

# Emerging magnetic materials for electric vehicle drive motors

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Increasing demand for electric vehicles (EVs) is increasing demand for the permanent magnets that drive their motors, as approximately 80% of modern EV drivetrains rely on high-performance permanent magnets to convert electricity into torque. In turn, these highperformance permanent magnets rely on rare earth elements for their magnetic properties. These elements are "critical" (i.e., at risk of limiting the growth of renewable energy technologies such as EVs), which motivates an exploration for alternative materials. In this article, we overview the relevant fundamentals of permanent magnets, describe commercialized and emerging materials, and add perspective on future areas of research. Currently, the leading magnetic material for EV motors is Nd<sub>2</sub>Fe<sub>14</sub>B, with samarium-cobalt compounds (SmCo<sub>5</sub> and Sm<sub>2</sub>Co<sub>17</sub>) providing the only high-performing commercialized alternative. Emerging materials that address criticality concerns include Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>, Fe<sub>16</sub>N<sub>2</sub>, and the L1<sub>0</sub> structure of FeNi, which use lower cost elements that produce similar magnetic properties. However, these temperature-sensitive materials are incompatible with current metallurgical processing techniques. We provide perspective on how advances in low-temperature synthesis and processing science could unlock new classes of high-performing magnetic materials for a paradigm shift beyond rare earth-based magnets. In doing so, we explore the question: What magnetic materials will drive future EVs?

# Introduction

Huge quantities of high-performance permanent magnets (PMs) are needed for continued deployment of renewable energy technologies.<sup>1,2</sup> In particular, the PM motors used in the drivetrains of >80% of electric vehicles (EVs) each require >2 kg of PMs, so massive amounts of PMs will be needed to meet the projected growth in EVs (Figure 1).<sup>3</sup> The magnetic materials currently used by these motors contain critical rare earth elements (REEs). While the exact definition of criticality depends on the technoeconomic metrics used, materials are generally considered critical when threats to their supply chain(s) (e.g., geopolitical risks, rising costs, limited availability, etc.) could constrain deployment of the dependent technologies.<sup>3</sup> Many REEs are defined as critical by the US Department of Energy because the dramatic expansion of renewable energy technologies requiring REEs will put increasing pressure on their supply chains. Developing new PM materials can help alleviate this criticality issue. The canonical example of a REE PM is Nd<sub>2</sub>Fe<sub>14</sub>B, which was independently discovered and developed in the mid-1980s by researchers in Japan's and the US' automotive industries; it is only fitting that development of next-generation PMs beyond materials such as Nd<sub>2</sub>Fe<sub>14</sub>B is also motivated by mobility.<sup>4,5</sup>

This article focuses on the challenges facing current PM technologies, surveys emerging materials, and adds perspective on future research. We summarize the fundamental physics behind the role of PMs in EV motors, describe the current state-of-the-art as well as the shortcomings therein, and detail some of the emerging technologies at the laboratory and early-startup stage. The authors' background in experimental materials discovery and design inspires our effort to identify how emerging materials hint at broad strategies for discovering and designing new PMs. This discussion is focused on early-stage research of intrinsic materials, though we recognize that for commercialization PMs must be heavily engineered beyond their intrinsic properties. Our overarching goal is to explore the question: What magnetic materials will drive future EV motors?

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PMs radially distributed in the rotor.

# **Fundamentals of PM motors**

(Electro)magnetic repulsion is the basic principle underlying electric drive motors: magnetic fields (B) from a static electromagnet and the PMs repel one another, turning the rotor (Figure 1b). Larger fields therefore lead to more force. PMs enable highly efficient motors because they generate fields without the need for additional energy inputs or moving electrical contacts. A representative magnetic hysteresis loop for a ferromagnetic compound is depicted in Figure 2. PM motors operate in quadrant two of this hysteresis loop (Figure 2b) against the opposing magnetic field of the electromagnet (shown as the horizontal axis, H). The PM strength is determined by remanent magnetization  $M_r$ , while the coercive field  $H_c$  represents its resistance to the opposing field. These terms describe the magnetic energy density  $(BH)_{max}$ , considered the PM figure of merit, so optimizing them is required for highperformance materials. For a competitive  $(BH)_{max}$ , it is critical that both  $M_r$  and  $H_c$  are suitably large. A summary of important terms related to PMs can be found in Table I.

