

Towards Advanced Robotics for Wind Blade Manufacturing

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National Renewable Energy Laboratory
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Presentation Overview

1 Economics of Automated Finishing

2 Tool Design

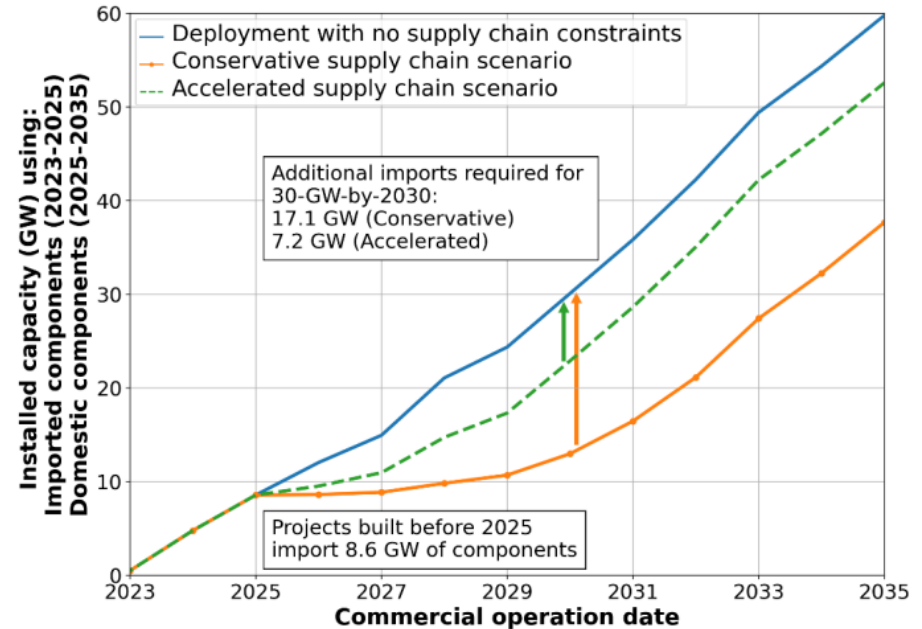
3 Toolpath Generation

4 Real-Time Control for Automated Finishing

5 Factory Mobility

Offshore wind deployments depend on domestic manufacturing

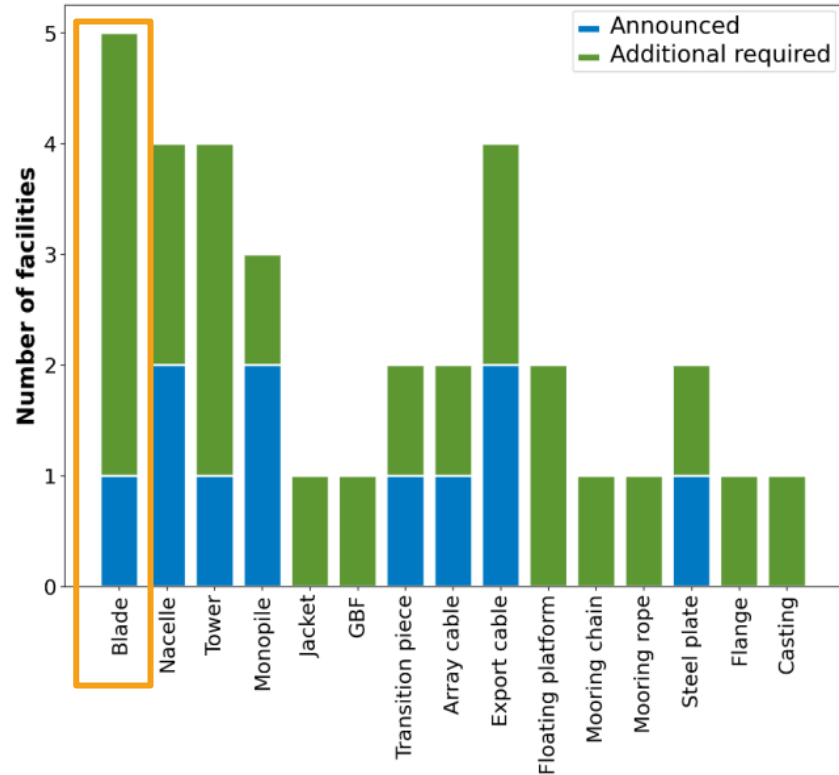
- To meet 30 gigawatts (GW) by 2030 requires a scenario with no supply chain constraints



Plot from Shields (2023)

Offshore wind deployments depend on domestic manufacturing

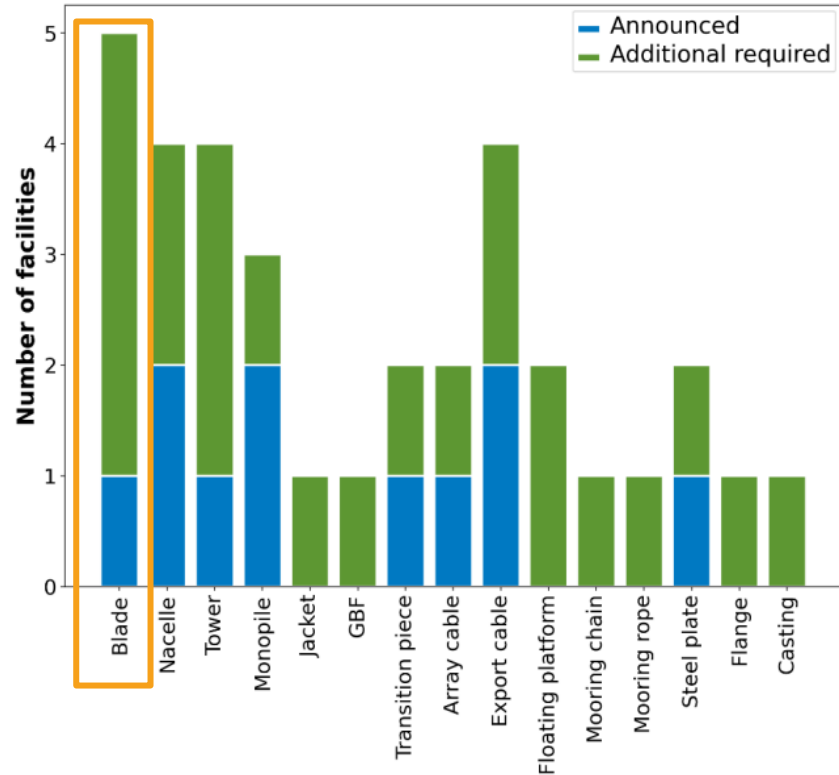
- To meet 30 gigawatts (GW) by 2030 requires a scenario with no supply chain constraints
- This requires five new blade manufacturing facilities to be developed, each producing 225 blades per year



Plot from Shields (2023)

Offshore wind deployments depend on domestic manufacturing

- To meet 30 gigawatts (GW) by 2030 requires a scenario with no supply chain constraints
- This requires five new blade manufacturing facilities to be developed, each producing 225 blades per year
- However, this considers only automation to have an impact in the long term.



Plot from Shields (2023)

Current breakdown of SNL 100-03 wind turbine blade manufacturing

- Premold steps are difficult to automate
- Automation has a lower material deposition rate
- Automated soft-fabric manipulation has a low technology readiness level.

Operation	Labor [hour]	Skin Mold Gating CT [hour]	Nongating CT [hour]
Material cutting	136.10	[-]	47.57
Root preform lp	16.64	[-]	10.42
Root preform hp	16.64	[-]	10.42
Infusion shear web number 1	155.97	[-]	19.27
Infusion shear web number 2	152.32	[-]	18.91
Infusion shear web number 3	69.18	[-]	10.12
Infusion shear web number 4	24.48	[-]	5.45
Infusion spar cap lp	152.87	[-]	19.51
Infusion spar cap hp	152.87	[-]	19.51
Lp skin	484.73	14.76	[-]
Hp skin	478.77	[-]	14.76
Assembly	443.55	6.33	[-]
Demolding	9.23	2.92	[-]
Trim	23.00	[-]	4.33
Overlay	86.99	[-]	9.91
Postcure	2.17	[-]	9.84
Root cut and drill	14.65	[-]	6.99
Root hardware installation	10.63	[-]	4.98
Surface preparation	145.22	[-]	18.28
Painting	30.82	[-]	7.79
Surface finishing	29.31	[-]	9.83
Weight balance	7.16	[-]	3.25
Final inspection	4.91	[-]	2.04
Shipping preparation	6.21	[-]	2.75
Total	2,654.46	24.00	255.93

Table from Bortolotti (2019)

Current breakdown of SNL 100-03 wind turbine blade manufacturing

- Postmold operations have a much higher technology readiness level and thus make an impact in the short- and mid-term
- Automation can have a huge impact on eliminating supply chain constraints.

Operation	Labor [hour]	Skin Mold Gating CT [hour]	Nongating CT [hour]
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Root preform lp	16.64	[-]	10.42
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Current breakdown of SNL 100-03 wind turbine blade manufacturing

- Trimming removes excess flashing material
 - Uses a cutting tool to remove the bulk of material
 - Grinds the remaining material to produce an aerodynamic shape

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- Surface preparation is done before painting and adding protective coating.

