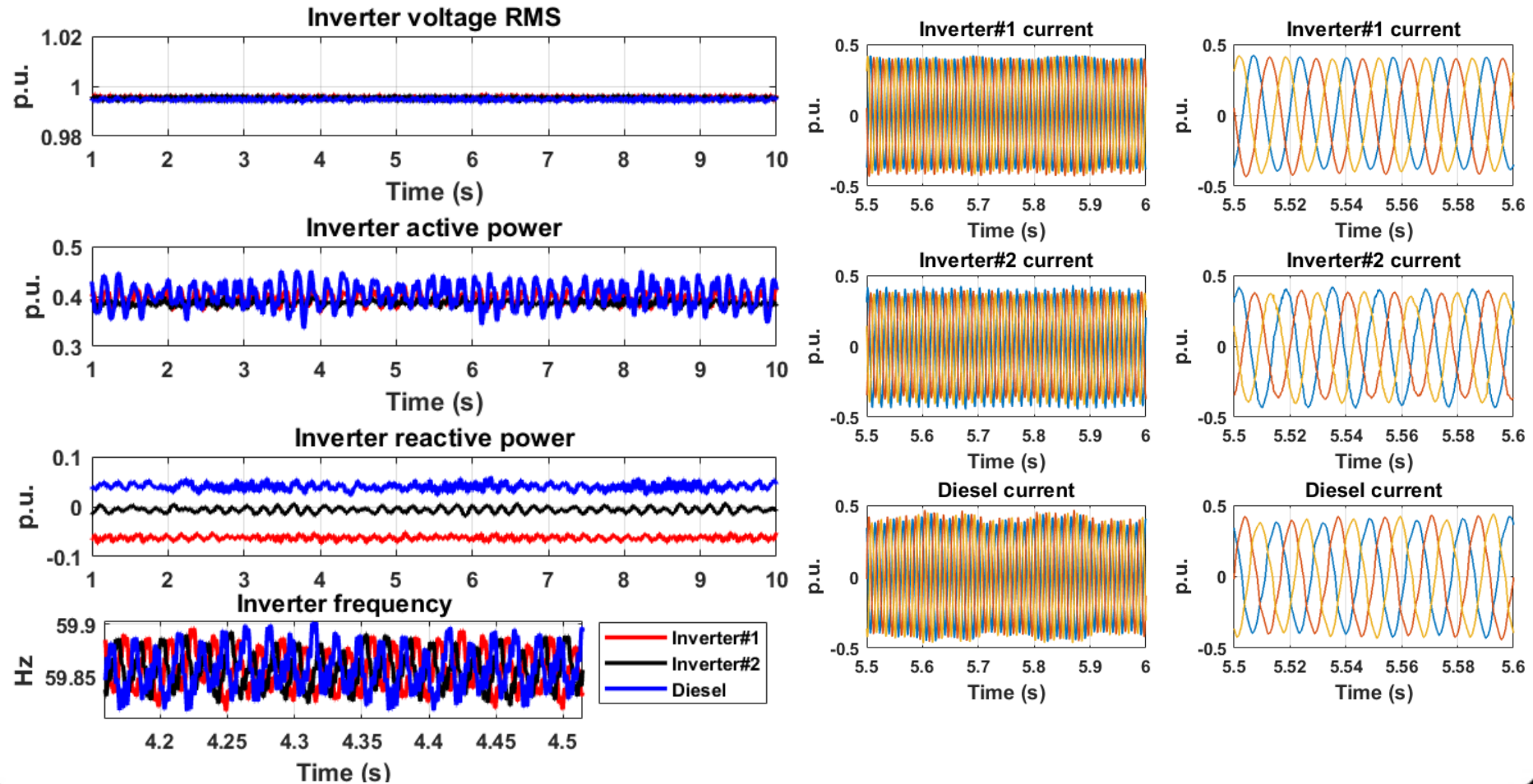
System Configuration

- Use the same frequency droop for all three GFM sources (0.6%).
- The voltage droop ($n * Q * 480$) needs to be compensated to avoid unnecessary reactive power flow.
- For the real-time dispatch, a controller is developed to simultaneously dispatch the three GFM sources through Modbus TCP/IP.