How can a phase with intrinsically strong PM parameters defined in Table I—be identified? Although it is difficult to predict the exact magnetic properties of a phase, there are general chemical trends that can be followed to identify candidates. First, compounds should be rich in open shell 3d transition metals (TMs) such as Fe and Ni, which lead to high  $M_s$  from the large fraction of unpaired spins. However, TMs alone are often soft ferromagnets, meaning the magnetic moments of each atom align parallel (ferromagnetism), but the net magnetization is easily changed by an opposing field (i.e., soft). To make hard ferromagnets (with large  $H_c$  values), magnetocrystalline anisotropy must be induced. Additional nonmagnetic elements (e.g., Al, B, O, N) can cause structural changes that support magnetocrystalline anisotropy, such as cubic to tetragonal distortions. In this case, the goal is to create a uniaxial "easy" crystallographic axis of magnetization, leading to an energy barrier to rotate spins through the concomitant "hard" plane. However, nonmagnetic elements dilute the magnetic atoms reducing  $M_s$  and, in anion-rich systems, often lead to ferrimagnetism (e.g., Fe<sub>3</sub>O<sub>4</sub>) or antiferromagnetism (e.g., Mn<sub>3</sub>N<sub>2</sub>). The role of REEs in PMs is also to increase magnetocrystalline anisotropy. Through spin–orbit coupling, noninteracting 4*f* electrons align with TM-rich frameworks and lead to high  $H_c$  values.

Maintaining a large  $(BH)_{max}$  at elevated temperatures is a key design criterion. Even below the ferromagnetic ordering temperature  $(T_c)$ , performance metrics are influenced by temperature (i.e., softening/weakening as T approaches  $T_c$ ) as the energy scale of thermal fluctuations becomes comparable to the energy scale of magnetic interactions in a material. Magnets used in EV motors are expected to operate as high as 150-220°C.<sup>8</sup> While the temperature dependence of magnetic properties is strongly affected by microstructural engineering and dopants, identifying a phase's  $T_{\rm C}$  is a functional proxy for most cases. Given that the useful magnetic properties of a phase begin to significantly decrease at ~80% of its  $T_{\rm C}$ , the  $T_{\rm C}$  should be >225°C.<sup>9</sup> In some of the emerging materials discussed below, such as  $Fe_{16}N_2$ , the material's  $T_{\rm C}$  is higher than its decomposition temperature.<sup>10</sup> Thus, operational thermal stability of the material is an additional key factor that must be considered for practical high-performance magnets.



#### Table I. Relevant terms for permanent magnets.

- Magnetic Field (H or B): Total field B is the sum of the external field (H) and the magnetization (M) of a material (i.e.,  $B = \mu_0[H + M]$ )
- Saturation Magnetization (*M*<sub>s</sub>): Magnetization achieved when all magnetic moments of the ferromagnetic phase are aligned. Units: G or emu/cm<sup>3</sup> (cgs); A·m<sup>2</sup>/kg or A/m (SI)
- Remanent Magnetization (*M<sub>r</sub>*): Magnetization at zero applied field (same units as *M<sub>s</sub>*). The unitless ratio *M<sub>r</sub>/M<sub>s</sub>* is also useful: ideally as close to 1 as possible
- Coercivity (H<sub>c</sub>): Value of the applied opposing field needed to reduce M to zero (i.e., demagnetize the sample). Arises from a combination of intrinsic (material property) and extrinsic (microstructure property) magnetic anisotropy. Units: Oe (cgs); T or A/m (SI)
- Magnetocrystalline Anisotropy: An intrinsic property related to the anisotropy field (*H*<sub>a</sub>) needed to rotate a domain between crystallographic axes. Units: Oe (cgs); T or A/m (SI)
- Magnetic Energy Density ((*BH*)<sub>max</sub>): The maximum magnetostatic energy of a PM. Measured as the maximal product of I*B*·*H* on demagnetization. Units: MG0e (cgs); kJ/m<sup>3</sup> (SI)
- Curie Temperature (T<sub>C</sub>): Temperature below which the atomic magnetic moments of the ferromagnetic phase are ordered. Above this temperature, there is no net magnetization
- Temperature Coefficient: As key magnetic terms tend to decrease with increasing temperature, the rate of decrease is often quantified in a derivative (e.g., dH<sub>c</sub>/d7). Units: %/K

These values can be determined via magnetic susceptibility measurements as detailed by Reference 6. Magnetic units are notoriously confusing, as CGS and SI standards are both in active use.<sup>7</sup>

# **Currently commercialized PM materials**

The highest-performing commercialized magnets contain REEs: Sm-Co and Nd-Fe-B magnets. As previously described, REEs improve key properties of ferromagnets. Next, we distill a few lessons from these examples.