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- Automated finishing can
 - Increase quality
 - Reduce cycle time
 - Increase throughput

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- Automated finishing can
 - Increase quality
 - Reduce cycle time
 - Increase throughput
- However, to make automated wind turbine blade finishing economically viable:
 - Keep capital costs low
 - Be able to adapt to new blade designs
 - Dramatically reduce cycle time.

Our techno-economic model shows that an ~62% reduction in finishing time is needed

- If capital costs are spread over 3 years, an ~60% reduction in finishing costs per blade is achieved

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- Using the SNL 100-03 reference blade (Bortolotti 2019):
 - 10 meters (m) per hour (hr) per worker for 6 workers = 1 m per minute (min)
 - Automated trimming speed of 1.62 m/min

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 - 10 meters (m) per hour (hr) per worker for 6 workers = 1 m per minute (min)
 - Automated trimming speed of 1.62 m/min
 - 6 m²/worker/hr for 8 workers = .8 m²/min
 - Automated sanding speed of 1.296 m²/min.

Tool Design for Automated Wind Turbine Blade Finishing

Phase 1

Robots can use more aggressive tooling

- Robots can carry heavy payloads, produce high forces, and move quickly
- KUKA KR300 R2500 Ultra (2021), with a linear track, has the following features:
 - 2.5-m reach, 300-kilogram (kg) payload, 6.6-m track
 - Can reach up to 2.5 m per second (s).

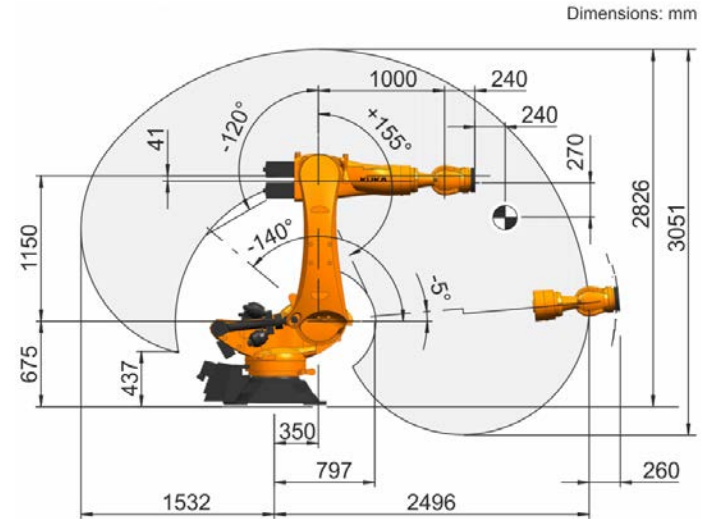


Photo from KUKA KR300 R2500

Trimming tool selection

- Band saw modified for cutting the bulk of flashing material from the wind turbine blade



Photo by Hunter Huth, NREL

Trimming tool selection

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- Diamond band-saw blades provide superior longevity



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Trimming tool selection

- Band saw modified for cutting the bulk of flashing material from the wind turbine blade
- Diamond band-saw blades provide superior longevity
- Much faster trimming speeds compared to hand-held tools
- Equipped with rpm and motor load sensors to adjust speed based on resistance.



Photo by Hunter Huth, NREL

Grinding tool selection

- PushCorp (2020) AFD1240 active compliance device with STC1515 spindle



Photo by Hunter Huth, NREL

Grinding tool selection

- PushCorp (2020) AFD1240 active compliance device with STC1515 spindle
- Custom dust collection shroud



Photo by Hunter Huth, NREL

Grinding tool selection

- PushCorp (2020) AFD1240 active compliance device with STC1515 spindle
- Custom dust collection shroud
- Flapped sanding wheels for more abrasive longevity



Photo by Hunter Huth, NREL

Grinding tool selection

- PushCorp (2020) AFD1240 active compliance device with STC1515 spindle
- Custom dust collection shroud
- Flapped sanding wheels for longevity
- Allows precise force control to consistently remove the desired amount of material.



Photo by Hunter Huth, NREL

Sanding tool selection

- Tyrolit (2024) drum sander on the PushCorp active compliance device



Photo by Hunter Huth, NREL

Sanding tool selection

- Tyrolit (2024) drum sander on the PushCorp active compliance device
- Allows application of consistent force with constantly changing orientation



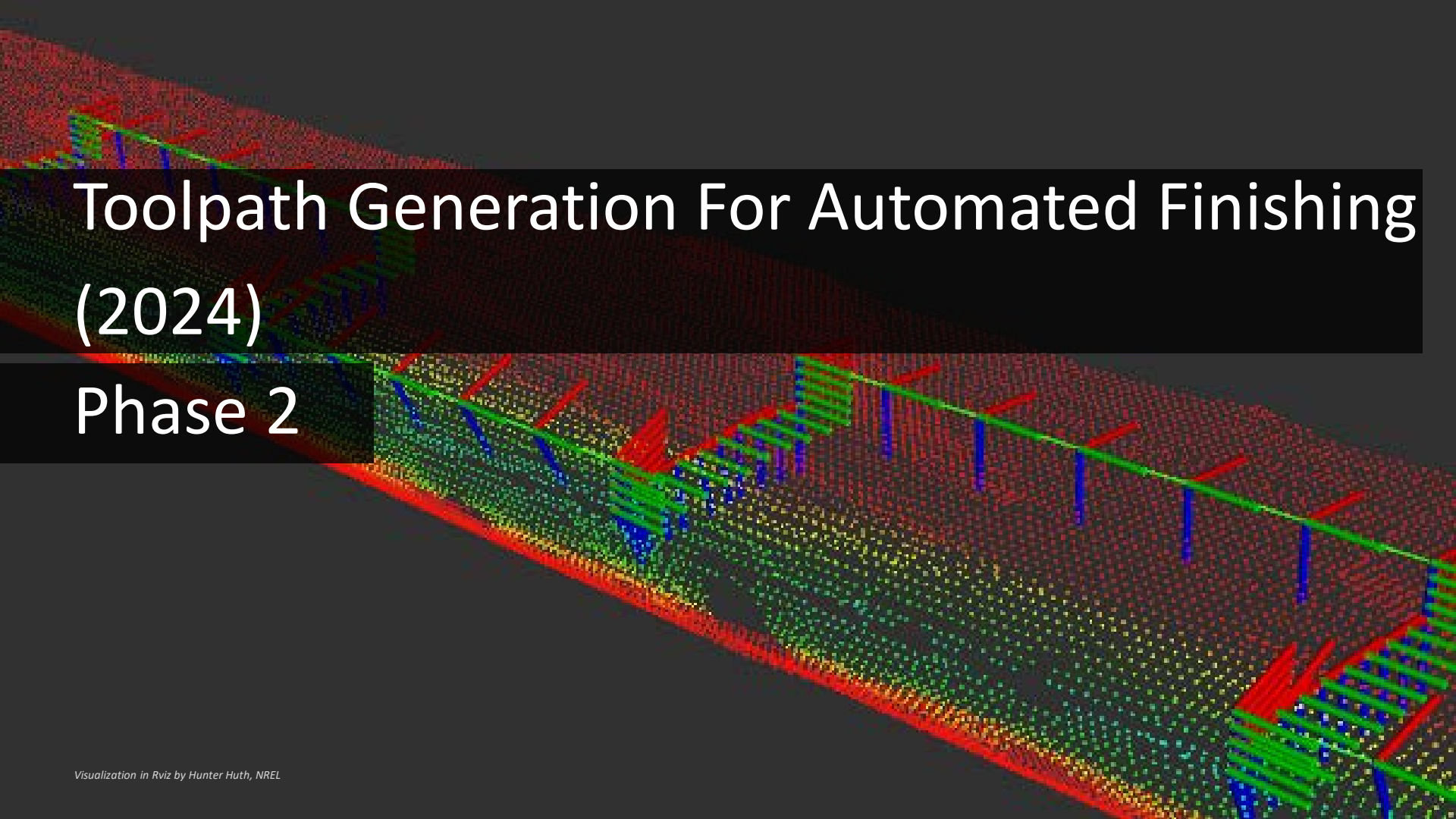
Photo by Hunter Huth, NREL

Sanding tool selection

- Tyrolit (2024) drum sander on the PushCorp active compliance device
- Allows application of consistent force with constantly changing orientation
- Drum sanders do not trap dust under the abrasive, resulting in more efficient use.



Photo by Hunter Huth, NREL

A 3D visualization of a curved surface, possibly a turbine blade, with a dense grid of points. Overlaid on this grid are several colored lines representing toolpaths: red, green, and blue. The lines are arranged in a series of parallel, slightly curved paths across the surface. The background is dark, making the colored lines and points stand out.