Element	Capacity	Configuration/Feature
Inverter 1	250 kVA	Droop: 0.6% (f-P) and 6% (v-Q). Change f^* directly to shift the droop intercept.
Inverter 2	125 kVA	Droop: 0.6% (f-P) and 5.68% (v-Q). Change the bias (default is zero) to shift the droop intercept.
Diesel generator	187.5 kVA	0.8 PF, 0.6% (f-P), and 6% (v-Q). Change the bias (default is -0.36 Hz) to shift the droop intercept.
Battery emulator 1	±660 kW	DC voltage: 900 V; current: 306 A; power: 275 kW
Battery emulator 2	±250 kW	DC voltage: 850 V; current: 162 A; power: 137.5 kW
Transformer 1	500 kVA	Delta: 480 V; wye: 480/277 V; current: 601 A, Z: 6%
PCC switch	1600 A	1600-A 4-pole circuit breaker
Transformer 2	250 kVA	Delta: 480 V, wye: 480/277 V; current: 300A, Z: 4.4%
Load banks	2*250 kVA	2 units in parallel 480 V, 3 phase

Experiment Results

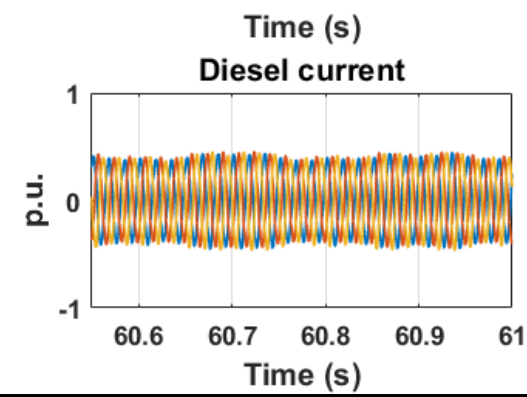
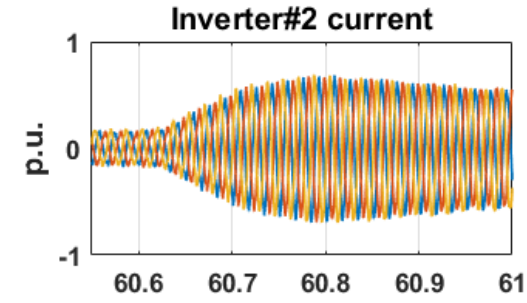
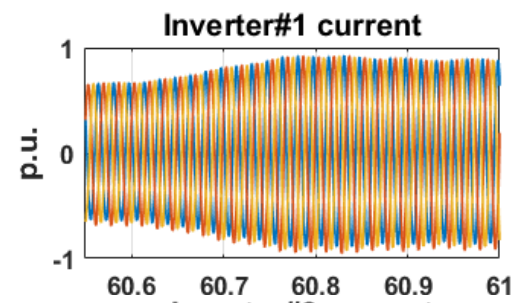
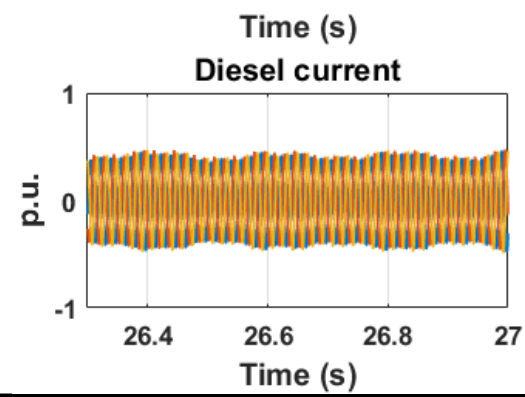
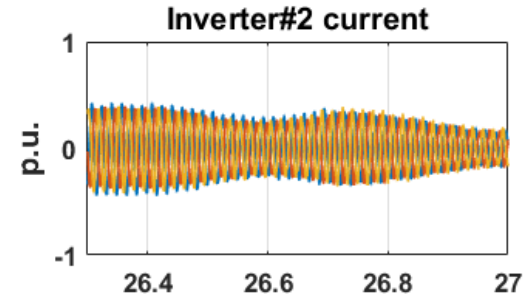
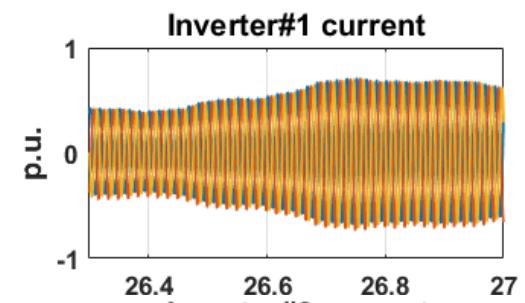
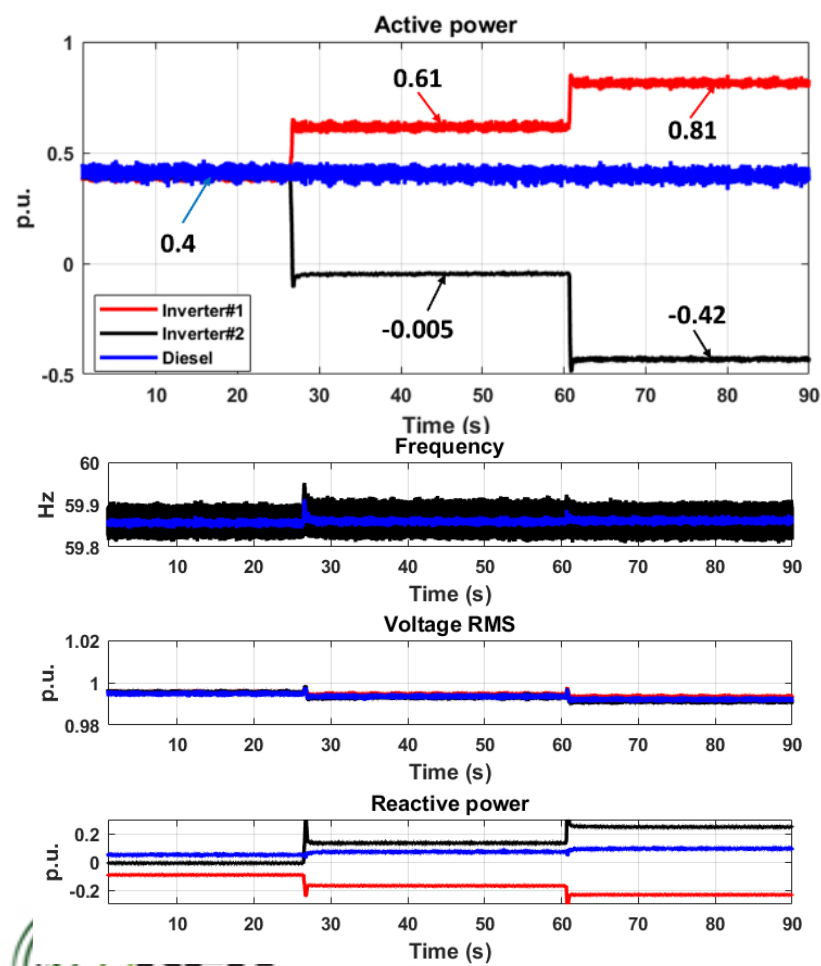
- Baseline: GFM sources **equally share power** on a per-unit basis.
 - Total load is equal to 40% of the total capacity of the three GFM sources.