# Samarium-cobalt magnets

Sm-Co magnets were developed in the early 1950s and were among the first materials with large enough  $H_c$  to resist reorienting against a reverse field. This meant a useful torque could be generated, spurring interest in PM motors.<sup>11</sup> There are two main stoichiometries with good PM properties: SmCo<sub>5</sub> and Sm<sub>2</sub>Co<sub>17</sub>. These phases share high  $T_{\rm C}$  and very large  $H_{\rm c}$ —the greatest of any commercialized magnet. SmCo<sub>5</sub> (**Figure 3**a) possesses a giant axial magnetocrystalline anisot-ropy resulting from the unquenched prolate *f*-electron density of Sm ions, with orbital moments aligned parallel to spin moments of Co (Figure 3d).<sup>12,13</sup> The Sm *f* shell aligns along the crystallographic *c*-axis, because this minimizes Coulombic interaction with the crystal field of hexagonal Co layers, and strong spin–orbit coupling concomitantly aligns spins.<sup>14</sup> SmCo<sub>5</sub> is hexagonal; however, Sm<sub>2</sub>Co<sub>17</sub> is either hexagonal or rhombohedral depending on the stacking sequence of the mixed Sm-Co planes (Figure 3b–c). The magnetocrystalline



anisotropy of Sm<sub>2</sub>Co<sub>17</sub> is one-fourth that of SmCo<sub>5</sub> because the Co–Co dumbbells that replace some of the Sm lead to multiple easy magnetization directions, reducing overall anisotropy.<sup>15</sup> Although Sm-Co magnets played an important role in the development of PM electric motors, they suffer from lower magnetization and higher cost than competitors, making them only appropriate for niche applications, especially those requiring high temperatures.

## *Neodymium iron boride (Nd<sub>2</sub>Fe<sub>14</sub>B)*

The discovery of REE-based PM neodymium iron boride  $(Nd_2Fe_{14}B)$  ushered in an exciting new era in PM research.  $Nd_2Fe_{14}B$  has a tetragonal structure with strong uniaxial anisotropy: the *c*-axis is its easy axis of magnetization (**Figure 4**). Each B is coordinated by six Fe in a distorted trigonal prismatic environment. Two of the B-occupied prisms share an edge, creating quasi-0D Fe<sub>10</sub>B<sub>2</sub> "bowties" punctuating a matrix otherwise comprising Fe and Nd. The large fraction of Fe contributes a large  $M_s$  (38  $\mu_B$  per formula unit), and the tetragonality induced by B (alongside magnetocrystalline

anisotropy from Nd *f* orbitals) leads to an anisotropy field  $(\mu_0 H_a)$  of 6.7 T at room temperature.<sup>16</sup> This high performance has led Nd<sub>2</sub>Fe<sub>14</sub>B to be the primary magnet material for EV motors.<sup>3</sup>

Though Nd<sub>2</sub>Fe<sub>14</sub>B has a high (BH)<sub>max</sub> at room temperature, its performance declines dramatically with increasing temperature (Figure 5a). To meet the elevated temperature conditions in EV motors, heavy REEs such as Dy or Tb are partially substituted for Nd to form (Nd,Dy/Tb)<sub>2</sub>Fe<sub>14</sub>B, which increases the magnetocrystalline anisotropy and  $T_{\rm C}$ , resulting in higher coercivity and better thermal performance.<sup>17,18</sup> However, incorporation of Dy deteriorates the magnetization as both the orbital and spin magnetic moments of the heavy REEs couple antiferromagnetically with those of Fe in (Nd,Dy)Fe14B. Significant effort has been applied to engineer the microstructure of Nd<sub>2</sub>Fe<sub>14</sub>B magnets in hopes of reducing or eliminating reliance on Dy, but heavy REEs-which are generally considered more critical-remain the most effective way to maintain the (BH)<sub>max</sub> of Nd<sub>2</sub>Fe<sub>14</sub>B at elevated temperatures.<sup>19–21</sup> The temperature dependence of  $(BH)_{max}$  values of these established materials are shown in Figure 5a.





