Transforming ENERGY

Understanding line losses and transformer losses in rural isolated distribution systems

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Photo by Dennis Schroeder, NREL 55200



1	Energy Systems	Integration	Facility
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2 Background on experimental capability

Background on system under study

4 Power system component modeling

5 Simulation results

6 Future work

Summary

Energy Systems Integration Facility

• The Energy Systems Integration Facility (ESIF) is a national User Facility located in Golden, Colorado on the campus of the National Renewable Energy Laboratory (NREL).



Controller and Power Hardware In The Loop (CHIL/PHIL)

 NREL's megawatt-scale controller and power hardware-in-the-loop (CHIL/PHIL) capability allows researchers and manufacturers to test energy technologies at full power in realtime grid simulations to safely evaluate performance and reliability.





Microgrids



Cosimulation

Power System Studies

Hardware-in-the-loop

Distributed

.....

Microgrid Controller

Generator

4 - 1

A) Pure simulation



B) <u>Controller-hardware-</u> in-the-loop

C) Controller-hardware-in-theloop and power-hardware-inthe-loop



D) Hardware only

Hardware-in-the-loop





Community Background

Background on Igiugig power system

- Igiugig, Alaska. Located South west of Anchorage.
- 12 kV system with peak loads approximately lower than 100 kW.
- Primarily supported by diesel generators.
- High diesel cost.



Background on Igiugig power system



2019 diesel fuel usage for electricity and heat, in total and by premise type

• Addressing losses in the power system can be crucial in saving diesel consumption.

Background on losses

- Well understood phenomenon.
- Primarily from lines, transformers (no load and on-load losses).
- Currently, a lack of information in open source to address this for the isolated microgrids, and small island power systems.
- We aim to address this by leveraging best modeling practices and using electromagnetic transient domain (EMT) simulation.

Network structure



- Radial in nature.
- Underground cable infrastructure to distribute power.
- Inductors used to compensate for reactive power contribution from underground cables.

Underground cables



- #2 AWG Aluminum, 15 kV, EPR insulation at 133%
- Conductor resistance 0.8715 Ω/km
- Cable Capacitance 0.157 μ F/km
- Positive sequence impedance 1.19 Ω/km
- Zero sequence impedance 2.5 Ω/km
- Zero sequence to positive sequence ratio – 2.1 (assumed)

Underground cables



- Conductor resistance 0.5518 Ω/km (calculated)
- Cable Capacitance 0.12 μF/km (assumed)
- Positive sequence impedance $0.56 \Omega/km$ (calculated)
- Zero sequence impedance 1.176 Ω/km (calculated)
- Zero sequence to positive sequence ratio – 2.1 (assumed)

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Stock Number	Code Word	Phase Cond. Size	DC Resistance @ 25°C	AC Resistance @ 90°C	Inductive Reactance @ 60Hz	GMR	Allowable Ampacity in Duct 90°C	Allowable Ampacity Directly Buried 90°C
		AWG/Kcmil	Ω/1000ft	Ω/1000ft	Ω/1000ft	ft	Amp	Amp
378182	Converse	2/0	0.1312	0.1682	0.0308	0.0121	150	150

Transformers



- Three large transformers
- Multiple distribution transformers
 - 15 kVA 2.2% impedance
 - 12.47 kV/7.2kV to 240V/120V

Transformers

	-					
~	General Maine V from					
	Transformer Name	Main Almr	TGen1			
	3 Phase Transformer MVA		0.2 [MVA]			
	Base Operation Frequency		60.0 [Hz]			
	Winding #1 Type		Y			
	Winding #2 Type		Y			
	Delta Lags or Leads Y		Lags			
	Positive Sequence Leakage	Reactance	0.035 [pu]			
	Ideal Transformer Model		No			
	Eddy Current Losses		0.02 [pu]			
	Copper Losses		0.03 [pu]			
	Tap Changer on Winding		None			
	Graphics Display		Single line (circles)			
	Display Details?		No			

General 1 phase	Xfmr				
Transformer MVA	0.005 [MVA]				
Base Operation Frequency	60.0 [Hz]				
Leakage Reactance	0.035 [pu]				
Eddy Current Core Loss	0.02 [pu]				
Copper Losses	0.03 [pu]				
Ideal Transformer Model	No				
Tap Changer on Winding	None				
Graphics Display	Windings				
Winding Voltages					
Winding #1 Voltage (RMS)	7.2 [kV]				
Winding #2 Voltage (RMS)	0.120 [kV]				

~	General 2 phase Vfmr					
	Transformer Name	5 phase Anni	TGen1			
	3 Phase Transformer MVA		0.02 [MVA]			
	Base Operation Frequency		60.0 [Hz]			
	Winding #1 Type		Delta			
	Winding #2 Type		Y			
	Delta Lags or Leads Y		Lags			
	Positive Sequence Leakage Re	actance	0.039 [pu]			
	Ideal Transformer Model		Yes			
	Eddy Current Losses		0.02 [pu]			
	Copper Losses		0.03 [pu]			
	Tap Changer on Winding		None			
	Graphics Display		Single line (circles)			
	Display Details?		No			

- No load losses are assumed to be 2%
- Copper losses are assumed to be 3%
- All single phase transformers are rated at 5 kVA
- Three phase transformers are rated at 20 kVA





Full load



Half load



10 percent load









Network loss summary

Scenario	Load		Generation		Losses (kW)
Scenario	Р	Q	Р	Q	
	(kW)	(kVAR)	(kW)	(kVAR)	
1 (Full load)	61	6	68.5	-29	7.5
2 (50% load)	30.5	3.05	39.5	-38.5	9
3 (10% load)	6.0	0.6	14.3	-44	8.1

- Loss values are as expected and primarily from transformers.
- Why is this important?
- How to compensate or reduce these loses?

Future work

: 20.004/div

Display Group





Acattole : Normal SUKS/s Ec/div

> Scope capture of the inverter dispatch change in gridconnected operation showing the (top) current, (middle) the amplifier voltage, and (bottom) inverter voltage.

> Scope capture of the load step change in islanded operation showing the (top) current, (middle) the amplifier voltage, and (bottom) inverter voltage.

Summary

- Losses in distribution system are not new. Well known and well studied.
- But, they are still a key challenge for isolated microgrid systems and island power systems.
- Understanding line losses and addressing line losses are critical for communities that are primarily using diesel generators.
- This work aims to support community efforts to address losses in the system.
- We are recommending building key EMT models to answer loss related questions and pave way for future grid integration questions.



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Thank you

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NREL/PR-5D00-89699

This work was authored by the National Renewable Energy Laboratory, operated by Alliance for Sustainable Energy, LLC, for the U.S. Department of Energy (DOE) under Contract No. DE-AC36-08GO28308. Funding provided by DOE Office of Energy Efficiency and Renewable Energy Energy Transitions Initiative, Building Technologies Office, Geothermal Technologies Office, Solar Energy Technologies Office, Vehicle Technologies Office, Water Power Technologies Office, and Wind Energy Technologies Office. The views expressed in the article do not necessarily represent the views of the DOE or the U.S. Government. The U.S. Government retains and the publisher, by accepting the article for publication, acknowledges that the U.S. Government retains a nonexclusive, paidup, irrevocable, worldwide license to publish or reproduce the published form of this work, or allow others to do so, for

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