Experiment Results

– Scenario #1: Dispatch GFM#2 Absorbing Desired Power

- Step 1: GFM#2 injects zero power; Step 2: GFM#2 absorbs 0.4 p.u. active power.



Conclusion:

Two steps are taken because there might be instability with such a big frequency intercept shift:

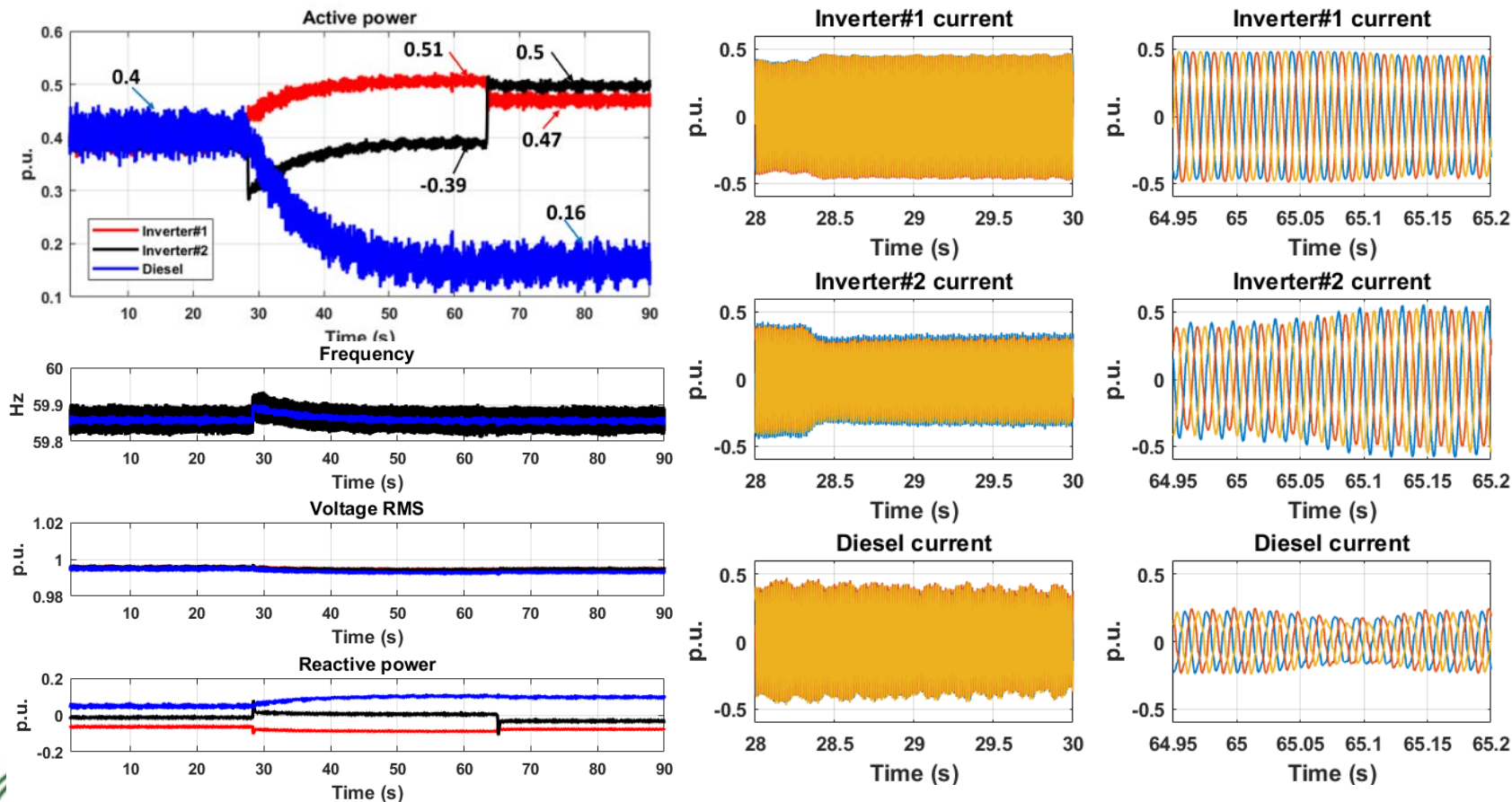
- The overall dispatch target is achieved.
- The tracking error is due to the round-up of the frequency droop intercept

$$GFM1: \Delta f = 0.006 * (0.4 - (-0.4)) * 60 = 0.288 \approx 0.29 \text{ Hz}$$

All GFM sources can only take two decimals.

Experiment Results

- Scenario #2: Reduce power in the diesel and let the GFM inverters equally share power.
 - Step 1: Diesel outputs 0.15 p.u. (minimal loading), GFM#1 takes over the power from the diesel.
 - Step 2: GFM#1 and GFM#2 equally share power.



Conclusion:

- The overall dispatch target is achieved.
- The tracking error is due to the round-up of the frequency droop intercept.
- Demonstrates the concept of dispatching GFM sources' power through dispatching the frequency droop intercept.

Conclusions

- The experimental results show that the dispatched GFM sources respond to the changed droop intercept to output the desired active power, and it is important to maintain the same frequency.
- It is important to compensate for the voltage drop across the transformers in the voltage droop equations to achieve the expected reactive power sharing.
- Even though the concept is demonstrated in an islanded microgrid, the concept is applicable to grid-connected operation.
- This dispatch algorithm can be included in energy management systems to dispatch a system with both GFM and grid-following (GFL) inverters.

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