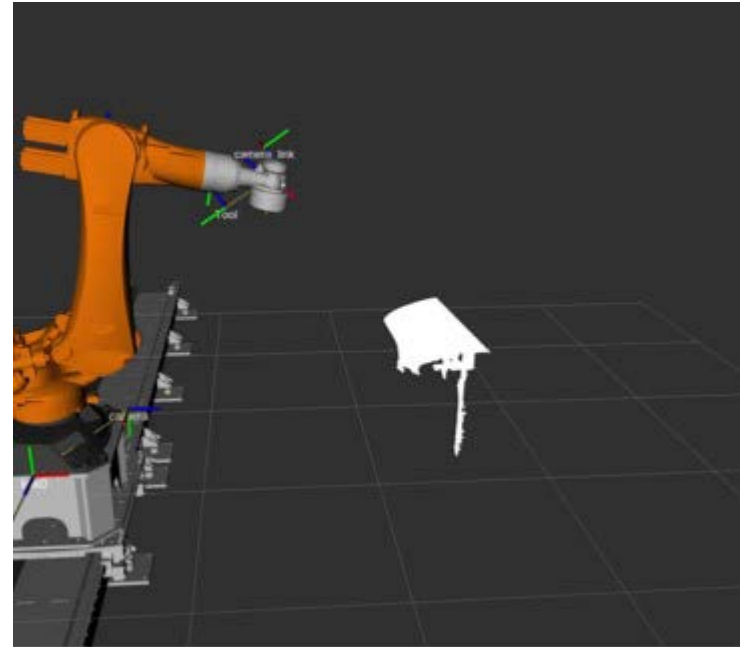
Toolpath Generation For Automated Finishing (2024)

Phase 2

Capturing blade geometry is a two-step process

- A global scan captures 3D point cloud data of the entire scene
- Blade position is determined by scene segmentation
- A local scan of the leading/trailing edge at the optimal distance for the Zivid 2 camera (2023) is performed.

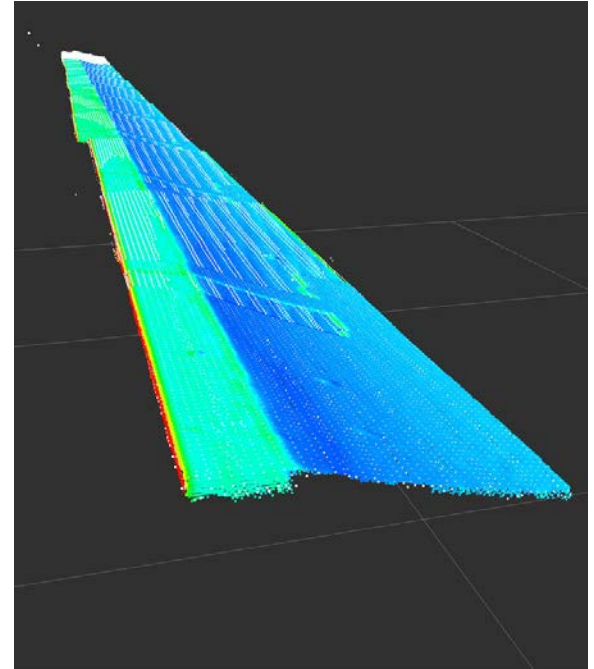
4x speed



Screen record of Rviz by Hunter Huth, NREL

First step is to identify important geometry on the wind turbine blade

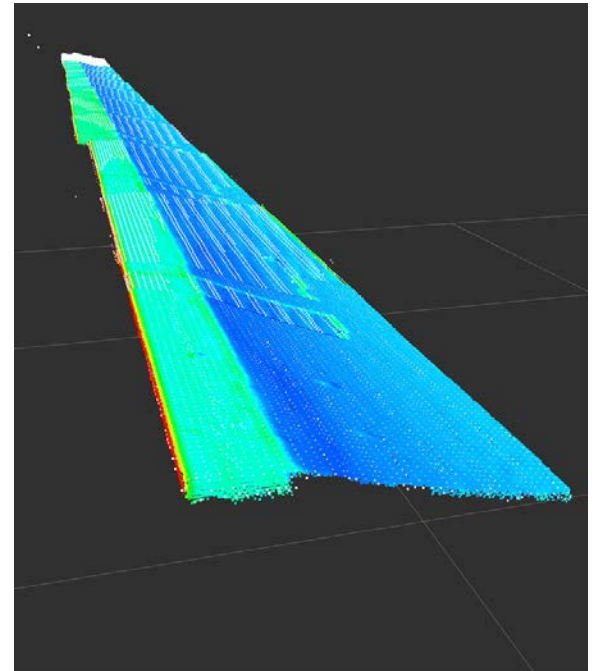
- A moving least squares implemented through the point cloud library (Rusu, 2011) is used to fit a smooth surface to the blade



Screen capture of Rviz by Hunter Huth, NREL

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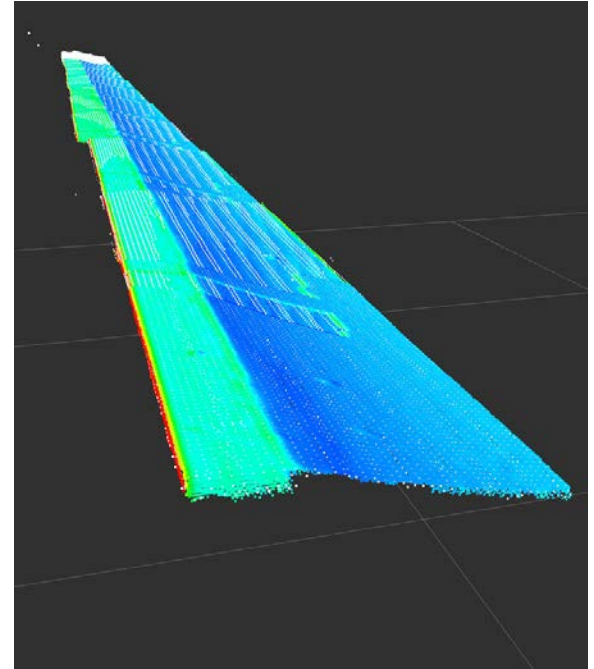
- A moving least squares implemented through the point cloud library (Rusu 2011) is used to fit a smooth surface to the blade
- The cloud is sliced in the spanwise direction



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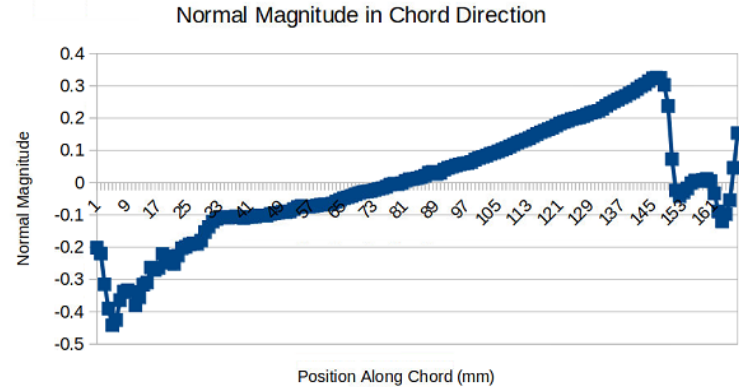
- A moving least squares implemented through the point cloud library (PCL 2011) is used to fit a smooth surface to the blade
- The cloud is sliced in the spanwise direction
- Normal vectors in the chordwise direction are calculated and analyzed to find large changes in the normal at the leading edge/flashing boundary.



Screen capture of Rviz by Hunter Huth, NREL

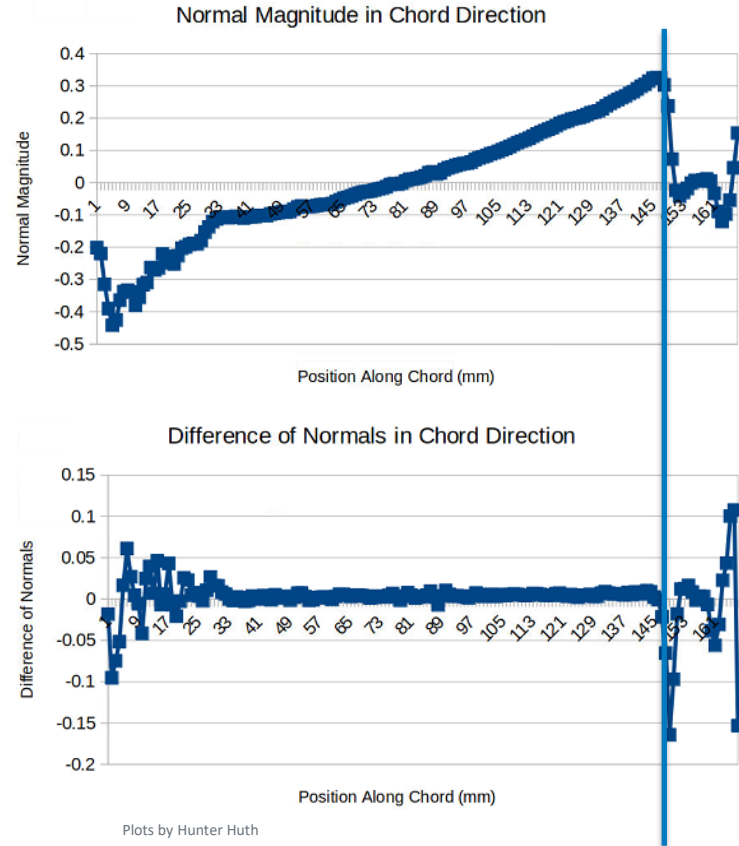
Trimming toolpath generation

- Normal components in chordwise direction are calculated along the chord shown in the top plot



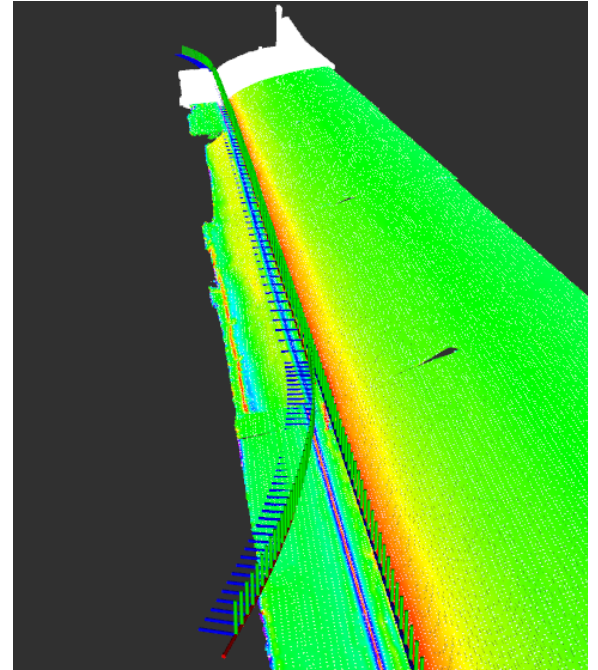
Trimming toolpath generation

- Normal components in chordwise direction are calculated along the chord shown in the top plot
- Difference between adjacent normal vector magnitudes is calculated along the chord shown in the bottom plot
 - Analogous to first derivative
- Flashing begins at the horizontal line, discovered by reducing high-frequency noise and finding the absolute maximum.