# Other commercialized magnets

Many other magnetic materials have been researched, and several have been commercialized, but they are too weak or expensive for EV applications. Ferrite-based magnets (e.g.,  $SrFe_{12}O_{19}$ ) are low-cost and widespread but weak ((*BH*)<sub>max</sub>~5 MGOe).<sup>22</sup> Alnico magnets (composite alloys of Fe with Al, Ni, and Co) are moderately powerful  $((BH)_{\text{max}} \sim 10 \text{ MGOe})$  but tend to be high-cost relative to their performance.<sup>9,22</sup> Although analysis based on electron microscopy suggests that optimizing the microstructure of Alnico could improve  $(BH)_{\text{max}}$  to ~20 MGOe,<sup>23</sup> this upper limit still falls below the performance of REE magnets.

# **Criticality issues**

Resource challenges limit the scalability of current highperformance REE magnets. These challenges include high costs associated with scarce and difficult-to-refine elements, supply chain risks, or both. As shown in **Figure 6**, REEs are not the only materials constrained by these challenges: Co too suffers as it is the most expensive 3d metal and is heavily used by other EV technologies, such as batteries. These



criticality issues could hinder the deployment of technologies based on the current high-performing magnets  $(Nd_2Fe_{14}B and Co-Sm)$ .

What elements should applications-focused researchers prioritize? Ideally, the elements should be low-cost, low-toxicity, produced in large quantities, and support large  $(BH)_{max}$ . Fe tops the list. Mn could also supply large magnetic moments with low materials costs. As 4*d* and 5*d* metals could boost coercivity via spin–orbit coupling, Zr, Nb, Mo, and W could also be important constituents of future low-cost high-performance magnets. Sm is a low-cost REE, as there are currently no large-scale applications of the element. However, criticality could change over time with market conditions and technological development. Research using critical elements can reveal valuable fundamental insights, but researchers should be clear-eyed about scalability, economic, and social (as well as technical) challenges.

# **Emerging PM materials**

Three emerging materials show the greatest promise for nearterm development as magnets for EVs:  $Sm_2Fe_{17}N_3$ ,  $Fe_{16}N_2$ , and the L1<sub>0</sub> structure of FeNi. These materials exhibit both promising magnetic properties (Figure 5b) and comprise (relatively) low-cost elements. However, these phases are less thermally stable than established technologies, so new processing techniques will be needed to realize their potential.

# Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>

One path to reduce criticality concerns is via REE-based materials that contain either a lower REE fraction and/or REE elements that are less critical than Nd and Dy. Building off the exceptional magnetic properties of  $SmCo_5$  and  $Sm_2Co_{17}$ , other materials in these and related families were investigated beginning in the 1980s. To mitigate the use of Co,

Fe-rich intermetallics in structure types such as ThMn<sub>12</sub> (e.g.,  $REFe_{11}Ti$ ), Th<sub>2</sub>Zn<sub>17</sub>, Th<sub>2</sub>Ni<sub>17</sub>, and CaCu<sub>5</sub> were studied.<sup>29,30</sup> However, their magnetic properties were often lacking in some important aspect, generally with low Curie temperatures and limited saturation magnetizations. For example, the  $RE_2Fe_{17}$  series has  $T_{CS}$  that are approximately 700–800°C lower than the analogous  $RE_2Co_{17}$  series.<sup>30</sup>

One strategy to circumvent these challenges is through intercalation. A breakthrough came in 1990, with the discovery that N intercalation into  $RE_2Fe_{17}$  increases the unit-cell volume by 6-7% and thus greatly improves its magnetic properties by strengthening Fe–Fe interactions (Figure 7).<sup>31</sup> The  $T_{\rm C}$ of Sm<sub>2</sub>Fe<sub>17</sub> increases from approximately 120 to 480°C; the  $M_s$ increases by 50% despite a lower magnetic ion fraction; and the magnetocrystalline anisotropy increases with a N content of approximately  $\text{Sm}_2\text{Fe}_{17}\text{N}_{2.7}$ .<sup>32,33</sup> While other intercalants like C and H similarly expand the lattice and improve properties,<sup>31,34, 35</sup> N produces the greatest expansion and improvement, with an intercalation level of Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> yielding the optimal magnetic properties.<sup>36</sup> Moreover, while Sm is a REE, its relative abundance, co-location with other REEs in ores, and lack of other technological uses lead to currently low commodity costs (cf. Figure 6). This sparked a flurry of research into Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> that continues to the present.<sup>37</sup> However, the major challenge facing Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> is thermal stability: Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> begins losing N at 600°C under N<sub>2</sub> atmosphere and 200°C under vacuum,<sup>38</sup> so while the material should be operationally stable in a drive motor, development of lowtemperature densification methods is necessary before sintered PMs can be fabricated.

