

Studying the Impact of IBR Modeling on the Commonly Applied Transmission Line Protective Elements

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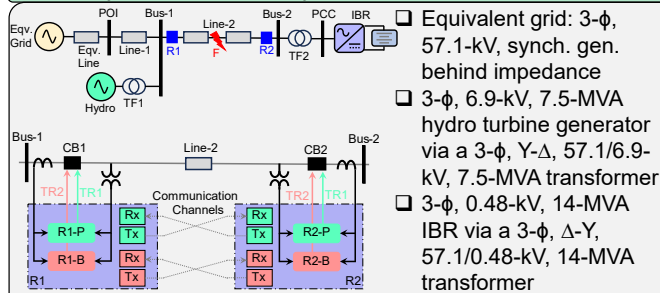
Motivations/Objectives/Problem Statement

- How does the type of the primary source on the DC side of the IBRs impact the functionality of the protective relay elements?
- How does the type of the voltage source inverter modeling of the IBRs impact the functionality of the protective relay elements?
- How does the type of the control scheme of the IBRs impact the functionality of the protective relay elements?
- How does the type of the fault current limiter scheme of the IBRs impact the functionality of the protective relay elements?

Contributions

- Identifies the dominant factors among the IBR modeling aspects, both qualitatively and quantitatively, that impact the functionalities of the relay elements
- Provides the required modifications in the fault prediction algorithms to be included in fault study software
- Provides a platform to modify settings for existing protection schemes or design new protection algorithms.

Power System Under Study



Protection System Under Study

- Line differential element \rightarrow phase current (87LP)-on each phase, ground current (87LG)-one element, negative-sequence current (87LQ)-one element
- Direction element \rightarrow directional supervision negative-sequence directional element, zero-sequence directional element
- Distance element \rightarrow distance elements using quad and mho characteristics, supervised by impedance-based directional, fault type identification logic.

IBR Model

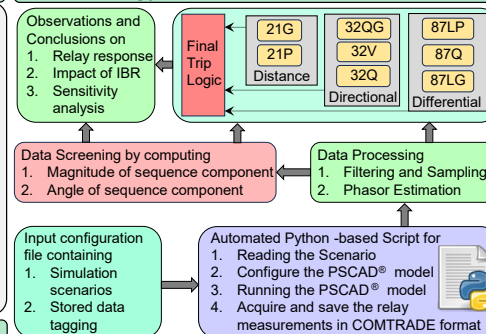
Controller Type		
Outer Power Control		Inner Current Control
Active Power	Reactive Power	dq domain
Open-loop P dispatch	Open-loop Q dispatch	$\alpha\beta$ domain
Closed-loop P dispatch	Closed-loop Q dispatch	Sequence domain
V_{dc} control	V_{dc} control	

Current Limiter	
Current Limiter Scheme	Windup Protection
Saturation - based	Anti-windup for PI controller.
d-axis priority	q-axis priority
Latching - based	Anti-windup for PR controller.
d-axis priority	q-axis priority

Controller Type		
Primary Control	Outer Voltage	Inner Current
Pf-QV droop	dq domain	dq domain
Virtual Synchronous Machine	$\alpha\beta$ domain	$\alpha\beta$ domain
	Sequence domain	Sequence domain

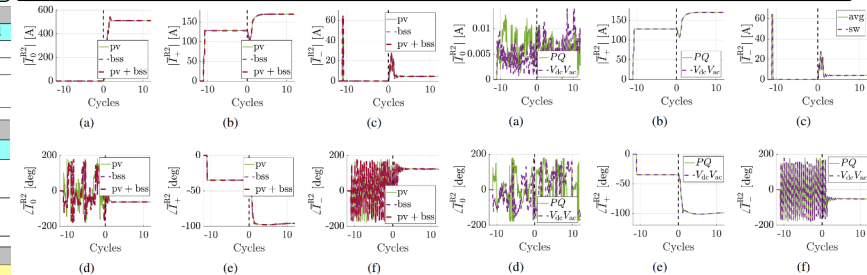
Limiter Logic	
Current Limiter	Windup
Saturation - based	Anti-windup for PI controller
d-axis priority	q-axis priority
Latching - based	Anti-windup for PR controller
d-axis priority	q-axis priority

Methodology

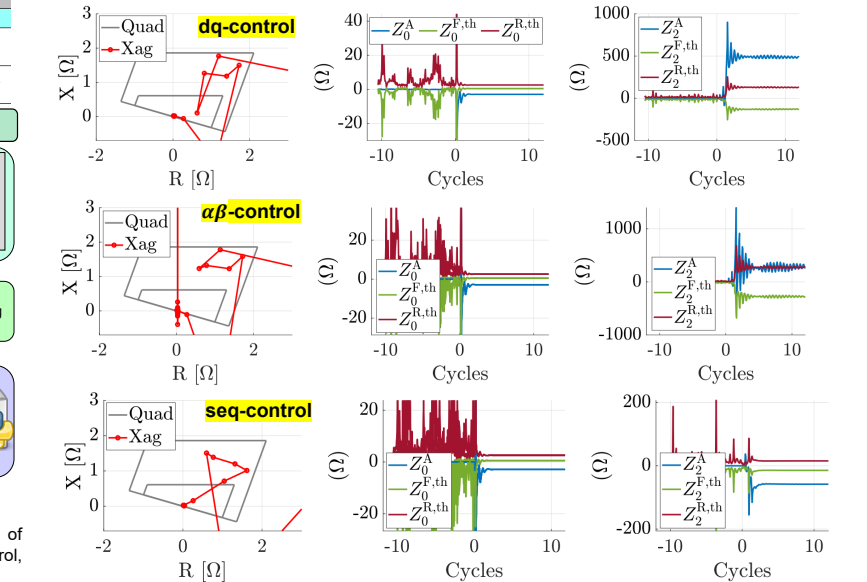


- AG fault at 'F' with $R_f = 0.01\Omega$ with TF2 as Y- Δ and Δ -Y
- BC fault at 'F' with $R_f = 0.01\Omega$ with TF2 as Δ -Y
- {# types of DC source} \times {# type of VSI model} \times {# type of outer-power control} for GFL cases: fixed current control, current limiter scheme
- {# types of inner-current control} \times {# type of current limiter scheme} for GFL cases: fixed type of DC source, VSI model, and outer-power control
- {# types of outer-power control} for GFM-IBR cases with fixed type of DC source, VSI model, inner-voltage control and current limiter scheme
- {# types of inner-voltage control} \times {# type of current limiter} for GFM-cases with fixed type of DC source, VSI model.

Key Findings



- Types of DC source, VSI model, types of outer-power controller \rightarrow No impact
- Types of inner-current controller for GFL-IBR, inner-voltage controller for GFM-IBR, and types of current-limiting scheme \rightarrow have impact on the protection schemes.



Conclusions

- Protection engineers should desensitize negative-sequence-dependent elements if the IBR does not use explicit negative-sequence current control.
- Negative-sequence directional elements require sufficient negative-sequence current with correct angle.
- The study can assist in proposing modifications to fault prediction algorithms and facilitate the development of a platform for protection algorithm design.