Trimming toolpath calculated from the leading/trailing edge

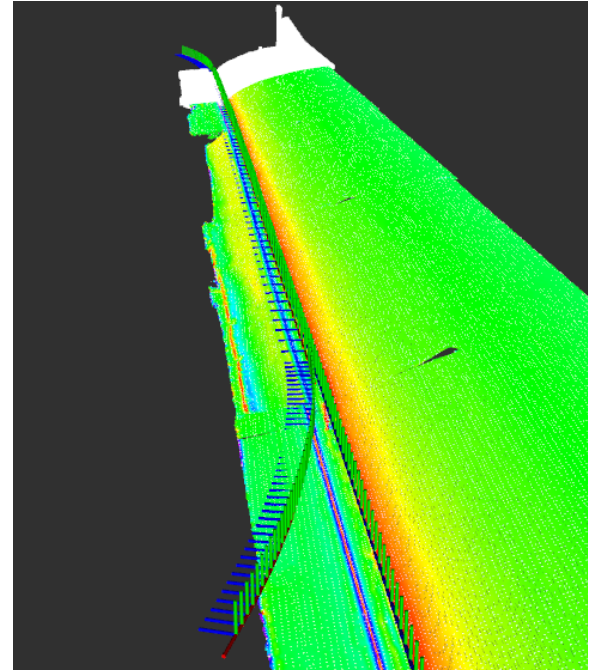
- An offset is added to prevent damage to the blade



Screen capture of Rviz by Hunter Huth, NREL

Trimming toolpath calculated from the leading/trailing edge

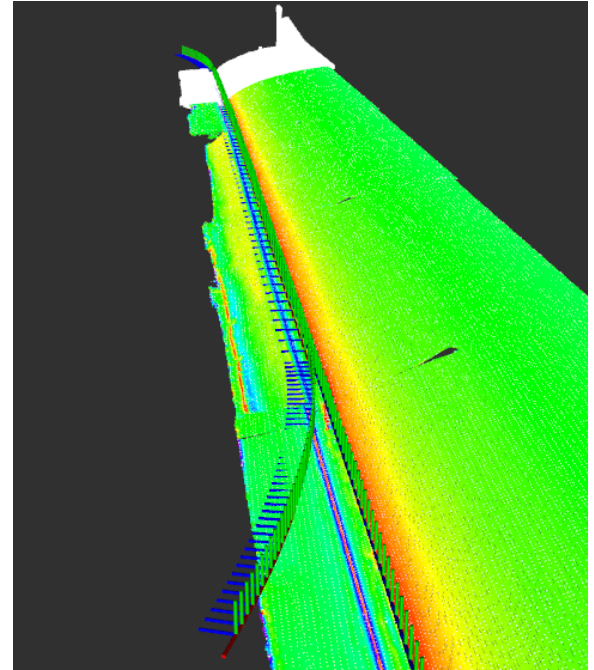
- An offset is added to prevent damage to the blade
- Lead-ins and lead-outs are added every 2.5 meters to separate hanging flashings



Screen capture of Rviz by Hunter Huth, NREL

Trimming toolpath calculated from the leading/trailing edge

- An offset is added to prevent damage to the blade
- Lead-ins and lead-outs are added every 2.5 meters to separate hanging flashings
- This toolpath is passed as a spline trajectory to the robot controller.



Screen capture of Rviz by Hunter Huth, NREL

Trimming execution

Leading Edge—4× speed

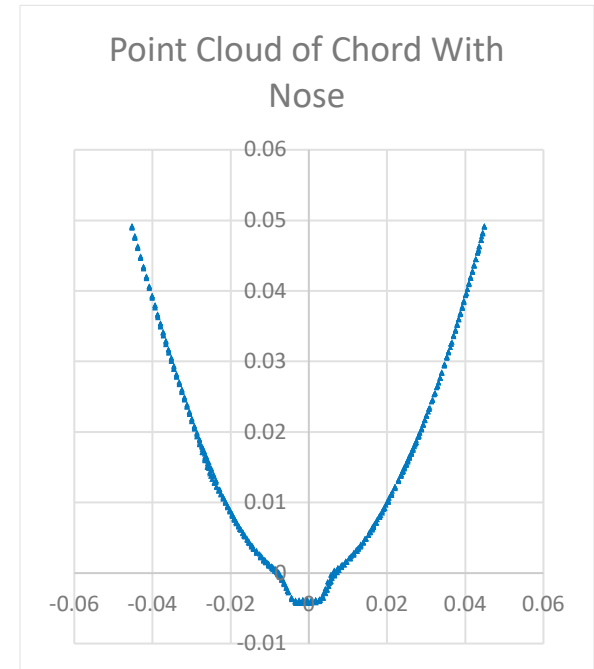


Trailing Edge—4× speed



Identifying leftover nose material after trimming from point cloud

- Slice leading-edge area into 2D cross sections



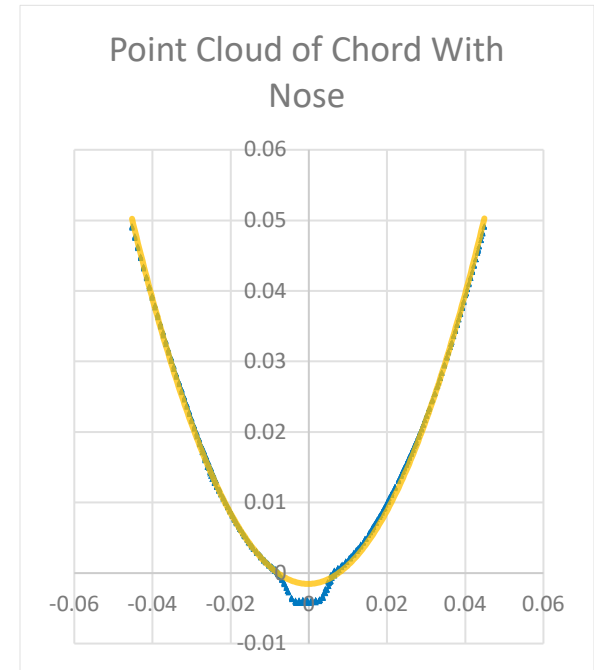
▲ Raw point cloud data

▲ Identified nose

— Parabolic fit

Identifying leftover nose material after trimming from point cloud

- Slice leading-edge area into 2D cross sections
- Fit a parabola along the leading-edge chord



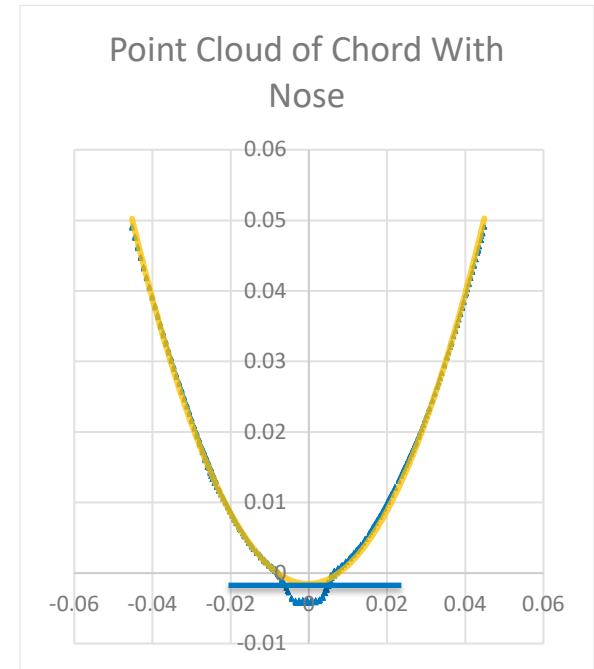
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Identifying leftover nose material after trimming from point cloud

- Slice leading-edge area into 2D cross sections
- Fit a parabola along the leading-edge chord
- Use parabola minimum as leading edge