## Fe<sub>16</sub>N<sub>2</sub>

A leading contender for REE-free PMs for EVs is a "- $Fe_{16}N_2$  (referred to here as  $Fe_{16}N_2$ ). It exhibits an







extremely high  $M_s$  of 2200 emu/cm<sup>3</sup>, which leads to a theoretical maximum  $(BH)_{max}$  of  $\mu_0 M_s^{2/4} \approx 130$  MGOe.<sup>39</sup> To date, the highest  $(BH)_{max}$  reported for Fe<sub>16</sub>N<sub>2</sub> is 20 MGOe, where this energy density is primarily limited by low  $H_c$ .<sup>10,40</sup> Notably, Fe<sub>16</sub>N<sub>2</sub> exhibits an excellent temperature coefficient with  $(BH)_{max}$  decreasing only slightly at elevated temperature (Figure 5b). Given its moderate magnetocrystalline anisotropy (1.8 MJ/m<sup>3</sup>), improvements to  $H_c$  should be possible. Importantly, Fe<sub>16</sub>N<sub>2</sub> faces no criticality challenges: Fe and N rank 1st and 3rd on the list of highest-volume global chemical production.<sup>41</sup> Fe<sub>16</sub>N<sub>2</sub> is currently undergoing commercialization.<sup>42</sup>

Although the large  $M_s$  of Fe<sub>16</sub>N<sub>2</sub> was initially discovered in the 1970s,<sup>43</sup> the slow development of this material stems from the difficulty of synthesizing it.<sup>39</sup> Fe<sub>16</sub>N<sub>2</sub> is deeply metastable and decomposes above 200°C, well below its estimated  $T_C$  (~380°C).<sup>10</sup> Additionally, achieving the necessary order on the N sublattice, which is required to realize the materials properties noted above, has proved exceedingly difficult. Synthetic approaches often rely on out-of-equilibrium processes to kinetically trap N in the solid, followed by low-temperature annealing to induce anion ordering.<sup>40,44,45</sup> Fe<sub>16</sub>N<sub>2</sub> can be made as both thin films and bulk powders.<sup>39</sup>

The powerful magnetism of  $Fe_{16}N_2$  comes from its unique structure. The range of  $M_s$  in literature far exceeds the value predicted by the Slater–Pauling curve, which relates the electron count of TM alloys to their magnetic moment (**Figure 8**a).  $Fe_{16}N_2$  adopts a tetragonal structure that can be described as  $Fe_8N$  with the interstitial, octahedrally coordinated N atoms in the body-centered-tetragonal (bct) Fe lattice arranged into an ordered supercell (Figure 8b). This leads to an overarching

structural motif of quasi-0D anion-metal polyhedra dispersed throughout a metal matrix. This motif can also be described as a partial N interstitial in a Cu<sub>3</sub>Au structure, which has recently been shown to yield high magnetic performance in Ni<sub>3</sub>MnN and Mn<sub>3</sub>IrN.<sup>46</sup>

The magnetic structure of  $Fe_{16}N_2$  is still under active debate. Two polarized neutron studies have concluded different models: an earlier study<sup>48</sup> concluded that crystallographic site Fe-4*d* (Figure 8b) has the largest moment, while a later study<sup>49</sup> concluded that site Fe-8*h* has the highest moment. Both measurements were plagued by experimental uncertainty, yet despite their disagreement, both reports concluded that there is a fundamental difference between Fe atoms bound in the [NFe<sub>6</sub>] cluster compared to Fe atoms outside the cluster. These discrepancies give rise to two contrasting possible mechanisms for the physics of Fe<sub>16</sub>N<sub>2</sub>, shown in Figure 8c–d. In one hypothesis, the N pulls electron density into the Fe of the octahedral cluster (Figure 8c); in the other, the N-centered octahedra push electron density out to the Fe-4*d* site (Figure 8d).