▲ Raw point cloud data

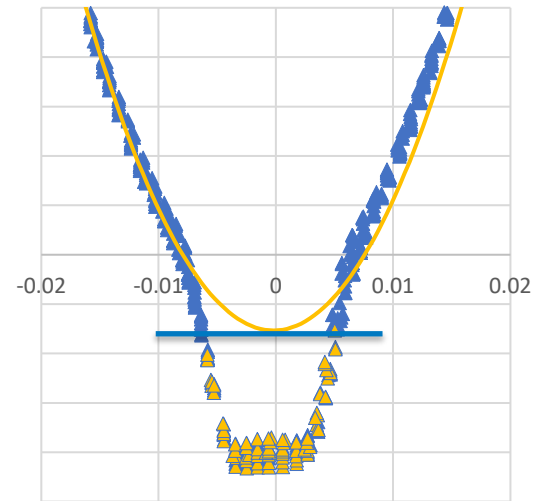
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Identifying leftover nose material after trimming from point cloud

- Slice leading-edge area into 2D cross sections
- Fit a parabola along the leading-edge chord
- Use parabola minimum as leading edge
- Extract nose points below parabola minimum

Point Cloud of Chord with Nose

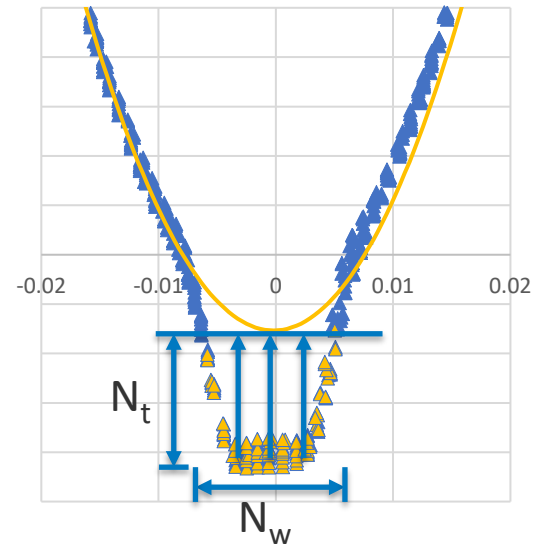


- ▲ Raw point cloud data
- ▲ Identified nose
- Parabolic fit

Identifying leftover nose material after trimming from point cloud

- Slice leading-edge area into 2D cross sections
- Fit a parabola along the leading-edge chord
- Use parabola minimum as leading edge
- Extract nose points below parabola minimum
- Nose thickness (N_t) is the average y-distance to the leading edge
- Nose width (N_w) is the range of nose points in the x-direction.

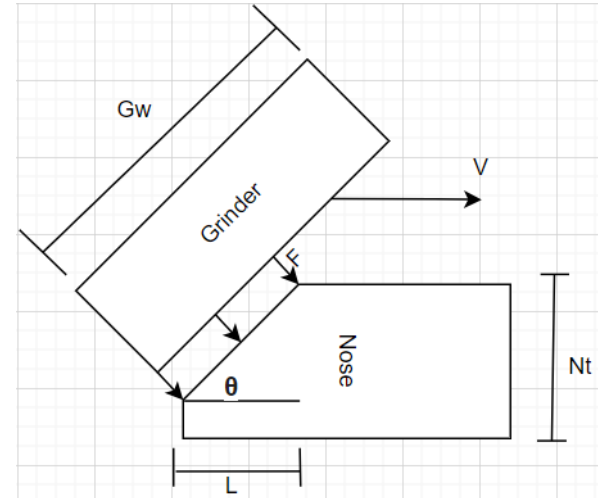
Point Cloud of Chord with Nose



- ▲ Raw point cloud data
- ▲ Identified nose
- Parabolic fit

Grinding model for calculating travel velocity

- Model determines linear travel speed necessary to grind to a certain depth
- On first contact, pressure is high, so grinding depth increases
- Pressure decreases as grinder plunges into material until a steady-state depth is reached.



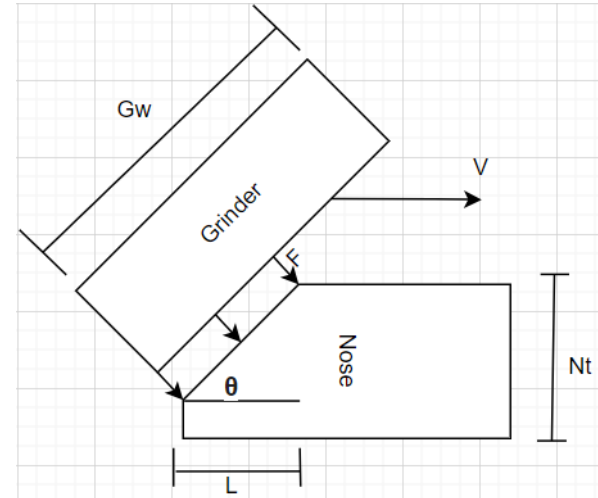
G_w = grinder width N_t = nose thickness
 F = force N_w = nose width
 V = linear velocity t = grind time
 θ = grinding angle μ = removal
 L = contact length constant

Grinding model for calculating travel velocity

$$L = \frac{N_t}{\tan(\theta)},$$

$$t = \frac{L}{V} = \frac{N_t}{R} = \frac{N_t}{\tan(\theta) * V}$$

Time each slice is in contact with grinder



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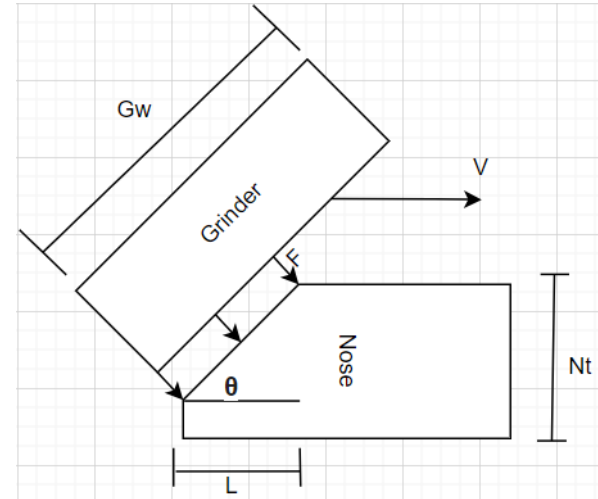
$$V = \frac{R}{\tan(\theta)},$$

Rate at which material is removed

$$R = \frac{F}{A} * \mu,$$

$$A = N_w * N_t * \sin(\theta)$$

Contact area of grinder and nose



G_w = grinder width N_t = nose thickness

F = force N_w = nose width

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Rate at which material is removed

$$R = \frac{F}{A} * \mu,$$

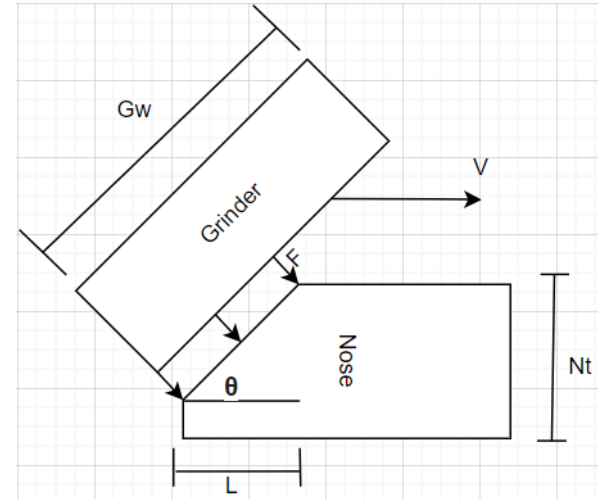
$$A = N_w * N_t * \sin(\theta)$$

Contact area of grinder and nose

$$V = \frac{F * \mu * \cos(\theta)}{N_w * N_t}$$

μ characterizes relationship between pressure and removal rate

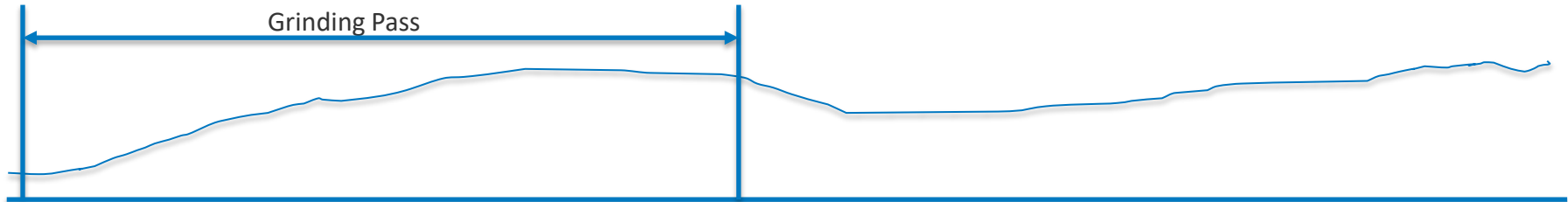
Linear velocity to remove nose given a grinding angle, force, nose size, and removal constant



G_w = grinder width N_t = nose thickness
 F = force N_w = nose width
 V = linear velocity t = grind time
 θ = grinding angle μ = removal constant
 L = contact length

Grinding toolpath executed in multiple passes

- Maximum material removed per pass is 2 millimeters (mm)
- The pass length is optimized for longer passes to get a smooth finish.



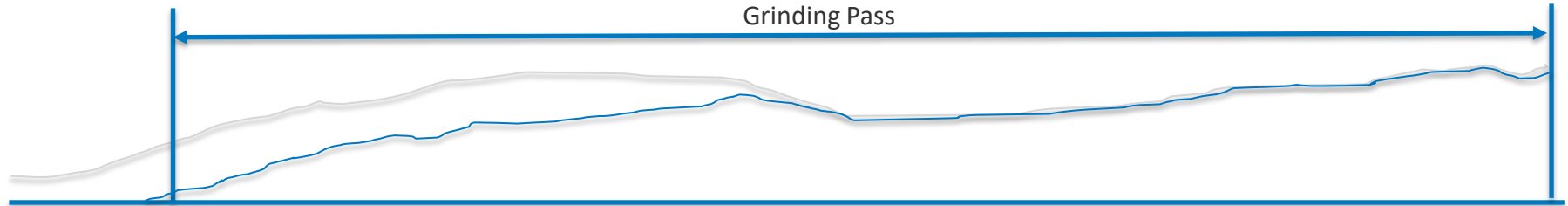
N_t	2	4	6	7	8	7	5	5	7	8	9
Pass 1	0	2	4	5	6	6	5	5	7	8	9
Pass 2											
Pass 3											

Small N_t has only 1 mm removed

End grinding pass because N_t is smaller than previous max N_t

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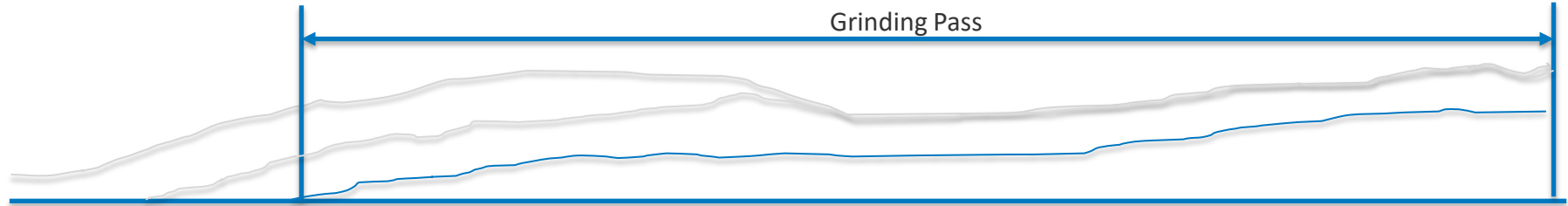


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Pass 1	0	2	4	5	6	6	5	5	7	8	9
Pass 2	0	0	2	3	4	4	4	4	5	6	7
Pass 3											

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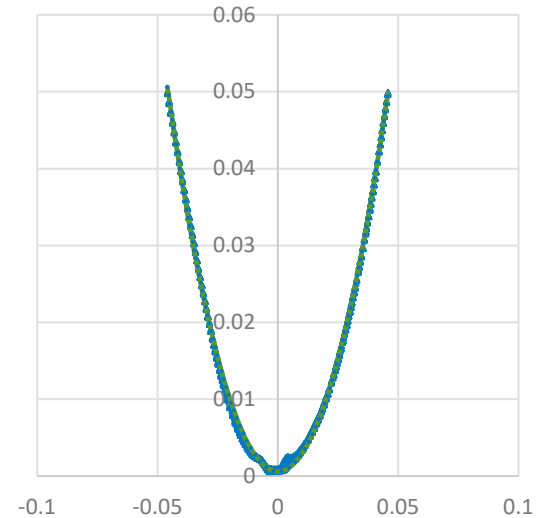


N_t	2	4	6	7	8	7	5	5	7	8	9
Pass 1	0	2	4	5	6	6	5	5	7	8	9
Pass 2	0	0	2	3	4	4	4	4	5	6	7
Pass 3	0	0	0	1	2	2	2	2	3	4	5

Leading- and trailing-edge detection for sanding toolpath

- Leading edge is detected through same algorithm as in the grinding process

Chord for Leading-Edge Detection



Plot by Hunter Huth

Leading- and trailing-edge detection for sanding toolpath

- Leading edge is detected through same algorithm as in the grinding process
- Trailing edge for sanding is detected with the same algorithm as for trailing-edge trimming
 - Needs scans above and below trailing edge
 - Large change in normal at trailing edge.

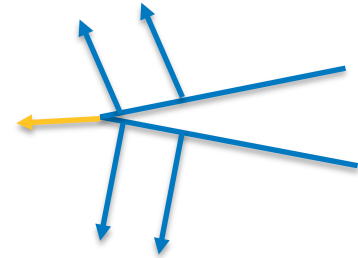
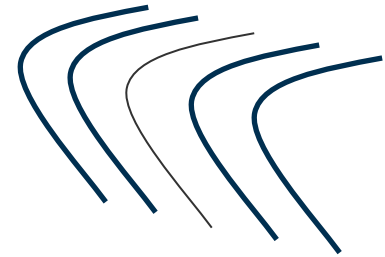


Image by Hunter Huth

Leading-edge sanding toolpath generation

- Separate leading-edge chords into sections that match width of sanding drum



Drawing created by Hunter Huth, NREL

Leading-edge sanding toolpath generation

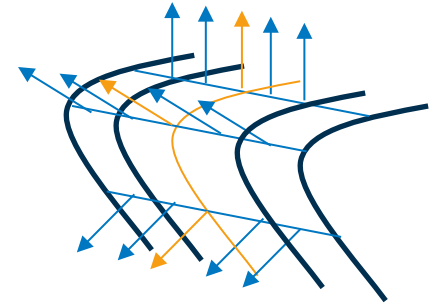
- Separate leading-edge chords into sections that match width of sanding drum
- Toolpath position follows the middle of the chord



Drawing created by Hunter Huth, NREL

Leading-edge sanding toolpath generation

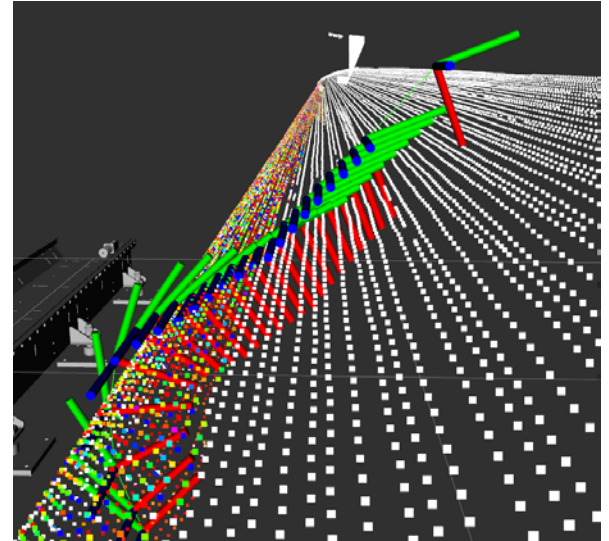
- Separate leading-edge chords into sections that match width of sanding drum
- Toolpath position follows the middle of the chord
- Toolpath orientation is the average orientation along the chords



Drawing created by Hunter Huth, NREL

Leading-edge sanding toolpath generation

- Separate leading-edge chords into sections that match width of sanding drum
- Toolpath position follows the middle of the chord
- Toolpath orientation is the average orientation along the chords
- Add lead-in/lead-outs for a soft touch with the sander



Screen capture of Rviz by Hunter Huth, NREL

Trailing-edge sanding toolpath generation

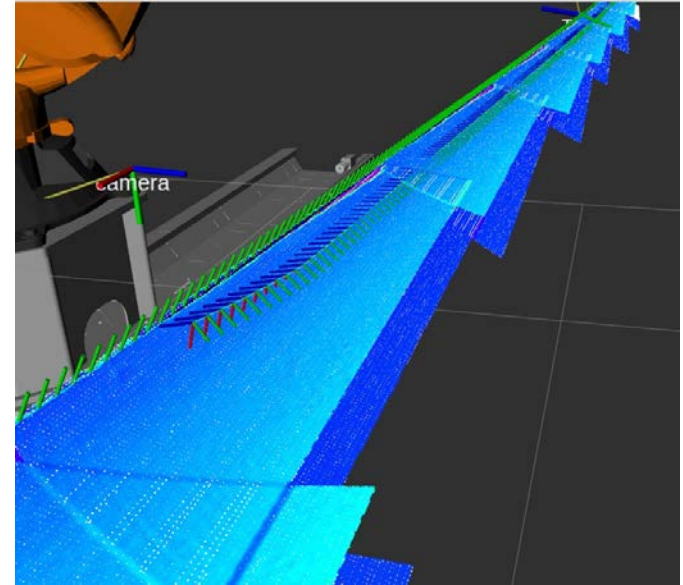
- Trailing-edge sanding toolpath follows the spanwise direction
- Sander angle relative to the trailing edge is calculated to sand to the desired chord depth and optimize abrasive usage



Photo by Hunter Huth, NREL

Trailing-edge sanding toolpath generation

- Trailing-edge sanding toolpath follows the spanwise direction
- Sander angle relative to the trailing edge is calculated to sand to the desired chord depth and optimize abrasive usage
- Sander orientation is determined by the average normal orientation under the sanding drum.