#### L1<sub>0</sub> FeNi

The mineral tetrataenite, also known as  $L1_0$  FeNi, is another REE-free PM contender, albeit less developed than  $Sm_2Fe_{17}N_3$  or  $Fe_{16}N_2$ . "L1<sub>0</sub>" denotes the CuAu structure type. L1<sub>0</sub> FeNi exhibits magnetic hardness that arises from the ordering of the metals into alternating sheets (**Figure 9**). In their disordered alloy, Fe and Ni randomly occupy sites on a face-centered-cubic (fcc) lattice (*Fm*-3*m*), resulting in a soft magnet. For the magnetically hard L1<sub>0</sub> structure, Fe and Ni layers alternate



along fcc (001), creating a concomitant tetragonal distortion (*P*4/*mmm*). The degree of metal ordering/tetragonality can be quantified via an order parameter *S*, where S=1 indicates fully ordered L1<sub>0</sub> FeNi and S=0 indicates fully disordered FeNi.<sup>50</sup> Experiments on thin films demonstrate that the anisotropy constant ( $K_u$ ) is proportional to *S*, as shown in Figure 9b.<sup>51</sup> Thinfilm experiments have achieved ordering as high as S=0.48,<sup>51</sup> while bulk methods reached S=0.71.<sup>50</sup> The naturally occurring tetrataenite found in meteorites likely has *S* near 0.5–0.6 based on magnetic anisotropy measurements<sup>52</sup> and Mossbauer spectroscopy.<sup>53</sup>

Unfortunately,  $L1_0$  FeNi is difficult to realize in the laboratory with high purity because solid-state diffusion is slow around the ordering temperature (ca. 320°C). The prevailing hypothesis for the natural formation of tetrataenite is that the astronomical timescales afforded by deep space asteroids with slow cooling rates (1–5°C per million years) allowed the atoms enough time to slowly diffuse into the ordered, thermodynamically stable  $L1_0$  FeNi phase.<sup>54</sup> On Earth, the initial discovery of  $L1_0$  FeNi used neutron bombardment to enhance diffusion near 320°C.<sup>55,56</sup> Recently, the simultaneous application of stress and an external magnetic field has shown promise for inducing order.<sup>53</sup>

Although  $L1_0$  FeNi has not yet been fabricated into PMs, the material should withstand the operating temperatures of drive motors. The magnetic properties of  $L1_0$  FeNi exhibit only small decreases with increasing temperature (Figure 5b).<sup>25</sup> And while the thermodynamic order–disorder transition is ~320°C,<sup>56</sup> differential scanning calorimetry shows tetrataenite is kinetically trapped up to  $530^{\circ}$ C.<sup>57</sup> These values are well above the maximum temperatures reached by EV drive motors (ca. 150–220°C). However, as with Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> and Fe<sub>16</sub>N<sub>2</sub>, synthesis and processing remain a challenge, as will be discussed in the "Perspective" section.

# Other emerging magnetic materials

Although there are numerous other emerging magnetic materials of great scientific interest, none are poised for incorporation into EVs soon. Other magnetic materials with the lowest supply risk (e.g., MnAl- and MnBi-based magnets) are about as powerful as Alnico magnets ((*BH*)<sub>max</sub> ~ 10 MGOe),<sup>22,58</sup> so seem unlikely to replace the current REE-based magnets in drive motor applications. Although more powerful magnets are found in this class of newer REE-free materials

(e.g.,  $Zr_2Co_{11}$ , HfCo<sub>5</sub>, Co<sub>3</sub>Si) with  $(BH)_{max}$  values on the order of 10–20 MGOe,<sup>22,59,60</sup> these materials face criticality challenges owing to their use of Co (or Hf).<sup>3</sup> Additionally, there are many other materials that are not suitable for PM applications themselves (owing to low overall magnetization) but which demonstrate design principles that may be useful for guiding further materials discovery efforts (e.g., Hf<sub>2</sub>FeIr<sub>5</sub>B<sub>2</sub>, Li<sub>2</sub>(Li<sub>1-x</sub>Fe<sub>x</sub>)N, and MnBi<sub>2</sub>). The ultimate goal is to match or exceed the performance of REE magnets with lower cost and less supply-constrained elements.

# Perspective

#### Design philosophy for disruptive magnetic materials

The emerging magnetic materials discussed in this article have been known for many decades. Next, we explore what limits these materials from commercialization and provide perspective on challenges for new magnetic materials discovery.