Screen capture of Rviz by Hunter Huth, NREL

Sanding execution

Leading Edge—4× speed



Trailing Edge—4× speed



Automated finishing results

- Trimming accuracy of $-4.5/+0.7$ mm and $-3.1/+3.6$ mm for leading and trailing edge, respectively

	Operational Speed (m/min)	
	Leading Edge	Trailing Edge
Trim	0.96	1.09
Grind	0.63	N/A
Sand	0.79	0.81

Automated finishing results

- Trimming accuracy of $-4.5/+0.7$ mm and $-3.1/+3.6$ mm for leading and trailing edge, respectively
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 - Real-time feedback required to update the grinding model
- Sanding offered full and even coverage of the surface.

	Operational Speed (m/min)	
	Leading Edge	Trailing Edge
Trim	0.96	1.09
Grind	0.63	N/A
Sand	0.79	0.81



Real-Time Control

Phase 3

Real-time control to optimize for speed and accuracy

- Previous phase focused on how to use captured blade geometry to plan toolpaths

Collect 3D data of blade geometry



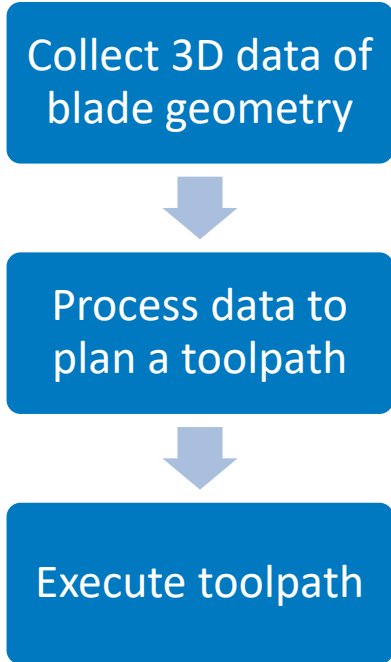
Process data to plan a toolpath



Execute toolpath

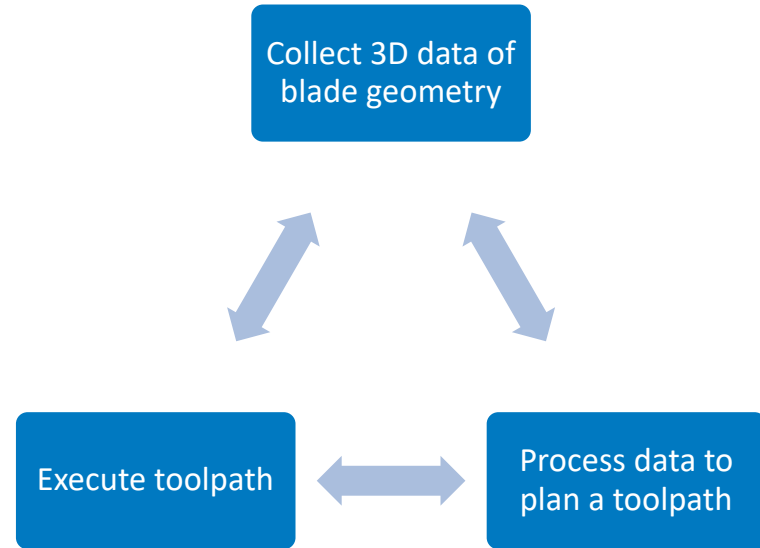
Real-time control to optimize for speed and accuracy

- Previous phase focused on how to use captured blade geometry to plan toolpaths
- Sequentially captured data, planned a toolpath, and executed the toolpath
 - Inefficient in terms of cycle time



Real-time control to optimize for speed and accuracy

- Previous phase focused on how to use captured blade geometry to plan toolpaths
- Sequentially captured data, planned a toolpath, and executed the toolpath
 - Inefficient in terms of cycle time
- Next phase will scan, plan, and execute in parallel
 - Substantial reduction in cycle time
 - Limited by tool operation speed
 - Real-time feedback to improve finish quality.



Real-time control of an industrial robot

- Kuka has a real-time interface that allows streaming of joint commands every 4 milliseconds (ms)
 - Allows finite control of joints to improve accuracy

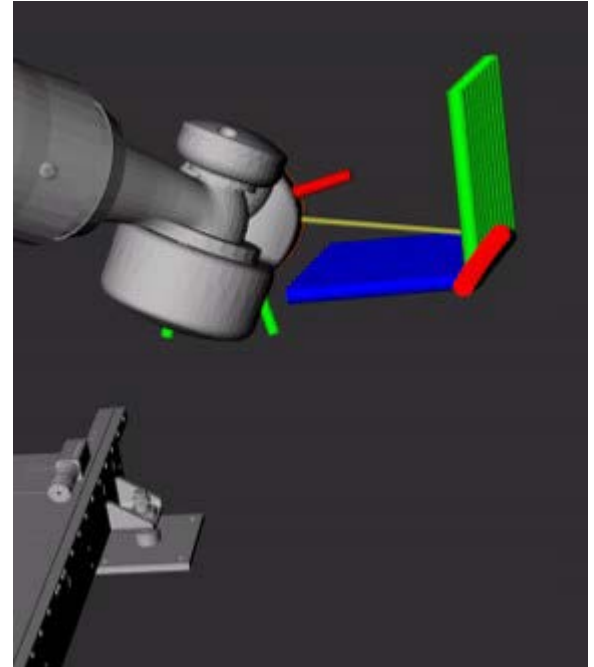


Image by Hunter Huth, NREL

Real-time control of an industrial robot

- Kuka has a real-time interface that allows streaming of joint commands every 4 milliseconds (ms)
 - Allows finite control of joints to improve accuracy
- Trajectory will be planned from Robot Operating System (ROS) 2 (Macenski, 2022)
 - Real-time improvements from ROS that leverage a real-time kernel.

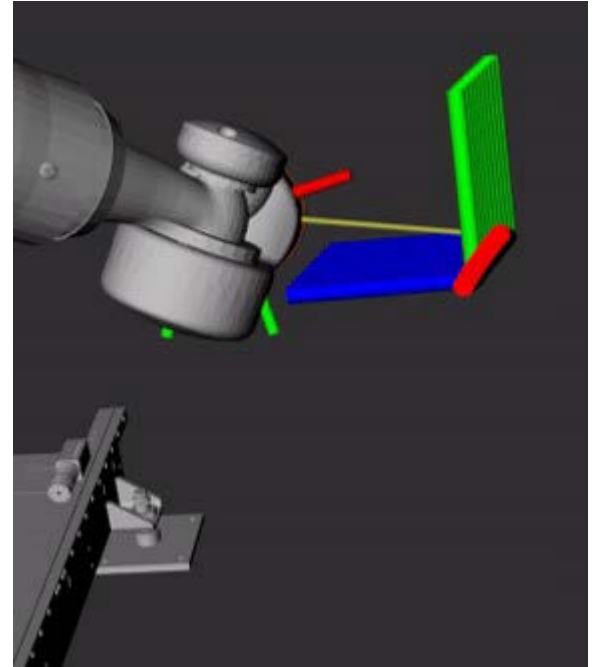


Image by Hunter Huth, NREL

Capture data with a 3D laser line profiler

- Capture real-time scans in the chordwise direction
 - Faster processing of chords
 - Capture and process data while performing the operation
- Real-time quality feedback to ensure the correct aerodynamic shape is being produced.

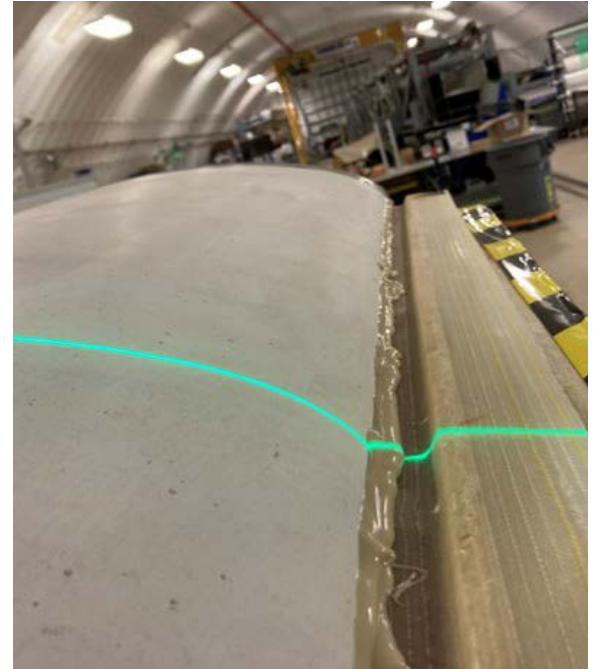
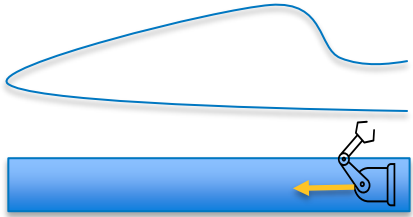


Photo by Casey Nichols, NREL

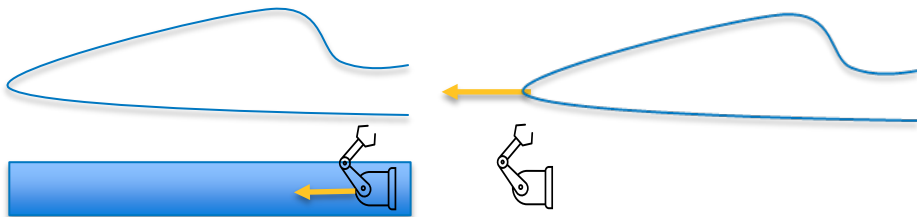
How does this robot reach the entire surface?