# Why have these emerging materials not yet been functionalized into commercially viable magnets?

Current commercialized high-performance PM materials rely on metallurgical processing techniques, which do not necessarily apply to these emerging materials. For example, the processing for Nd<sub>2</sub>Fe<sub>14</sub>B includes strategies such as rapidly quenching from melt, milling to control dispersion, and sintering to make fully dense magnets.9 In contrast, the most promising emerging materials previously discussed-Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>, Fe<sub>16</sub>N<sub>2</sub>, and L1<sub>0</sub> FeNi-require gentler processing, and the challenges to each are unique. While Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub> is stable at ambient conditions, it becomes metastable against N<sub>2</sub> loss at about 600°C, thus requiring altogether new sintering approaches to densify. Similarly, L1<sub>0</sub> FeNi is stable at ambient temperatures, but is impossible to make via metallurgical approaches because high-temperature processing results in Fe-Ni disorder. Fe<sub>16</sub>N<sub>2</sub> has both synthetic challenges (i.e., N<sub>2</sub> effusion and N vacancy order/disorder) but is made more difficult still due to its ambient condition metastability. And once synthesized, the stability of the material must be maintained in the operating environment of the PM (i.e., protected from air and excessive heat under drive-motor conditions). Novel "beyond metallurgy" techniques are being rapidly developed to overcome these challenges; eventually, they may be extended to other potential PM materials that have been historically underexplored due to their metastability and/or volatile anion chemistry.

# What chemical and physical features can we extract from the emerging magnetic materials, or other observations of desirable magnetic properties, to instill into new materials?

It is curious that two of the most promising magnetic materials are dilute nitrides given that the most common PM,  $Nd_2Fe_{14}B$ , contains dilute B. However, perhaps this is not surprising: Fe has  $a > d^5$  electron configuration, so the introduction of a more electronegative anion can reasonably increase the unpaired electron density on Fe (cf. Figure 8). Relative to boron, stronger/ more polarizing anions like nitrogen could also enable larger distortions from high-symmetry structures, providing an avenue to design uniaxial symmetry. On the other hand, too strong an anion leads to anion-rich materials with superexchange-mediated antiferromagnetic or ferrimagnetic configurations, as seen in ferrites. Convoluted with this electronic effect, anionic N is also larger than anionic B and C, increasing the unit-cell volume and improving magnetic properties, as observed in Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>. Thus, the observation that many emerging PMs are subnitrides might not be a coincidence at all-N could represent an ideal anion to promote ferromagnetism, motivating the discovery of new nitrides and materials with similar anion electronegativity (e.g., C, P, S, Cl, Br).

# How can we predict, in an efficient way, new materials that will have high magnetic performance?

Although several informatics-based papers have been published on the identification of potential PM materials,<sup>61–63</sup> the vast majority take the approach of down-selecting known phases. While there is some work on decorating known lattices with various chemical substitutions to predict new materials,<sup>64</sup> we are unaware of any works that extend the breadth of the search into new chemistries and structural prototypes



in a generalized, high-throughput way. While such approaches are rapidly being developed to predict the existence of new/ unknown anion-rich phases,<sup>65</sup> their underlying algorithms are based on ionic substitution so are likely unsuitable for PM candidates without formal ionic bonding. Thus, an open challenge to the materials informatics community is establishing a means to predict the stability, structure, and magnetic properties of *new* materials. In the absence of high-throughput computational frameworks, we posit a few design features based on our observations of emerging materials.

# Identifying compelling features for next-generation magnetic materials

We identify three design features we believe will be important for discovering new magnetic materials for high-performance PM applications (**Figure 10**). These features are: (a) 0D materials with isolated anion-centered polyhedra (inspired by  $Nd_2Fe_{14}B$ ,  $Fe_{16}N_2$ , and  $Sm_2Fe_{17}N_3$ ); (b) combining 3*d* elements (for high

 $M_{\rm s}$ ) with 4d and 5d elements (for high  $H_c$  from spin–orbit coupling); and (c) linear coordination environments for 3d metals. Our review of the literature suggests these features are underexplored and may yield powerful new PM materials.

First, 0D structural elements in Nd<sub>2</sub>Fe<sub>14</sub>B (B-centered bowties) and Fe<sub>16</sub>N<sub>2</sub> (N-centered octahedra) suggest that 0D anion-centered polyhedra may be an intriguing design feature. As described previously, neutron diffraction studies on Fe<sub>16</sub>N<sub>2</sub> present conflicting arguments for how the ordered N affect the charge distribution (and thus, the magnetism) compared to bcc Fe. Although the exact cause is uncertain, the result is strong ferromagnetism. A similar enhancement of  $M_s$  is seen in the conversion of Sm<sub>2</sub>Fe<sub>17</sub> to Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>. Future exploration of compounds with dilute anions may resolve this uncertainty. In doing so, new materials with quasi-0D motifs may be revealed to have powerful magnetism.

Second, the combination of 3*d* with 5*d* (or 4*d*) transition metals is a well-worn strategy for PM materials discovery, yet the space has not been explored comprehensively. Here, high  $M_s$  can come from 3*d* metals, and high spin–orbit coupling from 4*d* or 5*d* metals (which leads to high magnetocrystalline anisotropy and high  $H_c$ ). MnBi, HfCo<sub>7</sub>, and Zr<sub>2</sub>Co<sub>11</sub> are well-developed examples of this concept.<sup>58,60</sup> The recent discovery of MnBi<sub>2</sub> suggests there is further room for exploration in even simple binary phase spaces.<sup>66</sup> Work on multinary systems such as Hf<sub>2</sub>*M*Ir<sub>5</sub>B<sub>2</sub> (*M*=Mn, Fe) experimentally demonstrates the boost to magnetic anisotropy from heavy elements.<sup>67</sup> There are an enormous number of possible elemental combinations and structural configurations in this space, with a great deal yet to be explored. One area that appears ripe for systematic study is connecting the bond character of these systems to magnetic properties.

Finally, linear coordination environments may also enhance  $H_c$  via spin-orbit coupling. Li<sub>3x</sub>Fe<sub>x</sub>N highlights the impact of this structural feature on magnetic properties. Although too Fe-poor for PM applications, the linearly coordinated Fe exhibit high saturation magnetic moments  $(\mu^{\parallel} \sim 5\mu_{\rm B})$  and giant magnetocrystalline anisotropy with  $\mu_0 H_c = 11.6 \text{ T}.^{68}$  This arises because the linear coordination environment preserves spin-orbit coupling, which is otherwise quenched in 3d metals. Linearly coordinated motifs cannot undergo first-order Jahn-Teller distortions, which preserves the orbital angular momentum. Similar behavior is observed in organometallic compounds with linearly coordinated Fe.<sup>69</sup> Li<sub>3-x</sub>Fe<sub>x</sub>N in essence behaves as a collection of highly anisotropic single-ion magnets. Finding such geometries in phases with higher 3d metal density is an extremely promising path toward high performance REE-free PMs.

# **Summary and outlook**

The accelerating demand for EVs is increasing the need for new PM materials. Current magnet technologies are heavily dependent on metals with critical supply risks (e.g., Nd, Dy, Co). Scaling up the production of PM-based electric motors will require the development of new materials; Sm<sub>2</sub>Fe<sub>17</sub>N<sub>3</sub>, Fe<sub>16</sub>N<sub>2</sub>, and L1<sub>0</sub> FeNi are the current most promising candidates. These emerging materials exhibit high magnetic energy densities with the potential to compete with established technologies and are composed of less critical materials. Advances in materials processing beyond traditional metallurgical methods are needed to boost the coercivity of these emerging materials. Beyond these three candidates, we hypothesize that materials discovery efforts could further realize promising new magnetic materials. We propose several design concepts toward this goal: 0D motifs, combining 3d with 4d/5d transition metals, and using linearly coordinated transition metals to replace the magnetic anisotropy currently provided by rare earth elements. The need to develop and scale up new magnetic materials is urgent, but the opportunity for new discoveries is similarly great.

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#### **Author contributions**

Conceptualization: C.L.R. and S.R.B.; visualization: C.L.R. and S.R.B.; supervision: S.R.B.; writing-original draft: C.L.R., R.W.S., S.O., S.D., and S.R.B.; writing-review and editing: C.L.R., R.W.S., S.O., S.D., and S.R.B.

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# **Data availability**

No new data were generated for this article.

## **Conflict of interest**

Several of the authors (Smaha, O'Donnell, Bauers) declare a research collaboration with Niron Magnetics, Inc., a startup

company focused on commercializing  $Fe_{16}N_{2}$ , which may be perceived as a conflict of interest.

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