Full-Length Track With Stationary Blade

- +Requires less factory space
- +Simple concept
- High track cost
- Less flexibility

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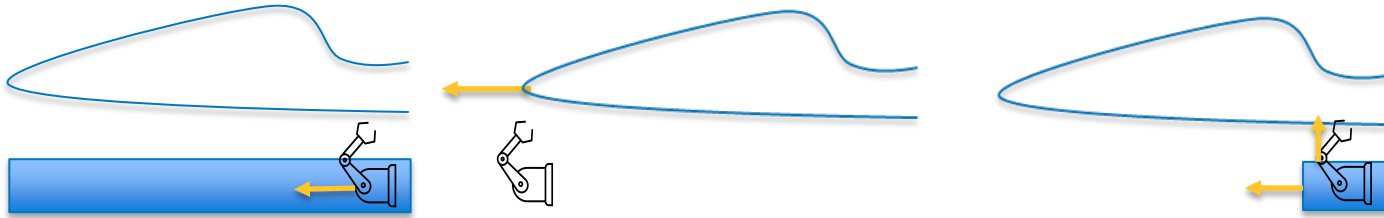
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Mobile Blade With Stationary Robot

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- +Efficient moving-line layout
- +High flexibility
- Complex control
- Requires 2× blade length for finishing bay

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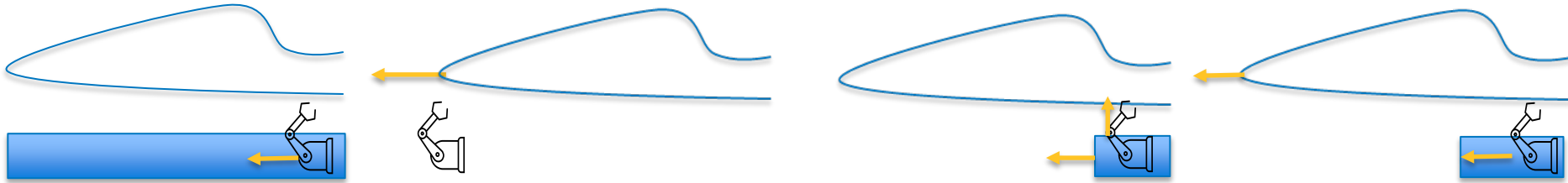
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Robot on Mobile Platform

- +Requires less factory space
- +Highly flexible
- Expensive automated guided vehicle (AGV)
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Robot on Mobile Platform

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- Complex cable management
- Complex control

Partial-Length Track With Mobile Blade

- +Lowest risk due to simplicity
- +Low cost
- +High flexibility
- Requires 2× blade length for finishing bay

Selecting a mobility design is critical for economic success

- Factory mobility is the main driver for capital costs and risk

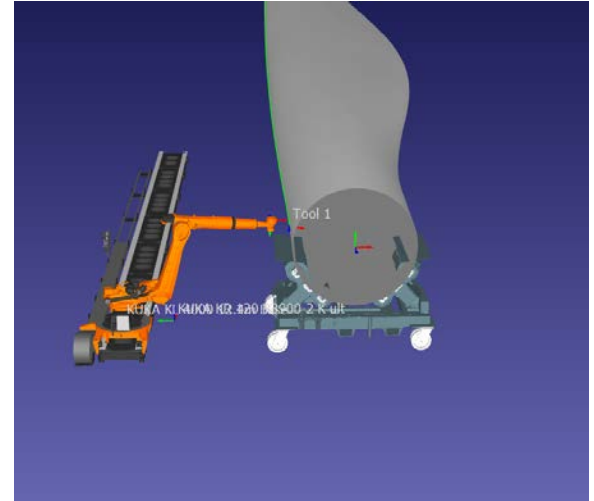


Photo by Hunter Huth, NREL

Selecting a mobility design is critical for economic success

- Factory mobility is the main driver for capital costs and risk
- Different factories have different constraints
 - Not a one-size-fits-all scenario

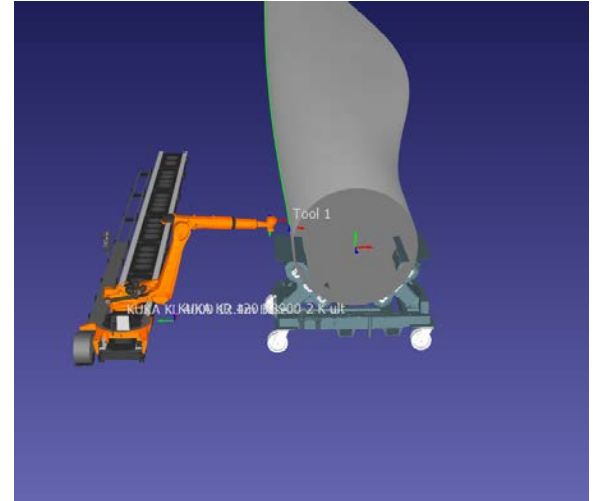


Photo by Hunter Huth, NREL

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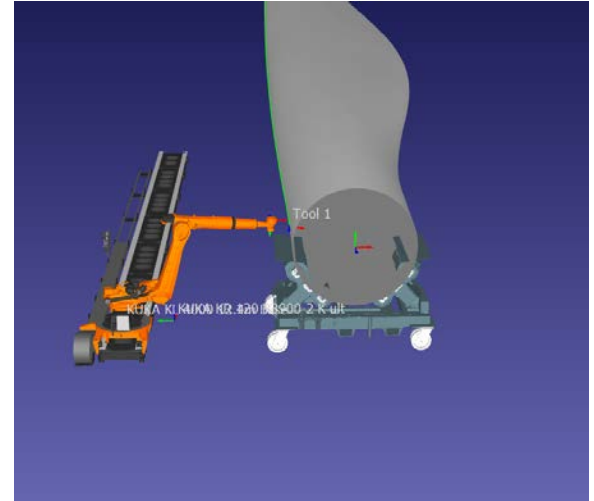


Photo by Hunter Huth, NREL

Selecting a mobility design is critical for economic success

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- Determines how adaptable this system is to new blade designs

- For this research to maximize industry impact, the rest of the system must be agnostic to mobility concept and blade design.

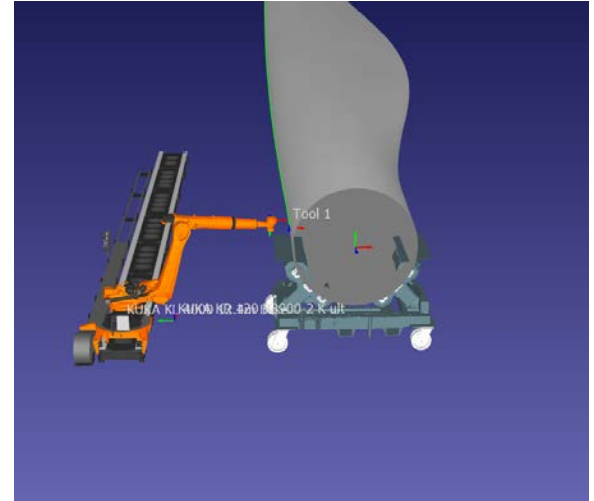


Photo by Hunter Huth, NREL

Real-time control must accompany all factory mobility concepts

- The six degrees-of-freedom of the robot arm react to the changing position of the blade
- The external motion of the blade, track, or autonomous vehicle move the robot arm along the blade.

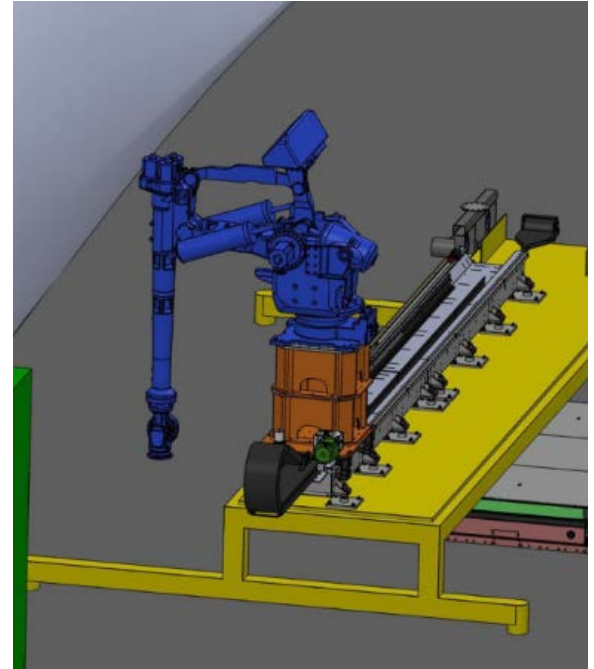


Photo by Casey Nichols, NREL

Concluding Remarks

- Automated wind blade finishing can have a large impact on blade manufacturing in the short- and mid-term

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Concluding Remarks

- Automated wind blade finishing can have a large impact on blade manufacturing in the short- and mid-term
- Custom tools for robotic manufacturing allow for improved processing speeds
- Captured data from the blade surface can be used to produce toolpaths for automated wind blade finishing
- **Real-time control can optimize speed and accuracy to make automated wind blade finishing economically viable.**

Acknowledgments

- LM Wind Power at GE Vernova
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Thank You

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